MONASH University



TEST REPORT EVALUATION OF STRUCTURAL WALL BRACING CAPACITY (MAXIMUM HEIGHT 2.7M) USING WILMAPLEX HOOP IRON WITH TENSIONER

CLIENT:

WILMAPLEX PTY LTD. 57 LATHAMS ROAD, CARRUM DOWNS, VIC 3201

TESTING AUTHORITY:

MONASH UNIVERSITY DEPARTMENT OF CIVIL ENGINEERING WELLINGTON ROAD CLAYTON, VIC. 3800

JOB NUMBER:

WILMAPLES/14/001

14/012

REPORT NUMBER: *Prepared By: Dr C ADAM*

This Test Report refers to testing only one sample This Test Report can only be reproduced in full

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1. Introduction

Monash University was commissioned by Wilmaplex Pty. Ltd. to evaluate the structural bracing wall capacity (horizontal racking resistance) for of timber walls braced with 30x0.8mmWilmaplex Hoop Iron straps, with studs spaced at 450 and 600mm centre to centre, as shown in Figures 1 and 2. The wall frames comprised of 90x45mm MGP10 Radiata pine frames with the straps nailed to the frame using 33mmx3.15mm flat head galvanized nails. Three replicates of each stud spacing specimens were tested at the structures laboratory at Monash University, Clayton Campus.

2. Executive summary of test results

One row of nogging, see Figures 1 and 2.						
Stress grade and	Steel strap size	Stud spacing	Bracing capacity			
size	(mm)	(mm)	(kN/m)			
MGP10	30x0.8mmG300	450	1.5			
90x45mm	Z275 steel	600	1.4			

 Table 1
 Recommended design racking load for strength

3. Test specimens details

Six MGP10 wall frames fitted with Wilmaplex Hoop iron straps and tensioner were delivered at Monash University for testing. All wall frames comprised of 90x45mm MGP radiata pine components with the first three having a 450mm stud spacing, and the second three with a 450mm stud spacing, see Figures 1 and 2. All wall frames were braced using Wilmaplex 30x0.8mm G300 Z275 steel straps, the braces were tensioned using Wilmaplex galvanized steel tensioners. The straps were connected to the top and bottom plates with 2x33mmx3.15mm nails, one on the top face and the second on the side, straps were connected to the studs with one similar nail where the strap intersected with the studs. The straps cover the following Wilmaplex codes as given in the wilmaplex 2013 catalogue, 3086M, 30815M, 30830M and 30850M. The tensioner is identified as TEN in the same catalogue.

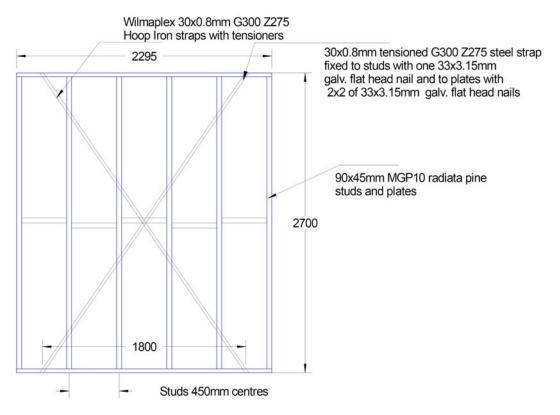


Figure 1 Wall frame specimen for 450mm stud spacing

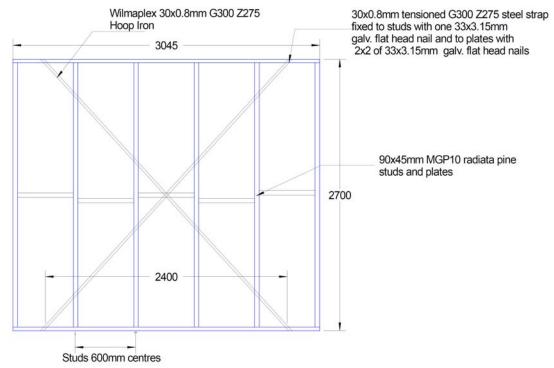


Figure 2 Racking specimen for 600mm stud spacing

4. Testing methodology

The test set-up used was similar to the method used in ASTM E72, Section 14. The test set up is shown in Figure 4, which was extracted from ASTM E72. The load was applied using a hydraulic cylinder fitted with a 50kN calibrated load cell. Four transducers were fitted onto the assembly; the first two ($D_{1a\&b}$) were located on the lower left of the wall to measure the rotation; the rotation was measured averaging the two readings. The third transducer (D_2) was located on the lower right end to measure the slippage and the forth transducer (D_3) located on the upper right end measured the total of the first three transducers plus the deformation of the panel. The net horizontal deflection of the panel at any given load, in accordance with ASTM E72, was the reading of D_3 less the sum of the readings of the average of $D_{1a\&b}$ and D_2 . Test data from all transducers and load sensors were electronically recorded.

Net deflection= D_3 - (D_1+D_2)

Note that $D_{la\&b}$ represents the average of 2 transducers that were fitted to measure the rotation of the panel.

The loading sequence followed during the racking test was to:

- apply a preload of 0.2 kN; no deflections recorded;
- load continuously increased to a level of 2kN, in around 2minutes.
- hold load for 5 minutes; then release the load

note the residual deflections;

- allow 5 minutes recovery time;
- reload to 2kN level record deflections;

• continue loading to failure and note the racking load at a deflection of 9 and 27mm, i.e. height/300 and height/100; the height was 2.7m.

After each loading cycle wall assemblies were closely examined for any signs of material or connector distress or buckling especially at the serviceability limit state levels.

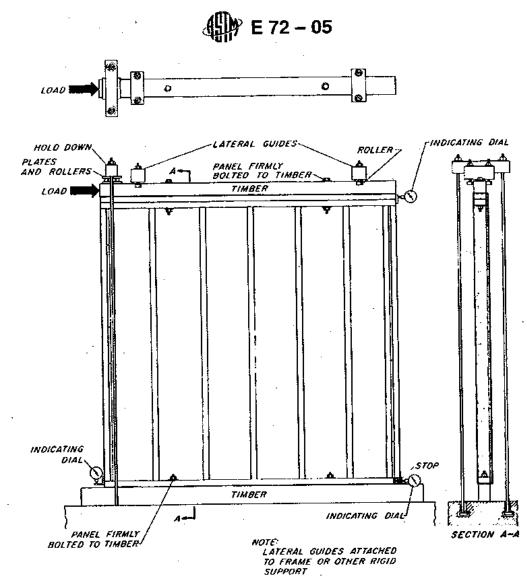


Figure 3 Racking load test setup taken from ASTM E72

5. Test results and analysis

The following criteria was followed in order to satisfy the limit state design criteria. Limit state design criteria requires that a serviceability limit (SLS) is met, this was undertaken via imposing a deflection limit of height/300, which is 9mm for the specimens tested, at this deflection level the specimen did not to show any significant signs of buckling or failure and shall be stable.

A strength limit state was established by determining the racking load capacity (ULS) at a deflection of height/100, which is 27mm for the specimens tested, at this load level the specimen continues to resist further load despite some material and fasteners might look under stress.

The recommended racking load capacity was considered to be the most critical value of the minimums of the following:

• The strength limit design load (ULS) shall be greater or equal to the serviceability limit state (SLS) load multiplied by a factor 1.5 to ensure stability.

• The strength limit design load shall be less or equal to 0.85 of the ultimate load (ULT), this serves as what is defined as a capacity factor for limit state design in AS1720.1 for housing structures.

Tables 2 and 3 give all the calculated test data for the 450 and 600mm stud spacing consecutively.

Table 2	Summary of test data analysis and evaluation for walls
with 450m	m stud spacing

Wall type	1.5xSLS	ULS	0.85xULT
1	0.9	1.6	1.6
2	1.2	1.6	1.6
3	1.2	1.6	1.6
Mean	1.1	1.6	1.6
Minimum		1.6	1.6

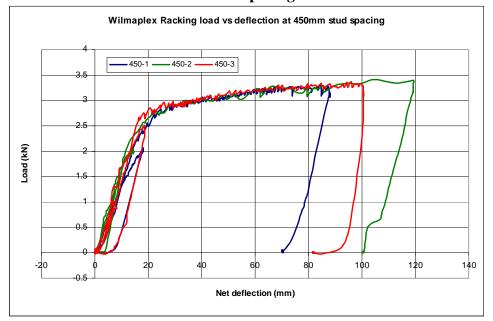
Note that in Table 1, the recommended bracing capacity is 1.5kN which is less than the tested value of 1.6kN to be compatible with AS1684.2, Table 8.18.

Table 3Summary of test data analysis and evaluation for wallswith 600mm stud spacing

Wall type	1.5xSLS	ULS	0.8xULT
1	0.9	1.5	1.5
2	0.6	1.4	1.4
3	0.6	1.5	1.4
Mean	0.7	1.5	1.4
Minimum		1.4	1.4

Note that the recommended bracing capacity is 1.4kN which is less than the 1.5kN quoted in AS1684.2, Table 8.18, the difference between the layout described in Table 8.18 and the actual wall panel tested is that the tested wall bracing strap was connected to the plates with 2 nails only in lieu of the AS1684's 3 nails.

6. Detailed test results

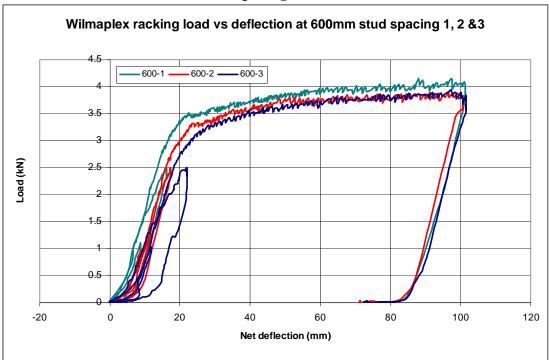


6.1. Walls with 450mm stud spacing test results

Figure 5 Racking load versus net deflection D3 for 450mm stud spacing

Mode of failure:

Specimen 450-1, 2 and 3: Frame distorting diagonally, strap buckling on the compression side.



6.2. Walls with 600mm stud spacing test results

Figure 6 Racking load versus net deflection D3 for 600mm stud

Mode of failure:

Specimen 600-1, 2 and 3: Frame distorting diagonally, strap buckling on the compression side.

APPENDIX



Figure A1 Test set-up for the 450mm studs wall



Figure A2 Transducers measuring the uplift.



Figure A3 Hydraulic cylinder and a load cell fitted to apply the racking load.



Figure A4 Typical mode of failure, diagonal distortion and buckling of strap in the compression side.

BLUESCOPE STEEL TEST CERTIFICATE

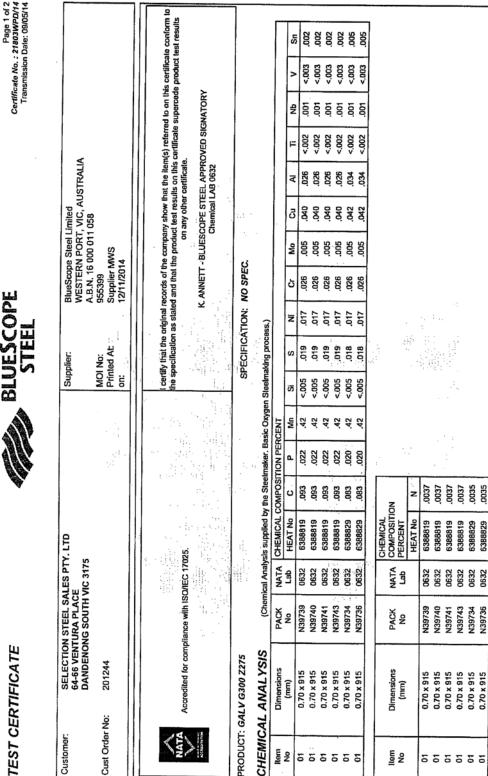


Figure A5 Steel test certificate