## SD2932 RF MOSFET for 300 W FM amplifier

## Introduction

This application note gives a description of a broadband power amplifier operating over the frequency range 88-108 MHz using the new STMicroelectronics RF MOSFET transistor SD2932.

Table 1. Typical achievable performances

| Parameter | Performance |
| :---: | :---: |
| Device | $1 \times$ SD2932 |
| Frequency | $88-108 \mathrm{MHz}$ |
| Vdd | 50 V |
| Idq | 200 mA |
| Pout | 300 W |
| Gain | $>19 \mathrm{~dB}$ |
| Input return loss | $<-11 \mathrm{~dB}$ |
| Drain efficiency | $>70 \%$ |

## 1 Amplifier design

### 1.1 Input matching network

Typical input gate-to-gate impedance of SD2932 at 100 MHz is $\mathrm{Zin}=\mathrm{Rs}+\mathrm{jXs}=2-2.6 \mathrm{j}$, and can also be expressed as the combination of parallel resistance and reactance using the following formulas:

## Equation 1

$$
\mathrm{Rp}=\mathrm{Rs} \bullet\left[1+\left(\frac{\mathrm{Xs}}{\mathrm{Rs}}\right)^{2}\right]=5.38 \Omega
$$

## Equation 2

$$
X_{P}=R_{P} /\left(\frac{X_{S}}{R_{S}}\right)=-4.14 j \Omega
$$

Therefore, in order to achieve good input matching performances over the frequency range $88-108 \mathrm{MHz}$ the unbalanced $50 \Omega$ is to be transformed into an impedance with a value as close as possible to Rp of $5.38 \Omega$

From the circuit schematic given in Figure 6 , we can see that the input matching network is based on a two section balun (1:1 balun in cascade with a $9: 1$ balun transformer) which transforms the unbalanced $50 \Omega$ to a balanced $5.56 \Omega(2 \times 2.78 \Omega / 9: 1$ ratio). The first section, a 5" long - $50 \Omega$ coaxial cable and the second section, a two 3.9" long - $25 \Omega$ flexible coaxial cables with ferrite core NEOSIDE, are connected as described: a 10 nH inductor (L1) is connected between the two gates to compensate SD2932 input parallel reactance Xp.

### 1.2 Input matching network tuning

Figure 1. Input Impedance of $1: 1$ balun in cascade with $4: 1$ balun


Figure 2. Input Impedance of 1:1 balun in cascade with $9: 1$ balun


SD2932 input matching network was tuned in order to achieve the best compromise in terms of power gain (Gp) and input return loss (Rtl) over the frequency range $88-108 \mathrm{MHz}$. Best results were achieved by adding a 10 pF chip capacitor (C1) between RFIN and the 1 nF blocking capacitor (C2).

### 1.3 Output matching network

The output impedance of each side is a combination of the output capacitance Coss ( 195 pF ) and the optimum load resistance which can be determined as follows:

## Equation 3

$$
\mathrm{Rp}=\frac{(0.85 \cdot \mathrm{Vdd})^{2}}{2 \cdot \text { Pout }}=\frac{0.85 \cdot 2500}{2 \cdot 150 \mathrm{~W}}=6.02 \Omega
$$

The total optimum load, seen by SD2932 (drain to drain), is $2 \times 6.02=12.04 \Omega$ Therefore, a simple two section balun ( $1: 1$ balun in cascade with a $4: 1$ balun transformer) is used to transform the unbalanced $50 \Omega$ to a balanced $12.5 \Omega(2 \times 6.25 \Omega)$ which is very near to the total optimum load resistance.

The first section, a $5^{\prime \prime}$ long - $50 \Omega$ flexible coaxial cable, and the second section, two 5 " long - $25 \Omega$ flexible coaxial cables, are connected as described in Figure 6.

To compensate for the output capacitance Coss of SD2932, a 40 nH inductor (L2) is connected between the two drains. This LC network (L2 \& Coss) is a high pass filter with a resonance frequency calculated at $10 \%$ below the minimum operating frequency:

## Equation 4

$$
C_{O S S}=\frac{C_{\text {OSS }}(\text { per side })}{2}=\frac{180 \mathrm{pF}}{2}=90 \mathrm{pF}
$$

## Equation 5

$$
\text { Frequency of resonance }=0.9 \bullet 88 \mathrm{MHz}=80 \mathrm{MHz}
$$

## Equation 6

$$
\mathrm{L} 2 \cdot \text { Coss } \cdot(2 \cdot \mathrm{pi} \cdot F)^{2}=1 \rightarrow L 2=44 \mathrm{nH}
$$

Figure 3. Power gain vs. frequency


Figure 4. Drain efficiency vs. frequency


Figure 5. Drain efficiency vs. frequency


## 2 SD2932 typical performances and conclusion

Figure 3, Figure 4 and Figure 5 show power gain, efficiency and input return loss over the frequency range $88-108 \mathrm{MHz}$ at a constant output power of 300 W and a drain supply voltage of 50 V and a quiescent current of 200 mA . Typical performances are as follows:

Table 2. Typical performances

| Parameters | Min | Max |
| :---: | :---: | :---: |
| Gp | 19.3 dB | 19.6 dB |
| $\mathrm{R}_{\mathrm{TL}}$ | -18 dB | -11 dB |
| Eff | $71 \%$ | $73 \%$ |

Finally, in this report we have demonstrated ST's SD2932 MOSFET transistor excellent performance as a wideband $300 \mathrm{~W}-50 \mathrm{~V}$ push-pull amplifier for FM applications.

Figure 6. $\quad \mathbf{8 8 - 1 0 8} \mathbf{~ M H z}$ circuit schematic


Table 3. 88-108 MHz circuit components list

| Symbol | Description |
| :---: | :---: |
| PCB | $1 / 32^{\prime \prime}$ Woven fiberglass $0.0030 \mathrm{Cu}, 2$ side, er |
| T1 | $50 \Omega$ Flexible coax cable OD $0.006 ", 5 "$ long |
| T2/ T3 | $9: 1$ Transformer, $25 \Omega$ flexible coax cable OD $0.1 " 3.9 "$. ferrite core NEOSIDE |
| T4 / T5 | $4: 1$ Transformer, $25 \Omega$ flexible coax cable OD $0.1 " 5.0 "$ long. |
| T6 | $50 \Omega$ flexible coax cable OD $0.1 " 5.0^{\prime \prime}$ long. |
| FB1 | VK200 |
| C1 | 10 pf Ceramic capacitor |
| C2/C3/C4/C7/C8 | 1 nF Chip capacitor |
| C5/C6 | 1 nF ATC chip capacitor |

Table 3. 88-108 MHz circuit components list (continued)

| Symbol | Description |
| :---: | :---: |
| C9 | 470 pF ATC chip capacitor |
| C10 | 100 nF chip capacitor |
| R1 | $56 \Omega$ Resistor |
| R2/R4 | $10 \Omega$ Chip resistor |
| R3 | $10 \mathrm{~K} \Omega$ Resistor |
| R5 | $5.6 \mathrm{~K} \Omega$ Resistor |
| R6 | $10 \mathrm{~K} \Omega 10$ Turn trim resistor |
| R7 | $3.3 \mathrm{~K} \Omega 1$ W Resistor |
| R8 | $15 \Omega 1$ W Resistor |
| D1 | 6.8 V Zener diode |
| L1 | 10 nH inductor |
| L2 | 40 nH inductor |
| L3 | 70 nH inductor |

## 3 Revision history

Table 4. Revision history

| Date | Revision | Changes |
| :---: | :---: | :--- |
| 21-Jun-2006 | 2 | Minor text changes |
| 30-Jul-2007 | 3 | The document has been reformatted |

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