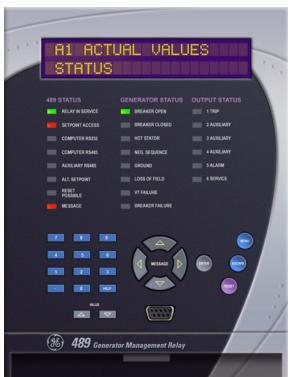




Firmware Revision: 4.0X

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Part number: 1601-0150-AC (April 2009)



Multilink Hardened Ethernet Switch -

A Dependable way to Network your Relays and Meters



ML2400

19" Rack-mounted Managed Switch



ML1600

9" Rack-mounted Managed Switch



ML600 Unmanaged Compact Switch



Ability to withstand Harsh Environments

- IEC 61850-3 compliant for electric utility substations
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- Secure Web Management
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TOC TABLE OF CONTENTS

Table of Contents

1: GETTING STARTED	IMPORTANT PROCEDURES	1_1
1. 02111110 31/11(12)	CAUTIONS AND WARNINGS	
	Inspection Checklist	
/	Manual Organization	
	USING THE RELAY	1
	Menu Navigation	
	PANEL KEYING EXAMPLE	
/ \	CHANGING SETPOINTS	
/ \	INTRODUCTION	
/ \ \	THE HELP KEY	
	NUMERICAL SETPOINTS	
	ENUMERATION SETPOINTS	
	OUTPUT RELAY SETPOINTS	
	TEXT SETPOINTS	-
	INSTALLATION	
	PLACING THE RELAY IN SERVICE	
	TESTING	1-16
2. INTRODUCTION	OVERVIEW	2 1
2: INTRODUCTION	DESCRIPTION	
	Ordering	
	OTHER ACCESSORIES	
	SPECIFICATIONS	
	INPUTS	= •
	OUTPUTS	
	Protection	
	DIGITAL INPUTS	
	Monitoring	
	POWER SUPPLY	
	COMMUNICATIONS	
	Testing	
	Certification	
	Physical	
	Environmental	2-15
	LONG-TERM STORAGE	2-16
7 INICTALL ATION	MECHANICAL INCTALLATION	7.1
3: INSTALLATION	MECHANICAL INSTALLATION	
	Description	
	Product Identification	
	INSTALLATION	
	Unit Withdrawal and Insertion	
	ETHERNET CONNECTION	
	Terminal Locations	
	ELECTRICAL INSTALLATION	
	Typical Wiring	
	GENERAL WIRING CONSIDERATIONS	
	Control Power	3-10
	Current Inputs	3-11

	VOLTAGE INPUTS	7 1/1	
	DIGITAL INPUTS		
	ANALOG INPUTS		
	ANALOG OUTPUTS		
A	RTD Sensor Connections		
/	OUTPUT RELAYS		
/	IRIG-B		
/ 1	RS485 PORTS		
	DIELECTRIC STRENGTH	3-18	
/ INTERFACES 546	EDI ATE A TEDEA CE	- 11	
4: INTERFACES FAC	EPLATE INTERFACE		
/ \	DISPLAY		
	LED INDICATORS		
	RS232 PROGRAM PORT	,	
	Keypad		
	SETPOINT ENTRY		
	DIAGNOSTIC MESSAGES	4-8	
	Self-Test Warnings	4-8	
	FLASH MESSAGES	4-9	
ENE	RVISTA SOFTWARE INTERFACE	4-10	
	Overview	4-10	
	Hardware	4-10	
	INSTALLING THE ENERVISTA 489 SETUP SOFTWARE		
CON	INECTING ENERVISTA 489 SETUP TO THE RELAY		
	Configuring Serial Communications		
	Using the Quick Connect Feature		
	Configuring Ethernet Communications		000
	CONNECTING TO THE RELAY	2000	bUL
WO	RKING WITH SETPOINTS AND SETPOINT FILES		
VVO	ENGAGING A DEVICE		
	ENTERING SETPOINTS		
LIDO	USING SETPOINT FILES		
UPG			
	DESCRIPTION		
	SAVING SETPOINTS TO A FILE		
	LOADING NEW FIRMWARE		
ADV	'ANCED ENERVISTA 489 SETUP FEATURES		
	Triggered Events		
	Waveform Capture (Trace Memory)		
	Phasors	4-35	
	Trending (Data Logger)	4-37	
	EVENT RECORDER	4-40	
	MODBUS USER MAP	4-41	
	VIEWING ACTUAL VALUES	4-41	
USIN	NG ENERVISTA VIEWPOINT WITH THE 489		
	PLUG AND PLAY EXAMPLE		
5: SETPOINTS OVE	RVIEW	5-1	_
3,1	SETPOINT MESSAGE MAP		
	TRIPS / ALARMS/ CONTROL FEATURES		
	RELAY ASSIGNMENT PRACTICES		
	DUAL SETPOINTS		
	2 Of IL 3 LTT 011 VI 13		

COMMISSIONING	5-8
S1 489 SETUP	5-9
Passcode	5-9
Preferences	5-10
COMMUNICATIONS	5-12
REAL TIME CLOCK	5-13
Default Messages	5-14
Message Scratchpad	5-15
CLEAR DATA	5-16
S2 SYSTEM SETUP	5-18
CURRENT SENSING	5-18
VOLTAGE SENSING	5-18
GENERATOR PARAMETERS	5-19
Serial Start/Stop Initiation	
\$3 DIGITAL INPUTS	5-21
DESCRIPTION	5-21
Breaker Status	5-21
GENERAL INPUT A TO G	5-22
REMOTE RESET	5-23
Test Input	5-23
Thermal Reset	5-23
Dual Setpoints	5-24
Sequential Trip	5-25
Field-Breaker	5-26
Tachometer	5-26
WAVEFORM CAPTURE	5-27
GROUND SWITCH STATUS	, 5-27
S4 OUTPUT RELAYS	5-28
Description	5-28
Relay Reset Mode	
S5 CURRENT ELEMENTS	
Inverse Time Overcurrent Curve Characteristics	
OVERCURRENT ALARM	
OFFLINE OVERCURRENT	
Inadvertent Energization	
Phase Overcurrent	
NEGATIVE SEQUENCE	
GROUND OVERCURRENT	
Phase Differential	
GROUND DIRECTIONAL	
HIGH-SET PHASE OC	
S6 VOLTAGE ELEMENTS	
Undervoltage	
OVERVOLTAGE	
Volts/Hertz	
Phase Reversal	
Underfrequency	
OVERFREQUENCY	
NEUTRAL OVERVOLTAGE	
Neutral Undervoltage	
LOSS OF EXCITATION	
DISTANCE ELEMENT	
S7 POWER ELEMENTS	
Power Measurement Conventions	5-60

	REACTIVE POWER	5	5-61
	Reverse Power	5	5-62
	Low Forward Power	5	5-63
	S8 RTD TEMPERATURE	5	5-64
	RTD Types	5	5-64
	//h	5	
	/ \	5	
	/ \		
		5	
		5	
A.			
/ `		5	
/		5	
/ 1		5	
		5	
		5	
		5	
		5	
		5	
		5	
		5	
		5	
		5	
		5	
	S12 TESTING	0.5	5-100
	Simulation Mode		5-100
		5	
		5	
	TEST ANALOG OUTPUT	5	5-103
	COMM PORT MONITOR	5	5-104
	FACTORY SERVICE	5	5-104
6: ACTUAL VALUES	OVFRVIFW	6	5-1
		6	
	Description	6	5-3
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
		6	
	DEMAND METERING	C	J-2U

TOC TABLE OF CONTENTS

	ANALOG INPUTS	6-20
	Speed	
	A3 LEARNED DATA	
	Parameter Averages	
	RTD MAXIMUMS	
	Analog Input Min/Max	
	A4 MAINTENANCE	
	TRIP COUNTERS	
/	GENERAL COUNTERS	
	TIMERS	
	A5 EVENT RECORDER	
/ \	EVENT RECORDER	
/ \	A6 PRODUCT INFORMATION	
	489 MODEL INFO	
	Calibration Info	
	DIAGNOSTICS	
	DIAGNOSTIC MESSAGES	
	FLASH MESSAGES	6-33
7: TESTING	TEST SETUP	
	Description	
	HARDWARE FUNCTIONAL TESTS	
	Output Current Accuracy	7-4
	Phase Voltage Input Accuracy	7-4
	GROUND (1 A), NEUTRAL, AND DIFFERENTIAL CURRENT ACCURACY	7-5
	NEUTRAL VOLTAGE (FUNDAMENTAL) ACCURACY	7-6
	Negative Sequence Current AccuracyRTD Accuracy	im
	RTD Accuracy	10070420
	DIGITAL INPUTS AND TRIP COIL SUPERVISION	7-9
	ANALOG INPUTS AND OUTPUTS	
	OUTPUT RELAYS	7-11
	ADDITIONAL FUNCTIONAL TESTS	
	Overload Curve Accuracy	
	Power Measurement Test	
	REACTIVE POWER ACCURACY	
	Voltage Phase Reversal Accuracy	
	INJECTION TEST SETUP #2	
	GE MULTILIN 50:0.025 GROUND ACCURACY	
	NEUTRAL VOLTAGE (3RD HARMONIC) ACCURACY	
	Phase Differential Trip Accuracy	
	INJECTION TEST SETUP #3	
	VOLTAGE RESTRAINED OVERCURRENT ACCURACY	
	DISTANCE ELEMENT ACCURACY	/-21
APPENDIX	STATOR GROUND FAULT	
	Description Neutral Overvoltage Element	
	GROUND OVERCURRENT ELEMENT	
	GROUND DIRECTIONAL ELEMENT	
	THIRD HARMONIC VOLTAGE ELEMENT	
	REFERENCES	
	STATOR DIFFERENTIAL PROTECTION SPECIAL APPLICATION	A-8

Background	
Stator Differential Logic	A-9
CURRENT TRANSFORMERS	A-11
GROUND FAULT CTS FOR 50:0.025 A CT	
GROUND FAULT CTS FOR 5 A SECONDARY CT	A-13
Phase CTs	A-13
TIME OVERCURRENT CURVES	A-15
ANSI Curves Definite Time Curves IAC Curves	A-15
DEFINITE TIME CURVES	A-19
IAC CURVES	A-20
IEC Curves	
REVISION/HISTORY	A-27
CHANGE NOTES	A-27
Changes to the 489 Manual	
EU DECLARATION OF CONFORMITY	
EU DECLARATION OF CONFORMITY	
WARRANTY	A-31
GE MULTILIN WARRANTY	







1.1 **Important Procedures**

1.1.1 Cautions and Warnings

Please read this chapter to guide you through the initial setup of your new relay.





Before attempting to install or use the relay, it is imperative that all WARNINGS and CAUTIONS in this manual are reviewed to help prevent personal injury, equipment damage, and/or downtime.

Inspection Checklist 1.1.2

- Open the relay packaging and inspect the unit for physical damage.
- View the rear nameplate and verify that the correct model has been ordered.
- Ensure that the following items are included:
 - Instruction Manual
 - GE EnerVista CD (includes software and relay documentation)
 - mounting screws
- For product information, instruction manual updates, and the latest software updates, please visit the GE Multilin website at http://www.GEmultilin.com.



If there is any noticeable physical damage, or any of the contents listed are missing, please contact GE Multilin immediately.

1.1.3 Manual Organization

Reading a lengthy instruction manual on a new product is not a task most people enjoy. To speed things up, this introductory chapter provides guidelines for basic relay usability. Important wiring considerations and precautions discussed in *Electrical Installation* on page 3–9 should be observed for reliable operation. Detailed information regarding accuracy, output relay contact ratings, and so forth are detailed in *Specifications* on page 2–6. The remainder of this manual should be read and kept for reference to ensure maximum benefit from the 489 Generator Management Relay. For further information, please consult your local sales representative or the factory. Comments about new features or modifications for your specific requirements are welcome and encouraged.

Setpoints and actual values are indicated as follows in the manual:

A4 MAINTENANCE $\triangleright \nabla$ TRIP COUNTERS \triangleright TOTAL NUMBER OF TRIPS

This 'path representation' illustrates the location of an specific actual value or setpoint with regards to its previous menus and sub-menus. In the example above, the **TOTAL NUMBER OF TRIPS** actual value is shown to be an item in the **TRIP COUNTERS** sub-menu, which itself is an item in the **A4 MAINTENANCE** menu, which is an item of **ACTUAL VALUES**.

Sub-menu levels are entered by pressing the MESSAGE ▶ or ENTER key. When inside a submenu, the ◀ MESSAGE or ESCAPE key returns to the previous sub-menu. The MESSAGE ▼ and MESSAGE ▲ keys are used to scroll through the settings in a sub-menu. The display indicates which keys can be used at any given point.



1.2 Using the Relay

1.2.1 Menu Navigation

The relay has three types of display messages: actual value, setpoint, and target messages. A summary of the menu structure for setpoints and actual values can be found at the beginning of chapters 5 and 6, respectively.

Setpoints are programmable settings entered by the user. These types of messages are located within a menu structure that groups the information into categories. Navigating the menu structure is described below.

Actual values include the following information:

. Generator and System Status:

- a. Generator status either online, offline, or tripped.
- b. The status of digital inputs.
- c. Last trip information, including values such as cause of last trip, time and date of trip, pre-trip temperature measurements, pre-trip analog inputs values, and pretrip instantaneous values of power system quantities.
- d. Active alarms.
- e. Relay date and time.

2. Metering Data:

- Instantaneous current measurements including phase, neutral, and ground currents.
- Instantaneous phase to phase and phase to ground voltages (depending on the VT connections), average voltage, and system frequency.
- c. Power quantities including apparent, real and reactive power.
- d. Current and power demand including peak values.
- e. Analog inputs.
- f. Generator speed.
- g. System phasors.
- h. RTD temperatures.

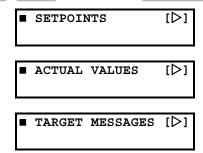
3. Learned Data:

- a. Average magnitudes of generator load, negative-sequence current, and phase-phase voltage.
- b. RTD learned data, which includes the maximum temperature measured by each of the twelve (12) RTDs.
- c. Minimum and maximum values of analog inputs.
- 4. Maintenance data. This is useful statistical information that may be used for preventive maintenance. It includes:
 - a. Trip counters

- b. General counters such as number of breaker operations and number of thermal resets.
- c. Generator hours online timer.
- 5. Event recorder downloading tool.
- 6. Product information including model number, firmware version, additional product information, and calibration dates.
- 7. Oscillography and data logger downloading tool.

Alarm, trip conditions, diagnostics, and system flash messages are grouped under *Target Messages*.

Press the MENU key to access the header of each menu, which will be displayed in the following sequence:



To access setpoints,

- > press the MENU key until the display shows the header of the setpoints menu
- Press the MESSAGE ▶ or ENTER key to display the header for the first setpoints page.

The setpoint pages are numbered, have an 'S' prefix for easy identification and have a name which provides a general idea of the settings available in that page.

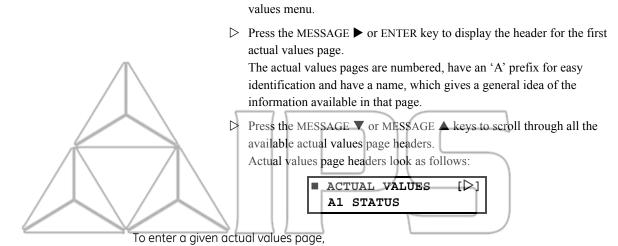
Press the MESSAGE ▼ and MESSAGE ▲ keys to scroll through all the available setpoint page headers.
Setpoint page headers look as follows:



To enter a given setpoints page,

- ▶ Press the MESSAGE ▶ or ENTER key.
- Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through sub-page headers until the required message is reached.
 The end of a page is indicated by the message END OF PAGE. The beginning of a page is indicated by the message TOP OF PAGE.

To access actual values.



- ▶ Press the MESSAGE ▶ or ENTER key.
- Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through sub-page headers until the required message is reached.
 The end of a page is indicated by the message END OF PAGE. The beginning of a page is indicated by the message TOP OF PAGE.

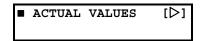
Press the MENU key until the display shows the header of the actual

Similarly, to access additional sub-pages,

- Press the MESSAGE ▶ or ENTER key to enter the first sub-page,
- Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through the available sub-pages, until the desired message is reached.
 The process is identical for both setpoints and actual values.

The following procedure illustrates the key sequence to access the Current Demand actual values.

Press the MENU key until you reach the actual values main menu.



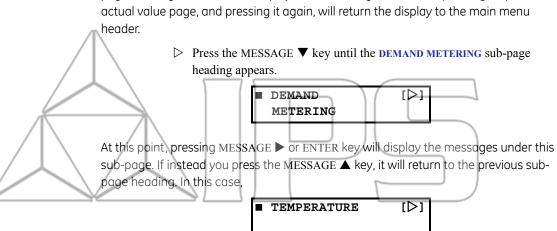
- ▶ Press MESSAGE ▶ or ENTER key to enter the first actual values page.
- Press the MESSAGE ▼ or MESSAGE ▲ key to scroll through pages, until the A2 METERING DATA page appears.



Press the MESSAGE ▶ or ENTER key to display the first sub-page heading for the Metering Data actual values page:

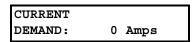


Pressing the MESSAGE ▼ or MESSAGE ▲ keys will scroll the display up and down through the sub-page headers. Pressing the ◀ MESSAGE or ESCAPE key at any sub-page heading will return the display to the heading of the corresponding setpoint or actual value page, and pressing it again, will return the display to the main menu header.



When the symbols \blacksquare and $[\triangleright]$ appear on the top line, it indicates that additional subpages are available and can be accessed by pressing the MESSAGE \blacktriangleright or ENTER key.

Press the MESSAGE ▶ or ENTER while at the Demand Metering subpage heading to display the following:



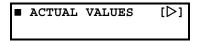
- ▶ Press ■ MESSAGE key to return to the Demand Metering sub-page heading.
- Press the MESSAGE ▼ key to display the next actual value of this subpage.

Actual values and setpoints messages always have a colon separating the name of the value and the actual value or setpoint. This particular message displays the current demand as measured by the relay.

The menu path to the value shown above is indicated as A2 METERING DATA > DEMAND METERING > CURRENT DEMAND. Setpoints and actual values messages are referred to in this manner throughout the manual.

For example, the A4 MAINTENANCE > TRIP COUNTERS > TOTAL NUMBER OF TRIPS path representation describes the following key-press sequence:

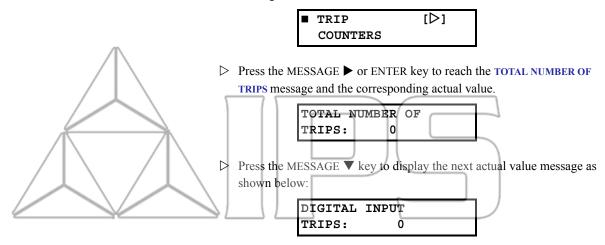
Press the MENU key until the actual value header appears on the display.



Press MESSAGE ▶ or the ENTER key, and then MESSAGE ▼ key until the A4 MAINTENANCE message is displayed.

■ ACTUAL VALUES	[▷]
A4 MAINTENANCE	

Press the MESSAGE ▶ or ENTER key to display TRIP COUNTERS message.



- Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll the display up and down through all the actual value displays in this corresponding subpage.
- Press the ■ MESSAGE key to reverse the process described above and return the display to the previous level.



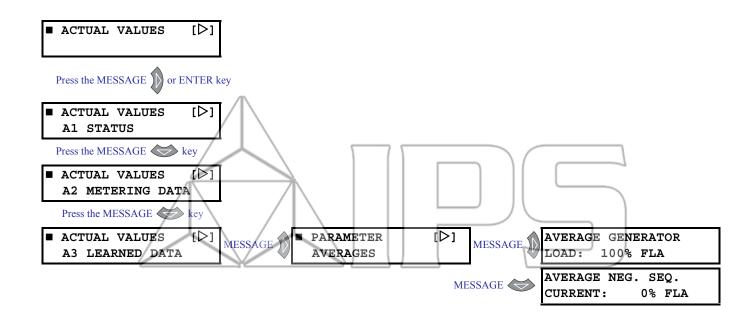
Press the ■ MESSAGE key twice to return to the A4 MAINTENANCE page header.



1.2.2 Panel Keying Example

The following figure provides a graphical example of how the keypad is used to navigate through the menu structure. Specific locations are referred to throughout this manual by using a 'path representation'. The example shown in the figure gives the key presses required to read the average negative-sequence current denoted by the path A3 LEARNED DATA > PARAMETER AVERAGES > ∇ AVERAGE NEG. SEQ. CURRENT.

Press the menu key until the relay displays the actual values page.



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1.3 Changing Setpoints

1.3.1 Introduction

There are several classes of setpoints, each distinguished by the way their values are displayed and edited.

The relay's menu is arranged in a tree structure. Each setting in the menu is referred to as a setpoint, and each setpoint in the menu may be accessed as described in the previous section.

The settings are arranged in pages with each page containing related settings; for example, all the Phase Overcurrent settings are contained within the same page. As previously explained, the top menu page of each setting group describes the settings contained within that page. Pressing the MESSAGE keys allows the user to move between these top menus.

All of the 489 settings fall into one of following categories: device settings, system settings, digital input settings, output relay settings, current element settings, voltage element settings, power element settings, RTD temperature settings, thermal model settings, monitoring settings, analog input/output settings, and testing settings.



IMPORTANT NOTE: Settings are stored and used by the relay immediately after they are entered. As such, caution must be exercised when entering settings while the relay is in service. Modifying or storing protection settings is not recommended when the relay is in service since any incompatibility or lack of coordination with other previously saved settings may cause unwanted operations.

Now that we have become more familiar with maneuvering through messages, we can learn how to edit the values used by all setpoint classes.

Hardware and passcode security features are designed to provide protection against unauthorized setpoint changes. Since we will be programming new setpoints using the front panel keys, a hardware jumper must be installed across the setpoint access terminals (C1 and C2) on the back of the relay case. Attempts to enter a new setpoint without this electrical connection will result in an error message.

The jumper does not restrict setpoint access via serial communications. The relay has a programmable passcode setpoint, which may be used to disallow setpoint changes from both the front panel and the serial communications ports. This passcode consists of up to eight (8) alphanumeric characters.

The factory default passcode is "0". When this specific value is programmed into the relay it has the effect of removing all setpoint modification restrictions. Therefore, only the setpoint access jumper can be used to restrict setpoint access via the front panel and there are no restrictions via the communications ports.

When the passcode is programmed to any other value, setpoint access is restricted for the front panel and all communications ports. Access is not permitted until the passcode is entered via the keypad or is programmed into a specific register (via communications). Note that enabling setpoint access on one interface does not automatically enable access for any of the other interfaces (i.e., the passcode must be explicitly set in the relay via the interface from which access is desired)

A front panel command can disable setpoint access once all modifications are complete. For the communications ports, writing an invalid passcode into the register previously used to enable setpoint access disables access. In addition, setpoint access is automatically disabled on an interface if no activity is detected for thirty minutes.

The EnerVista 489 Setup software incorporates a facility for programming the relay passcode as well as enabling and disabling setpoint access. For example, when an attempt is made to modify a setpoint but access is restricted, the software will prompt the user to enter the passcode and send it to the relay before the setpoint is actually written to the relay. If a SCADA system is used for relay programming, it is the programmer's responsibility to incorporate appropriate security for the application.

1.3.2 The HELP Key

Pressing the HELP key displays context-sensitive information about setpoints such as the range of values and the method of changing the setpoint. Help messages will automatically scroll through all messages currently appropriate.

1.3.3 Numerical Setpoints

Each numerical setpoint has its own minimum, maximum, and step value. These parameters define the acceptable setpoint value range. Two methods of editing and storing a numerical setpoint value are available.

The first method uses the 489 numeric keypad in the same way as any electronic calculator. A number is entered one digit at a time with the 0 to 9 and decimal keys. The left-most digit is entered first and the right-most digit is entered last. Pressing ESCAPE before the ENTER key returns the original value to the display.

The second method uses the VALUE ▲ key to increment the displayed value by the step value, up to a maximum allowed value. Likewise, the VALUE ▼ key decrements the displayed value by the step value, down to a minimum value. For example:

Select the S1 489 SETUP ▷ ▼ PREFERENCES ▷ ▼ DEFAULT MESSAGE TIMEOUT setpoint message.

> DEFAULT MESSAGE TIMEOUT: 300 s

Press the 1, 2, and 0 keys. The display message will change as shown.

DEFAULT MESSAGE TIMEOUT: 120 s

Until the ENTER key is pressed, editing changes are not registered by the relay. Therefore.

Press the ENTER key to store the new value in memory. The following message will momentarily appear as confirmation of the storing process.

> NEW SETPOINT HAS BEEN STORED

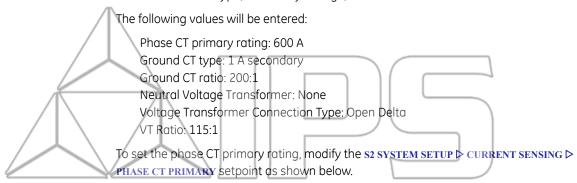
■ SETPOINTS

Press MESSAGE ▶ or ENTER

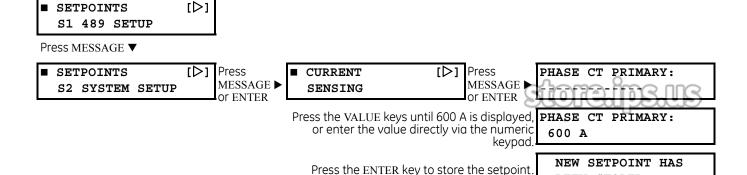
1.3.4 Enumeration Setpoints

[\(\)]

The example shown in the following figures illustrates the keypress sequences required to enter system parameters such as the phase CT primary rating, ground CT primary rating, bus VT connection type, secondary voltage, and VT ratio.



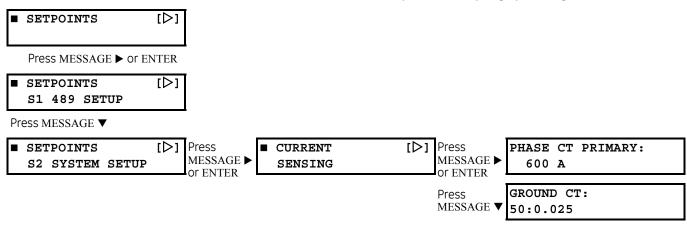
Press the MENU key until the relay displays the setpoints menu header.



To select the Ground CT type, modify the s2 SYSTEM SETUP \triangleright CURRENT SENSING $\triangleright \nabla$ GROUND CT setpoint as shown below.

Press the MENU key until the relay displays the setpoints menu header.

BEEN STORED



Press the VALUE keys until "1 A Secondary" is displayed.

1 A Secondary

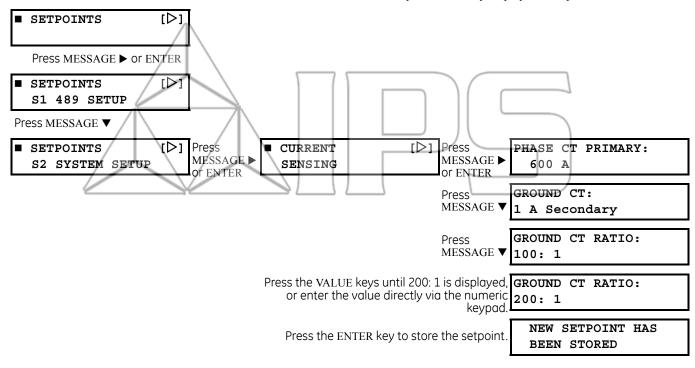
Press the ENTER key to store the setpoint.

NEW SETPOINT HAS BEEN STORED

store.ips.us

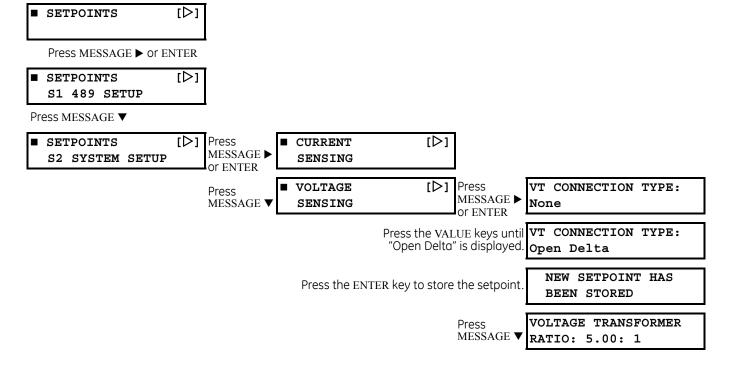
To set the ground CT ratio, modify the S2 SYSTEM SETUP \triangleright CURRENT SENSING $\triangleright \nabla$ GROUND CT RATIO setpoint as shown below.

Press the MENU key until the relay displays the setpoints menu header.



To set the VT connection type and ratings, modify the **S2 SYSTEM SETUP** $\triangleright \nabla$ **VOLTAGE SENSING** $\triangleright \nabla$ **VT CONNECTION TYPE** and the **S2 SYSTEM SETUP** $\triangleright \nabla$ **VOLTAGE SENSING** $\triangleright \nabla$ **VOLTAGE TRANSFORMER RATIO** Setpoints as shown below.

Press the MENU key until the relay displays the setpoints menu header.



Press the VALUE keys until 115.00: 1 is displayed, or enter the value directly via the numeric keypad.

Press the ENTER key to store the setpoint.

Press the ENTER key to store the setpoint.

NEW SETPOINT HAS BEEN STORED

If an entered setpoint value is out of range, the relay displays a message with the following format:

OUT-OF-RANGE! ENTER:
1-300:1" indicates the range and "0.01:1" indicates the step value

In this case, 1 is the minimum setpoint value, 300 is the maximum, and 0.01 is the step value. To have access to information on maximum, minimum, and step value, press the

1.3.5 Output Relay Setpoints

HELP key.

The output relays 1 Trip and 5 Alarm can be associated to auxiliary relays 2 to 4. Each can be selected individually, or in combination, in response to customer specific requirements. These relays are initiated through the ASSIGN ALARM RELAYS OF ASSIGN TRIP RELAYS setpoints specific to a protection element or function.

Select the S6 VOLTAGE ELEMENTS ▷ UNDERVOLTAGE ▷ ♡ ASSIGN TRIP RELAYS (1-4) setpoint message.

ASSIGN TRIP
RELAYS (1-4): 1---

If an application requires the undervoltage protection element to trip the 3 Auxiliary relay,

Select this output relay by pressing the "3" key; pressing the "3" key again disables the 3 Auxiliary relay.
 Enable/disable relays 1, 3, and 4 in the same manner until the desired combination appear in the display.

ASSIGN TRIP RELAYS (1-4): --3-

Press the ENTER key to store this change into memory. As before, confirmation of this action will momentarily flash on the display.

> NEW SETPOINT HAS BEEN STORED

1.3.6 Text Setpoints

Text setpoints have data values, which are fixed in length, but user defined in character. They may be comprised of uppercase letters, lowercase letters, numerals, and a selection of special characters. The editing and storing of a text value is accomplished with the use of the decimal [.], VALUE, and ENTER keys.

For example:

Nove to the S3 DIGITAL INPUTS > GENERAL INPUT A > V INPUT NAME message:

INPUT NAME: Input A

The name of this user-defined input will be changed in this example from the generic "Input A" to something more descriptive.

If an application is to be using the relay as a station monitor, it is more informative to rename this input "Stn. Monitor".

▶ Press the decimal [.] key to enter the text editing mode. The first character will appear underlined as follows:

INPUT NAME: Input A

- Press the VALUE keys until the character "S" is displayed in the first position.
- Press the decimal [.] key to store the character and advance the cursor to the next position.
- Change the second character to a "t" in the same manner.
- Continue entering characters in this way until all characters of the text "Stn. Monitor" are entered.

 Note that a space is selected like a character. If a character is entered incorrectly, press the decimal [.] key repeatedly until the cursor returns to the position of the error. Re-enter the character as required.
- Once complete, press the ENTER key to remove the solid cursor and view the result.

Once a character is entered, by pressing the ENTER key, it is automatically saved in flash memory, as a new setpoint.

INPUT NAME: Stn. Monitor

1.4 Installation

1.4.1 Placing the Relay in Service

The relay is defaulted to the Not Ready state when it leaves the factory. A minor self-test warning message informs the user that the 489 Generator Management Relay has not yet been programmed. If this warning is ignored, protection will be active using factory default setpoints and the Relay In Service LED Indicator will be on.

1.4.2 Testing

Extensive commissioning tests are available in Chapter 7. Tables for recording required settings are available in Microsoft Excel format from the GE Multilin website at http://www.GEmultilin.com. The website also contains additional technical papers and FAQs relevant to the 489 Generator Management Relay.







2.1 Overview

2.1.1 Description

The 489 Generator Management Relay is a microprocessor-based relay designed for the protection and management of synchronous and induction generators. The 489 is equipped with 6 output relays for trips and alarms. Generator protection, fault diagnostics, power metering, and RTU functions are integrated into one economical drawout package. The single line diagram illustrates the 489 functionality using ANSI (American National Standards Institute) device numbers.

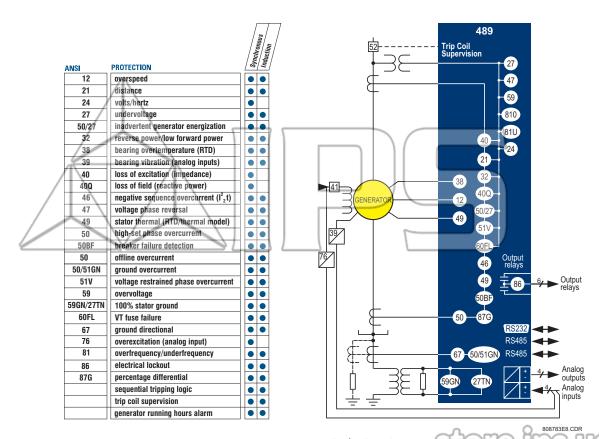


FIGURE 2-1: Single Line Diagram

Fault diagnostics are provided through pretrip data, event record, waveform capture, and statistics. Prior to issuing a trip, the 489 takes a snapshot of the measured parameters and stores them in a record with the cause of the trip. This pre-trip data may be viewed using the NEXT key before the trip is reset, or by accessing the last trip data in actual values page 1. The event recorder stores a maximum of 256 time and date stamped events including the pre-trip data. Every time a trip occurs, the 489 stores a 16 cycle trace for all measured AC quantities. Trip counters record the number of occurrences of each type of trip. Minimum and maximum values for RTDs and analog inputs are also recorded. These features allow the operator to pinpoint a problem quickly and with certainty.

A complete list protection features is shown below:

Table 2–1: Trip and Alarm Protection Features

	Trip Protection	Alarm Protection
1	Seven (7) Assignable Digital Inputs: General Input, Sequential Trip (low forward power or reverse power), Field- Breaker discrepancy, and Tachometer	7 assignable digital inputs: general input and tachometer
ı	forward power or reverse power), Field-	Overload
$\hat{}$	Breaker discrepancy, and Tachometer	Negative Sequence
	Offline Overcurrent (protection during startup)	Ground Overcurrent
	Inadvertent Energization	Ground Directional
	Phase Overcurrent with Voltage Restraint	Undervoltage
¥	Negative-Sequence Overcurrent	Overvoltage
	Ground Overcurrent	Volts Per Hertz
	Percentage Phase Differential	Underfrequency
	Ground Directional	Overfrequency
	High-Set Phase Overcurrent	Neutral Overvoltage (Fundamental)
	Undervoltage	Neutral Undervoltage (3rd Harmonic)
	Overvoltage	Reactive Power (kvar)
	Volts Per Hertz	Reverse Power
	Voltage Phase Reversal	Low Forward Power
	Underfrequency (two step)	RTD: Stator, Bearing, Ambient, Other
	Overfrequency (two step)	Short/Low RTD
	Neutral Overvoltage (Fundamental)	Open RTD
	Neutral Undervoltage (3rd Harmonic)	Thermal Overload
	Loss of Excitation (2 impedance circles)	Trip Counter
	Distance Element (2 zones of protection)	Breaker Failure
	Reactive Power (kvar) for loss of field	Trip Coil Monitor
	Reverse Power for anti-motoring	VT Fuse Failure
	Low Forward Power	Demand: Current, MW, Mvar, MVA
	RTDs: Stator, Bearing, Ambient, Other	Generator Running Hours
	Thermal Overload	Analog Inputs 1 to 4
	Analog Inputs 1 to 4	Service (Self-Test Failure)
	Electrical Lockout	IRIG-B Failure
		ul 1



The following protection elements require neutral-end current inputs.

- Distance Element
- Offline Overcurrent
- Phase Differential

Power metering is a standard feature in the 489. The table below outlines the metered parameters available to the operator through the front panel and communications ports. The 489 is equipped with three independent communications ports. The front panel RS232 port may be used for setpoint programming, local interrogation or control, and firmware upgrades. The computer RS485 port may be connected to a PLC, DCS, or PC based interface software. The auxiliary RS485 port may be used for redundancy or simultaneous interrogation and/or control from a second PLC, DCS, or PC program. There are also four 4 to 20 mA transducer outputs that may be assigned to any measured parameter. The range of these outputs is scalable. Additional features are outlined below.

Table 2-2: Metering and Additional Features

Metering	
Voltage (phasors)	Drawout C
Current (phasors) and Amps Demand	Breaker Fa
Real Power, MW Demand, MWh	Trip Coil Su
Apparent Power and MVA demand	VT Fuse Fa
MW, Mvar, and ±MVarh demand	Simulation
Frequency	Flash Mem upgrades
Power Factor	
RTD	
Speed in RPM with a Key Phasor Input	
User-Programmable Analog Inputs	

Additional Features		
Drawout Case (maintenance and testing)		
Breaker Failure		
Trip Coil Supervision		
VT Fuse Failure		
Simulation		
Flash Memory for easy firmware upgrades		



2.1.2 Ordering

All features of the 489 are standard, there are no options. The phase CT secondaries, control power, and analog output range must be specified at the time of order. There are two ground CT inputs: one for a 50:0.025 CT and one for a ground CT with a 1 A secondary (may also accommodate a 5 A secondary). The VT inputs accommodate VTs in either a delta or wye configuration. The output relays are always non-failsafe with the exception of the service relay. The EnerVista 489 Setup software is provided with each unit. A metal demo case may be ordered for demonstration or testing purposes.

489 Base unit 489 Generator Management Relay 489 1 A phase CT secondaries Ρ1 Phase current inputs P5 5 A phase CT secondaries 20 to 60 V DC; LO 20 to 48 V AC at 48 to 62 Hz Control power 90 to 300 V DC; HI. 70 to 265 V AC at 48 to 62 Hz 0 to 1 mA analog outputs Α1 **Analog outputs** A20 4 to 20 mA analog outputs Basic display Enhanced display, larger LCD Display Ε Enhanced with Ethernet (10Base-T) Т Harsh (chemical) environment conformal Harsh environment Н coating

Table 2-3: 489 Order Codes

For example, the 489-P1-LO-A20-E code specifies a 489 Generator Management Relay with 1 A CT inputs, 25 to 60 V DC or 20 to 48 V AC control voltage, 4 to 20 mA analog outputs, and an enhanced display.

2.1.3 Other Accessories

Additional 489 accessories are listed below.

- EnerVista 489 Setup software: no-charge software provided with the 489
- SR 19-1 PANEL: single cutout for 19" panel
- SR 19-2 PANEL: double cutout for 19" panel
- **SCI MODULE:** RS232 to RS485 converter box, designed for harsh industrial environments
- Phase CT: 50, 75, 100, 150, 200, 250, 300, 350, 400, 500, 600, 750, 1000 phase CT primaries
- **HGF3, HGF5, HGF8:** For sensitive ground detection on high resistance grounded systems
- **489 1 3/8-inch Collar:** For shallow switchgear, reduces the depth of the relay by 1 3/8 inches
- **489 3-inch Collar:** For shallow switchgear, reduces the depth of the relay by 3 inches

2.2 Specifications

2.2.1 Inputs

ANALOG CURRENT INPUTS

Accuracy:.....±1% of full scale
Type:......Passive

Analog input supply:+24 V DC at 100 mA max. Sampling Interval:50 ms

ANALOG INPUTS FREQUENCY TRACKING

Frequency tracking: Va for wye, Vab for open delta; 6 V minimum, 10 Hz/s

DIGITAL INPUTS

Inputs: 9 opto-isolated inputs

External switch: dry contact $< 400 \Omega$, or open collector NPN transistor from

sensor. 6 mA sinking from internal 4K pull-up at 24 V DC with

Vce < 4 V DC

489 sensor supply: 24 V DC at 20 mA max.

GROUND CURRENT INPUT

CT primary: 10 to 10000 A (1 A / 5 A CTs)

CT secondary:1 A / 5 A or 50:0.025 (HGF CTs)

Conversion range: $0.02 \text{ to } 20 \times \text{CT for } 1\text{A}/5\text{A CTs}$

0.0 to 100 A primary for 50:0.025 CTs (HGF)

50:0.025 CT accuracy: $\pm 0.1 \text{ A}$ at < 10 A

 $\pm 1.0 \text{ A at} \ge 10 \text{ to } 100 \text{ A}$

1 A / 5 A CT accuracy: at $< 2 \times CT$: $\pm 0.5\%$ of $2 \times CT$

at \geq 2 × CT: ±1% of 20 × CT

GROUND CT BURDEN

Ground CT	Input	Burden	
		VA	Ω
	1 A	0.024	0.024
1A/5A	5 A	0.605	0.024
	20 A	9.809	0.024
	0.025 A	0.057	90.7
50:0.025 HGF	0.1 A	0.634	90.7
	0.5 A	18.9	75.6

GROUND CT CURRENT WITHSTAND (SECONDARY)

Ground CT	Withstand Time		
	1 sec.	2 sec.	continuo us
1A/5A	80 × CT	40 × CT	3×CT
50:0.025 HGF	N/A	N/A	150 mA

NEUTRAL VOLTAGE INPUT

VT ratio: 1.00 to 240.00:1 in steps of 0.01

VT secondary: 100 V AC (full-scale)
Conversion range: 0.005 to 1.00 × Full Scale

.Fundamental:+/-0.5% of Full Scale Accuracy:

3rd Harmonic at >3V secondary: +/-5% of reading

3rd Harmonic at < 3V secondary: +/- 0.15% of full scale

Max. continuous: 280 V AC

OUTPUT AND NEUTRAL END CURRENT INPUTS

CT primary: 10 to 50000 A

1 A or 5 A (specify with order) CT secondary:

Conversion range: 0.02 to $20 \times CT$

at $< 2 \times CT$: $\pm 0.5\%$ of $2 \times CT$ Accuracy:

at \geq 2 × CT: ±1% of 20 × CT Less than 0.2 VA at rated load Burden:

1 s at $80 \times \text{rated}$ current CT withstand: 2 s at $40 \times \text{rated current}$

continuous at $3 \times \text{rated current}$

PHASE VOLTAGE INPUTS

VT ratio: 1.00 to 300.00:1 in steps of 0.01

200 V AC (full-scale) VT secondary: Conversion range: 0.02 to $1.00 \times \text{full-scale}$ ±0.5% of full-scale Accuracy:

Max. continuous: 280 V AC Burden: $> 500 \text{ K}\Omega$

RTD INPUTS

100 Ω Platinum (DIN.43760) RTDs (3-wire type):

100 Ω Nickel, 120 Ω Nickel,

 10Ω Copper

RTD sensing current: 5 mA

Isolation: 36 Vpk (isolated with analog inputs and outputs)

-50 to +250°C Range:

Accuracy: ±2°C/±4°F for Pt and Ni

±5°C/±9°F for Cu

Lead resistance: 25 Ω max. per lead (Pt and Ni types); 3 Ω max. per lead (Cu type)

NO sensor: $>1 k\Omega$ Short/low alarm: <-50°C

2.2.2 **Outputs**

ANALOG CURRENT OUTPUT

Type: Active

Range: 4 to 20mA, 0 to 1 mA

(must be specified with order)

±1% of full scale Accuracy:

4 to 20 mA max. load: $1.2 \text{ k}\Omega$ 0 to 1 mA max. load: $10 \text{ k}\Omega$

Isolation: 36 Vpk (isolated with RTDs and analog inputs)

4 assignable outputs: phase A, B, C output current, three-phase average current,

> negative sequence current, generator load, hottest stator RTD, hottest bearing RTD, RTDs 1 to 12, voltage (AB, BC, and CA), average phase-phase voltage, volts/hertz, frequency, third harmonic neutral voltage, power (3-phase Mvar, MW, and MVA),

power factor, analog inputs 1 to 4, tachometer, thermal capacity used, demand (I, Mvar, MW, and MVA), torque

PULSE OUTPUT

Parameters: + kwh, +kvarh, -kvarh
Interval: 1 to 50000 in steps of 1
Pulse width: 200 to 1000 ms in steps of 1

RELAYS

WARNING

Relay contacts must be considered unsafe to touch when the relay is energized! If the output relay contacts are required for low voltage accessible applications, it is the customer's responsibility to ensure proper insulation levels.

Configuration: 6 electromechanical Form-C relays

Contact material: silver alloy
Operate time: 10 ms
Make/carry: 30 A for 0.2 s,

10 A continuous (for 100000 operations)

Maximum ratings for 100000 operations:

Voltage		Break	Max. Load
DC Resistive	30 V	10 A	300 W
	125 V	0.5 A	62.5 W
	250 V	0.3 A	75 W
DC inductive L/R = 40 ms	30 V	5 A	150 W
	125 V	0.25 A	31.3 W
	250 V	0.15 A	37.5 W
AC Resistive	120 V	10 A	2770 VA
	250 V	10 A	2770 VA
AC Inductive PF = 0.4	120 V	4 A	480 VA
	250 V	3 A	750 VA

2.2.3 Protection

PHASE DISTANCE (IMPEDANCE)

Characteristics: offset mho

Reach (secondary Ω): 0.1 to 500.0 Ω in steps of 0.1

Reach accuracy: $\pm 5\%$

Characteristic angle: $50 \text{ to } 85^{\circ} \text{ in steps of } 1$ Time delay: 0.15 to 150.0 s in steps of 0.1Timing accuracy: $\pm 50 \text{ ms or } \pm 0.5\% \text{ of total time}$

Number of zones: 2

GROUND DIRECTIONAL

Pickup level: 0.05 to $20.00 \times CT$ in steps of 0.01 Time delay: 0.1 to 120.0 s in steps of 0.1 Pickup accuracy: as per phase current inputs ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

GROUND OVERCURRENT

Pickup level: 0.05 to 20.00 × CT in steps of 0.01
Curve shapes: ANSI, IEC, IAC, Flexcurve, Definite Time
Time delay: 0.00 to 100.00 s in steps of 0.01
Pickup accuracy: as per ground current input

Timing accuracy: +50 ms at 50/60 Hz or $\pm 0.5\%$ total time

Elements: Trip

HIGH-SET PHASE OVERCURRENT

Pickup level: 0.15 to $20.00 \times CT$ in steps of 0.01 Time delay: 0.00 to 100.00 s in steps of 0.01 Pickup accuracy: as per phase current inputs

Timing accuracy: ± 50 ms at 50/60 Hz or $\pm 0.5\%$ total time

Elements: Trip

INADVERTENT ENERGIZATION

Arming signal: undervoltage and/or offline from breaker status

Pickup level: 0.05 to 3.00 × CT in steps of 0.01 of any one phase

Time delay: no intentional delay
Pickup accuracy: as per phase current inputs
Timing accuracy: +50 ms at 50/60 Hz

Elements: Trip

LOSS OF EXCITATION (IMPEDANCE)

Pickup level: 2.5 to 300.0 Ω secondary in steps of 0.1 with adjustable

impedance offset 1.0 to 300.0 Ω secondary in steps of 0.1

Time delay: 0.1 to 10.0 s in steps of 0.1

Pickup accuracy: as per voltage and phase current inputs

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time Elements: Trip (2 zones using impedance circles)

NEGATIVE SEQUENCE OVERCURRENT

Pickup level: 3 to 100% FLA in steps of 1

Curve shapes: I_2^2 t trip defined by k, definite time alarm

Time delay: 0.1 to 100.0 s in steps of 0.1

Pickup accuracy: as per phase current inputs

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

NEUTRAL OVERVOLTAGE (FUNDAMENTAL)

Pickup level: 2.0 to 100.0 V secondary in steps of 0.01

Time delay: 0.1 to 120.0 s in steps of 0.1

Pickup accuracy: as per neutral voltage input

±100 ms or ±0.5% of total time

Elements: Trip and Alarm

NEUTRAL UNDERVOLTAGE

(3RD HARMONIC)

Blocking signals: low power and low voltage if open delta

Pickup level: 0.5 to 20.0 V secondary in steps of 0.01 if open delta VT;

adaptive if wye VT

Time delay: 5 to 120 s in steps of 1
Pickup accuracy: as per Neutral Voltage Input

Timing accuracy: $\pm 3.0 \text{ s}$

Elements: Trip and Alarm

OFFLINE OVERCURRENT

Pickup level: $0.05 \text{ to } 1.00 \times \text{CT}$ in steps of 0.01 of any one phase

Time delay: 3 to 99 cycles in steps of 1
Pickup accuracy: as per phase current inputs

Timing accuracy: +50ms at 50/60 Hz

Elements: Trip

OTHER FEATURES

Serial Start/Stop Initiation, Remote Reset (configurable digital input), Test Input

(configurable digital input), Thermal Reset (configurable digital input), Dual Setpoints, Pre-Trip Data, Event Recorder, Waveform Memory, Fault Simulation, VT Failure, Trip Counter, Breaker Failure, Trip Coil Monitor, Generator Running Hours Alarm, IRIG-

B Failure Alarm

OVERCURRENT ALARM

Pickup level: 0.10 to $1.50 \times FLA$ in steps of 0.01 (average phase current) Time delay: 0.1 to 250.0 s in steps of 0.1

Pickup accuracy: as per phase current inputs Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Alarm

OVERFREQUENCY Required voltage: 0.50 to $0.99 \times \text{rated voltage in Phase A}$

Block from online: 0 to 5 sec. in steps of 1 Pickup level: 25.01 to 70.00 in steps of 0.01 Curve shapes: 1 level alarm, 2 level trip definite time

0.1 to 5000.0 s in steps of 0.1 Time delay:

Pickup accuracy: ±0.02 Hz

 ± 150 ms or $\pm 1\%$ of total time at 50Hz and 60Hz: ± 300 ms or 2% Timing accuracy:

of total time at 25Hz

Elements: Trip and Alarm

OVERLOAD / STALL PROTECTION / THERMAL MODEL

Overload curves:

15 Standard Overload Curves, Custom Curve, and Voltage

Dependent Custom Curve (all curves time out against average

phase current)

Phase Unbalance, Hot/Cold Curve Ratio, Stator RTD, Online Curve biasing:

Cooling Rate, Offline Cooling Rate, Line Voltage

Overload pickup: 1.01 to 1.25

Pickup accuracy: as per phase current inputs Timing accuracy: ± 100 ms or $\pm 2\%$ of total time

Elements: Trip and Alarm

OVERVOLTAGE

Pickup level: 1.01 to $1.50 \times \text{rated V}$ in steps of 0.01 Curve shapes: Inverse Time, definite time alarm Time Delay: 0.2 to 120.0 s in steps of 0.1 Pickup accuracy: as per Voltage Inputs

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

PHASE DIFFERENTIAL

0.05 to $1.00 \times CT$ in steps of 0.01Pickup level:

Curve shape: **Dual Slope**

Time delay: 0 to 100 cycles in steps of 1 Pickup accuracy: as per phase current inputs

+50 ms at 50/60 Hz or $\pm 0.5\%$ total time Timing accuracy:

Elements: Trip

PHASE OVERCURRENT

programmable fixed characteristic Voltage restraint:

Pickup level: 0.15 to $20.00 \times CT$ in steps of 0.01 of any one phase

Curve shapes: ANSI, IEC, IAC, FlexCurve, Definite Time Time delay: 0.000 to 100.000 s in steps of 0.001

Pickup accuracy: as per phase current inputs

Timing accuracy: +50 ms at 50/60 Hz or $\pm 0.5\%$ total time

Elements: Trip

RTDS 1 TO 12

Pickup: 1 to 250°C in steps of 1

Pickup hysteresis: 2°C Time delay: 3 sec.

Elements: Trip and Alarm

UNDERFREQUENCY

Required voltage: 0.50 to 0.99 × rated voltage in Phase A

Block from online: 0 to 5 sec. in steps of 1

Pickup level: 20.00 to 60.00 in steps of 0.01

Curve shapes: 1 level alarm, two level trip definite time

Time delay: 0.1 to 5000.0 sec. in steps of 0.1

Pickup accuracy: $\pm 0.02 \text{ Hz}$

Timing accuracy: ± 150 ms or $\pm 1\%$ of total time at 50Hz and 60Hz; ± 300 ms or 2%

of total time at 25Hz

Elements: Trip and Alarm

UNDERVOLTAGE

Pickup level: $0.50 \text{ to } 0.99 \times \text{rated V in steps of } 0.01$ Curve shapes: Inverse Time, definite time alarm Time Delay: 0.2 to 120.0 s in steps of 0.1

Pickup accuracy: as per voltage inputs

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

VOLTAGE PHASE REVERSAL

Configuration: ABC or ACB phase rotation

Timing accuracy: 200 to 400 ms

Elements: Trip

VOLTS PER HERTZ

Pickup level: 1.00 to $1.99 \times$ nominal in steps of 0.01 Curve shapes: Inverse Time, definite time alarm Time delay: 0.1 to 120.0 s in steps of 0.1 as per voltage inputs Timing accuracy: $\pm 100 \text{ ms at} \geq 1.2 \times \text{Pickup}$

 ± 100 ms at $\geq 1.2 \times$ Pickup ± 300 ms at $< 1.2 \times$ Pickup

Elements: Trip and Alarm

2.2.4 Digital Inputs

FIELD BREAKER DISCREPANCY

Configurable: assignable to Digital Inputs 1 to 7
Time delay: 0.1 to 500.0 s in steps of 0.1
Timing accuracy: ±100 ms or ±0.5% of total time

Elements: Trip

GENERAL INPUT A TO G

 $\begin{array}{lll} \mbox{Configurable:} & \mbox{ssignable Digital Inputs 1 to 7} \\ \mbox{Time delay:} & 0.1 to 5000.0 s in steps of 0.1 \\ \mbox{Block from online:} & 0 to 5000 s in steps of 1 \\ \mbox{Timing accuracy:} & \pm 100 \mbox{ ms or } \pm 0.5\% \mbox{ of total time} \\ \end{array}$

Elements: Trip, Alarm, and Control

SEQUENTIAL TRIP

Pickup level:

Time delay:
Pickup accuracy:

Configurable: assignable to Digital Inputs 1 to 7

0.02 to $0.99 \times \text{rated MW}$ in steps of 0.01, Low Forward Power /

Reverse Power

0.2 to 120.0 s in steps of 0.1

see power metering

 ± 100 ms or $\pm 0.5\%$ of total time

Trip

TACHOMETER

Elements:

Timing accuracy:

Configurable: assignable to Digital Inputs 4 to 7

RPM measurement: 0 to 7200 RPM

Duty cycle of pulse: >10%

Pickup level: $101 \text{ to } 175 \times \text{rated speed in steps of } 1$

Time delay: 1 to 250 s in steps of 1 Timing accuracy: ± 0.5 s or ± 0.5 % of total time

Elements: Trip and Alarm

2.2.5 Monitoring

DEMAND METERING

Metered values: maximum phase current,

3 phase real power,3 phase apparent power,3 phase reactive power

Measurement type: rolling demand

Demand interval: 5 to 90 min. in steps of 1

Update rate: 1 minute Elements: Alarm

ENERGY METERING

Description: continuous total of +watthours and ±varhours

Range: 0.000 to 4000000.000 Mvarh

Timing accuracy: $\pm 0.5\%$ Update Rate: $\pm 0.5\%$

LOW FORWARD POWER

Block from online: 0 to 15000 s in steps of 1 Pickup level: 0.02 to $0.99 \times \text{rated MW}$ Time delay: 0.2 to 120.0 s in steps of 0.1

Pickup accuracy: see power metering

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

POWER METERING

Range: -2000.000 to 2000.000 MW,

-2000.000 to 2000.000 Mvar.

0 to 2000.000 MVA

Accuracy at I_{avg} < 2 × CT: ±1% of $\sqrt{3}$ × 2 × CT × VT_{ratio} × VT_{full-scale} Accuracy at I_{avg} > 2 × CT: ±1.5% of $\sqrt{3}$ × 20 × CT × VT_{ratio} × VT_{full-scale}

REACTIVE POWER

Block from online: 0 to 5000 s in steps of 1

Pickup level: $0.02 \text{ to } 1.50 \times \text{rated Mvar}$

(positive and negative)
Time delay: 0.2 to 120.0 s in steps of 0.1

Pickup accuracy: see power metering
Timing accuracy: ±100ms or ±0.5% of total time

Elements: Trip and Alarm

REVERSE POWER

Block from online: 0 to 5000 s in steps of 1
Pickup level: 0.02 to $0.99 \times \text{rated MW}$ Time delay: 0.2 to 120.0 s in steps of 0.1

Pickup accuracy: see power metering

Timing accuracy: ± 100 ms or $\pm 0.5\%$ of total time

Elements: Trip and Alarm

TRIP COIL SUPERVISION

Applicable voltage: 20 to 300 V DC/AC

Trickle current: 2 to 5 mA

2.2.6 Power Supply

CONTROL POWER

Options: LO / HI (specify with order)

LO range: 20 to 60 V DC

20 to 48 V AC at 48 to 62 Hz

HI range: 90 to 300 V DC

70 to 265 V AC at 48 to 62 Hz

Power: 45 VA (max.), 25 VA typical

Total loss of voltage ride through time (0% control power): 16.7 ms



It is recommended that the 489 be powered up at least once per year to prevent deterioration of electrolytic capacitors in the power supply.

FUSE

Current rating: 2.5 A

Type: 5x20mm HRC SLO-BLO Littelfuse

Model: 215-02.5



An external fuse must be used if the supply voltage exceeds 250 V

2.2.7 Communications

COMMUNICATIONS PORTS

RS232 port: 1, front panel, non-isolated RS485 ports: 2, isolated together at 36 Vpk RS485 baud rates: 300, 1200, 2400, 4800, 9600, 19200

RS232 baud rate: 9600

Parity: None, Odd, Even

Protocol: Modbus[®] RTU / half duplex, DNP 3.0

2.2.8 Testing

PRODUCTION TESTS

Thermal cycling:

Dielectric strength:

Operational test at ambient, reducing to –40°C and then

increasing to 60°C

1.9 kV AC for 1 second or 1.6 kV AC for one minute, per UL 508.



DO NOT CONNECT FILTER GROUND TO SAFETY GROUND DURING ANY PRODUCTION TESTS!

TYPE TESTING

The table below lists the 489 type tests:

Standard	Test Name	Level
EIA 485	RS485 Communications Test	32 units at 4000 ft.
GE Multilin	Temperature Cycling	-50°C / +80°C
IEC 60068-2-38	Composite Temperature/Humidity	65/-10°C at 93% RH
IEC 60255-5	Dielectric Strength	2300 V AC
IEC 60255-5	Impulse Voltage	5 kV
IEC 60255-5	Insulation Resistance	>100 MΩ / 500 V AC / 10 s
IEC 60255-21-1	Sinusoidal Vibration	2 g
IEC 60255-22-2	Electrostatic Discharge: Direct	8 kV
IEC 60255-22-3	Radiated RF Immunity	10 V/m
IEC 60255-22-4	Electrical Fast Transient / Burst Immunity	4 kV
IEC 60255-22-5	Surge Immunity	4 kV / 2 kV
IEC 60255-22-6	Conducted RF Immunity, 150 kHz to 80 MHz	10 V/m
IEC 60255-25	Radiated RF Emission	Group 1 Class A
IEC 60255-25	Conducted RF Emission	Group 1 Class A
IEC 60529	Ingress of Solid Objects and Water (IP)	IP40 (front), IP20 (back)
IEC 61000-4-8	Power frequency magnetic field immunity	30 A/m
IEC 61000-4-11	Voltage Dip; Voltage Interruption	0%, 40%, 100%
IEEE C37.90	Make and carry	30 A DC
IEEE C37.90.1	Fast Transient SWC	±4 kV
IEEE C37.90.1	Oscillatory Transient SWC	±2.5 kV

2.2.9 Certification

CERTIFICATION IEC 1010-1:

IEC 1010-1: LVD - CE for Europe
EN 50263: EMC - CE for Europe
ACA Tick Mark: RF emissions for Australia
FCC part 15: RF emissions for North America
UL: listed E83849

registered

Seal provision

Dust tight door

IP20-X

Panel or 19" rack mount

 $12" \times 11" \times 10" (W \times H \times D)$

30.5cm $\times 27.9$ cm $\times 25.4$ cm

17 lbs / 7.7 kg max.

Fully drawout (automatic CT shorts)

ISO 9001:

2.2.10 Physical

CASE

Drawout: Seal: Door:

Mounting:

IP Class: PACKAGING

Shipping box:

Shipping weight:

Low voltage (A, B, C, D terminals): 12 AWG max

TERMINALS

High voltage (E, F, G, H terminals): #8 ring lug, 10 AWG wire standard

2.2.11 Environmental

ENVIRONMENTAL

Ambient operating temperature:-40°C to +60°C Ambient storage temperature:40°C to +80°C

Humidity: up to 90%, non-condensing

Altitude: up to 2000 m

Pollution degree: 2



At temperatures less than -20°C, the LCD contrast may be impaired.



2.2.12 Long-term Storage

LONG-TERM STORAGE

Environment:

Correct storage:

In addition to the above environmental considerations, the relay should be stored in an environment that is dry, corrosive-free, and not in direct sunlight.

Prevents premature component failures caused by environmental factors such as moisture or corrosive gases. Exposure to high humidity or corrosive environments will prematurely degrade the electronic components in any electronic device regardless of its use or manufacturer, unless specific precautions, such as those mentioned in the Environmental section above, are taken.

It is recommended that all relays be powered up once per year, for one hour continuously, to avoid deterioration of electrolytic capacitors and subsequent relay failure.







3.1 Mechanical Installation

3.1.1 Description

The 489 is packaged in the standard GE Multilin SR-series arrangement, which consists of a drawout unit and a companion fixed case. The case provides mechanical protection to the unit, and is used to make permanent connections to all external equipment. The only electrical components mounted in the case are those required to connect the unit to the external wiring. Connections in the case are fitted with mechanisms required to allow the safe removal of the relay unit from an energized panel, such as automatic CT shorting. The unit is mechanically held in the case by pins on the locking handle, which cannot be fully lowered to the locked position until the electrical connections are completely mated. Any 489 can be installed in any 489 case, except for custom manufactured units that are clearly identified as such on both case and unit, and are equipped with an index pin keying mechanism to prevent incorrect pairings.

No special ventilation requirements need to be observed during the installation of the unit, but the unit should be wiped clean with a damp cloth.

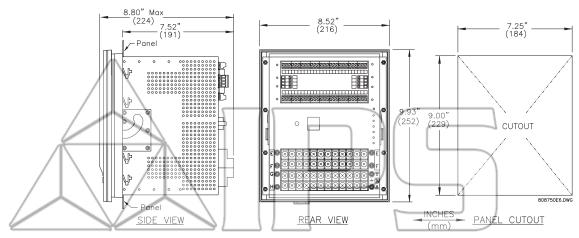


FIGURE 3-1: 489 Dimensions

To prevent unauthorized removal of the drawout unit, a wire lead seal can be installed in the slot provided on the handle as shown below. With this seal in place, the drawout unit cannot be removed. A passcode or setpoint access jumper can be used to prevent entry of setpoints but still allow monitoring of actual values. If access to the front panel controls must be restricted, a separate seal can be installed on the outside of the cover to prevent it from being opened.



FIGURE 3-2: Drawout Unit Seal



Hazard may result if the product is not used for its intended purpose.

3.1.2 Product Identification

Each 489 unit and case are equipped with a permanent label. This label is installed on the left side (when facing the front of the relay) of both unit and case. The case label details which units can be installed.

The case label details the model number, manufacture date, and special notes.

The unit label details the model number, type, serial number, file number, manufacture date, phase current inputs, special notes, overvoltage category, insulation voltage, pollution degree, control power, and output contact rating.



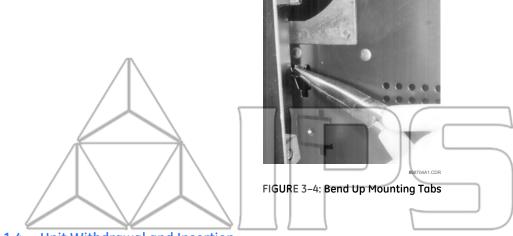
FIGURE 3-3: Product Case and Unit Labels

3.1.3 Installation



The 489 case, alone or adjacent to another SR-series unit, can be installed in a standard 19-inch rack panel (see 489 Dimensions on page 3–2). Provision must be made for the front door to swing open without interference to, or from, adjacent equipment. The 489 unit is normally mounted in its case when shipped from the factory and should be removed before mounting the case in the supporting panel. Unit withdrawal is described in the next section.

After the mounting hole in the panel has been prepared, slide the 489 case into the panel from the front. Applying firm pressure on the front to ensure the front bezel fits snugly against the front of the panel, bend out the pair of retaining tabs (to a horizontal position) from each side of the case, as shown below. The case is now securely mounted, ready for panel wiring.



3.1.4 Unit Withdrawal and Insertion



TURN OFF CONTROL POWER BEFORE DRAWING OUT OR RE-INSERTING THE RELAY TO PREVENT MALOPERATION!



If an attempt is made to install a unit into a non-matching case, the mechanical key will prevent full insertion of the unit. Do not apply strong force in the following step or damage may result.

To remove the unit from the case:

- Den the cover by pulling the upper or lower corner of the right side, which will rotate about the hinges on the left.
- Release the locking latch, located below the locking handle, by pressing upward on the latch with the tip of a screwdriver.



FIGURE 3-5: Press Latch to Disengage Handle

➢ Grasp the locking handle in the center and pull firmly, rotating the handle up from the bottom of the unit until movement ceases.



FIGURE 3-6: Rotate Handle to Stop Position

Once the handle is released from the locking mechanism, the unit can freely slide out of the case when pulled by the handle. It may sometimes be necessary to adjust the handle position slightly to free the unit.



FIGURE 3-7: Slide Unit out of Case

To insert the unit into the case:

- Raise the locking handle to the highest position.
- ➢ Hold the unit immediately in front of the case and align the rolling guide pins (near the hinges of the locking handle) to the guide slots on either side of the case.
- Slide the unit into the case until the guide pins on the unit have engaged the guide slots on either side of the case.
- □ Grasp the locking handle from the center and press down firmly, rotating the handle from the raised position toward the bottom of the unit.

When the unit is fully inserted, the latch will be heard to click, locking the handle in the final position.

3.1.5 Ethernet Connection

If using the 489 with the Ethernet 10Base-T option, ensure that the network cable is disconnected from the rear RJ45 connector before removing the unit from the case. This prevents any damage to the connector.

The unit may also be removed from the case with the network cable connector still attached to the rear RJ45 connector, provided that there is at least 16 inches of network cable available when removing the unit from the case. This extra length allows the network cable to be disconnected from the RJ45 connector from the front of the switchgear panel. Once disconnected, the cable can be left hanging safely outside the case for re-inserting the unit back into the case.

The unit may be re-inserted by first connecting the network cable to the rear RJ45 connector of the 489 (see step 3 of *Unit Withdrawal and Insertion* on page 3–4).



Ensure that the network cable does not get caught inside the case while sliding in the unit. This may interfere with proper insertion to the case terminal blocks and damage the cable.



FIGURE 3-8: Ethernet Cable Connection

To ensure optimal response from the relay, the typical connection timeout should be set as indicated in the following table:

TCP/IP sessions	Timeout setting
up to 2	2 seconds
up to 4	3 seconds



The RS485 COM2 port is disabled if the Ethernet option is ordered.

3.1.6 Terminal Locations

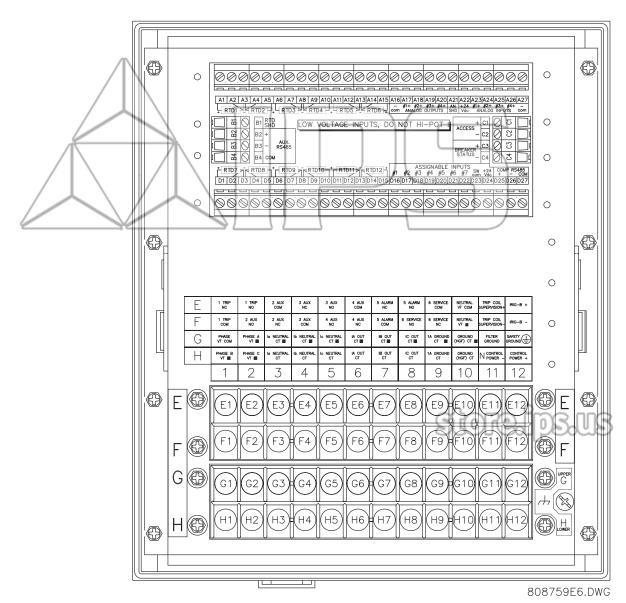


FIGURE 3-9: Terminal Layout

Table 3-1: 489 Terminal List

Terminal	Description	Terminal	Description
A01	RTD #1 Hot	D21	Assignable Switch 6
A02	RTD #1 Compensation	D22	Assignable Switch 7
A03	RTD Return	D23	Switch Common
A 0 4	RTD #2 Compensation	D24	Switch +24 V DC
A05	RTD #2 Hot	D25	Computer RS485 +
A06	RTD #3 Hot	D26	Computer RS485 -
A07	RTD #3 Compensation	D27	Computer RS485 Common
A08	RTD Return	E01	1 Trip NC
A09	RTD #4 Compensation	E02	1 Trip NO
A10	RTD #4 Hot	E03	2 Auxiliary Common
A11	RTD #5 Hot	E04	3 Auxiliary NC
A12	RTD #5 Compensation	E05	3 Auxiliary NO
A13	RTD Return	E06	4 Auxiliary Common
A14	RTD #6 Compensation	E07	5 Alarm NC
A15	RTD #6 Hot	E08	5 Alarm NO
A16	Analog Output Common –	E09	6 Service Common
A17	Analog Output 1 +	E10	Neutral VT Common
A18	Analog Output 2 +	E11	Coil Supervision +
A19	Analog Output 3 +	E12	IRIG-B +
A20	Analog Output 4 +	F01	1 Trip Common
A21	Analog Shield	F02	2 Auxiliary NO
A22	Analog Input 24 V DC Supply +	F03	2 Auxiliary NC
A23	Analog Input 1 +	F04	3 Auxiliary Common
A24	Analog Input 2 +	F05	4 Auxiliary NO
A25	Analog Input 3 +	F06	4 Auxiliary NC
A26	Analog Input 4 +	F07	5 Alarm Common
A27	Analog Input Common –	F08	6 Service NO
B01	RTD Shield	F09	6 Service NC
B02	Auxiliary RS485 +	F10	Neutral VT +
B03	Auxiliary RS485 –	F11	Coil Supervision –
B04	Auxiliary RS485 Common	F12	IRIG-B -
C01	Access +	G01	Phase VT Common
C02	Access -	G02	Phase A VT •
C03	Breaker Status +	G03	Neutral Phase A CT •
C04	Breaker Status -	G04	Neutral Phase B CT •
D01	RTD #7 Hot	G05	Neutral Phase C CT •
D02	RTD #7 Compensation	G06	Output Phase A CT •
D03	RTD Return	G07	Output Phase B CT •
D03	RTD #8 Compensation	G08	Output Phase C CT •
D04 D05	RTD #8 Hot	G09	1A Ground CT •
D05	RTD #9 Hot	G10	HGF Ground CT •
D07	RTD #9 Compensation	G11	Filter Ground
D07	RTD Return	G12	Safety Ground
D09	RTD #10 Compensation	H01	Phase B VT •
D10	RTD #10 Compensation	H02	Phase C VT •
D10 D11	RTD #10 HOT	H02	Neutral Phase A CT
D11 D12	RTD #11 HOT RTD #11 Compensation	H03	Neutral Phase B CT
D13	RTD Return	H05	Neutral Phase C CT
	RTD #12 Compensation		Output Phase A CT
D14	·	H06	•
D15	RTD #12 Hot	H07	Output Phase B CT
D16	Assignable Switch 1	H08	Output Phase C CT
D17	Assignable Switch 2	H09	1A Ground CT
D18	Assignable Switch 3	H10	HGF Ground CT
D19	Assignable Switch 4	H11	Control Power –
D20	Assignable Switch 5	H12	Control Power +

3.2 Electrical Installation

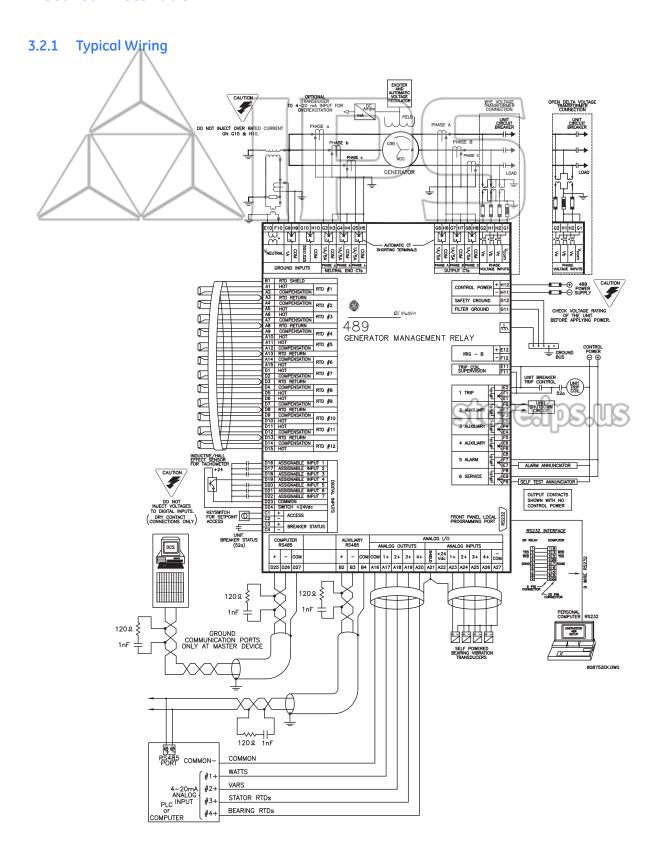


FIGURE 3-10: Typical Wiring Diagram

3.2.2 General Wiring Considerations

A broad range of applications are available to the user and it is not possible to present typical connections for all possible schemes. The information in this section will cover the important aspects of interconnections, in the general areas of instrument transformer inputs, other inputs, outputs, communications and grounding. See Terminal Layout on page 3-7 and 489 Terminal List on page 3-8 for terminal arrangement, and Typical Wiring Diagram on page 3-10 for typical connections. EXCITER AND AUTOMATIC VOLTAGE REGULATOR FIELD PHASE A PHASE a DO NOT INJECT OVER RATED CURRENT PHASE b PHASE B C(B) \ B(C) **GENERATOR** G9 H9 G10 H10 G3 H3 G4 H4 G5 H5 AUTOMATIC CT 1A/5A COM SHORTING TERMINALS COV COM COM _` GROUND INPUTS 808821A5.DWG

FIGURE 3-11: Typical Wiring (Detail)

3.2.3 Control Power



Control power supplied to the relay must match the installed power supply range. If the applied voltage does not match, damage to the unit may occur. All grounds MUST be connected for normal operation regardless of control power supply type.

The label found on the left side of the relay specifies its order code or model number. The installed power supply's operating range will be one of the following.

LO: 20 to 60 V DC or 20 to 48 V AC HI: 88 to 300 V DC or 70 to 265 V AC



The relay should be connected directly to the ground bus, using the shortest practical path. A tinned copper, braided, shielding and bonding cable should be used. As a minimum, 96 strands of number 34 AWG should be used. Belden catalog number 8660 is suitable.

Ensure applied control voltage and rated voltage on drawout case terminal label match. For example, the HI power supply will work with any DC voltage from 90 to 300 V, or AC voltage from 70 to 265 V. The internal fuse may blow if the applied voltage exceeds this range.

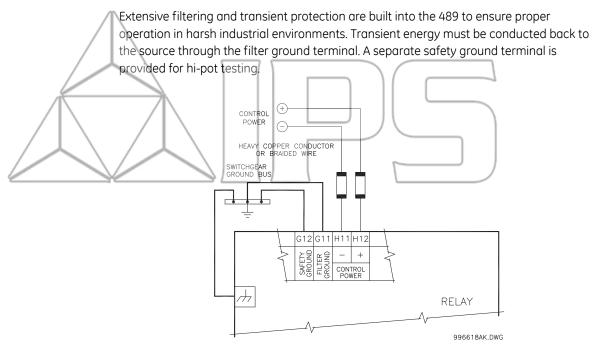


FIGURE 3-12: Control Power Connection

3.2.4 Current Inputs

Phase Current

The 489 has six phase current transformer inputs (three output side and three neutral end), each with an isolating transformer. There are no internal ground connections on the CT inputs. Each phase CT circuit is shorted by automatic mechanisms on the 489 case if the unit is withdrawn. The phase CTs should be chosen such that the FLA is no less than 50% of the rated phase CT primary. Ideally, the phase CT primary should be chosen such that the FLA is 100% of the phase CT primary or slightly less. This will ensure maximum accuracy for the current measurements. The maximum phase CT primary current is 50000 A.

The 489 will measure correctly up to 20 times the phase current nominal rating. Since the conversion range is large, 1 A or 5 A CT secondaries must be specified at the time of order such that the appropriate interposing CT may be installed in the unit. CTs chosen must be capable of driving the 489 phase CT burden (see SPECIFICATIONS for ratings).



Verify that the 489 nominal phase current of 1 A or 5 A matches the secondary rating and connections of the connected CTs. Unmatched CTs may result in equipment damage or inadequate protection. Polarity of the phase CTs is critical for phase differential, negative sequence, power measurement, and residual ground current detection (if used).

Ground Current

The 489 has a dual primary isolating transformer for ground CT connections. There are no internal ground connections on the ground current inputs. The ground CT circuits are shorted by automatic mechanisms on the case if the unit is withdrawn. The 1 A tap is used for 1 A or 5 A secondary CTs in either core balance or residual ground configurations. If the 1 A tap is used, the 489 measures up to 20 A secondary with a maximum ground CT ratio of 10000:1. The ground CT must be capable of driving the ground CT burden.

The HGF ground CT input is designed for sensitive ground current detection on high resistance grounded systems where the GE Multilin HGF core balance CT (50:0.025) is used. In applications such as mines, where earth leakage current must be measured for personnel safety, primary ground current as low as 0.25 A may be detected with the GE Multilin HGF CT. Only one ground CT input tap should be used on a given unit.

The HGF CT has a rating of 50:0.025. However if the HGF CT is used in conjunction with the 489, the relay assumes a fixed ratio of 5:0.0025. Therefore, the pickup level in primary amps will be Pickup \times CT, where CT is equal to 5.



Only one ground input should be wired. The other input should be unconnected.

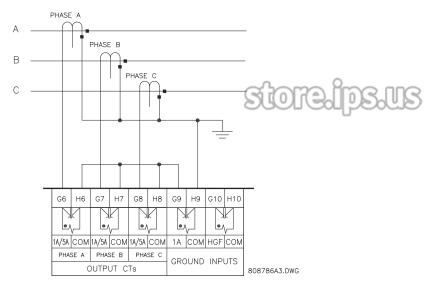


FIGURE 3-13: Residual Ground CT Connection



DO NOT INJECT OVER THE RATED CURRENT TO HGF TERMINAL (0.25 to 25 A PRIMARY).

The exact placement of a zero sequence CT to detect ground fault current is shown below. If the core balance CT is placed over shielded cable, capacitive coupling of phase current into the cable shield may be detected as ground current unless the shield wire is also passed through the CT window. Twisted pair cabling on the zero sequence CT is recommended.

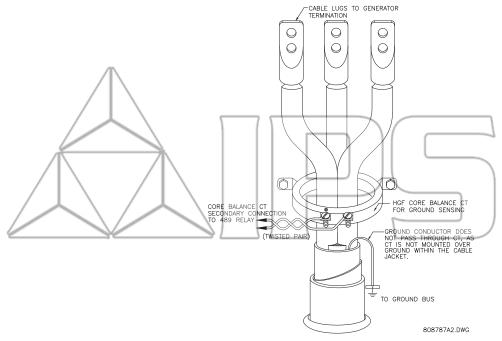


FIGURE 3-14: Core Balance Ground CT Installation - Unshielded Cable

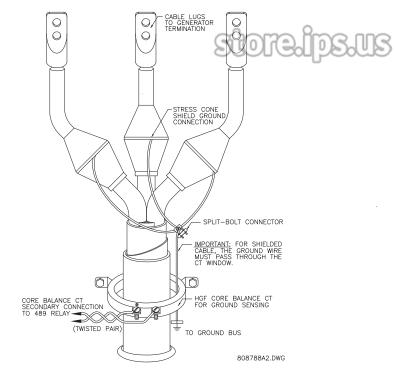


FIGURE 3-15: Core Balance Ground CT Installation - Shielded Cable

3.2.5 Voltage Inputs

The 489 has four voltage transformer inputs, three for generator terminal voltage and one for neutral voltage. There are no internal fuses or ground connections on the voltage inputs. The maximum phase VT ratio is 300.00:1 and the maximum neutral VT ratio is 240.00:1. The two possible VT connections for generator terminal voltage measurement are open delta or wye (see *Typical Wiring Diagram* on page 3–10). The voltage channels are connected in wye internally, which means that the jumper shown on the delta-source connection of the Typical Wiring Diagram, between the phase B input and the 489 neutral terminal, must be installed for open delta VTs.



Polarity of the generator terminal VTs is critical for correct power measurement and voltage phase reversal operation.

3.2.6 Digital Inputs



There are 9 digital inputs that are designed for dry contact connections only. Two of the digital inputs, Access and Breaker Status have their own common terminal, the balance of the digital inputs share one common terminal (see *Typical Wiring Diagram* on page 3–10).

In addition, the +24 V DC switch supply is brought out for control power of an inductive or capacitive proximity probe. The NPN transistor output could be taken to one of the assignable digital inputs configured as a counter or tachometer. Refer to the Specifications section of this manual for maximum current draw from the +24 V DC switch supply.



DO NOT INJECT VOLTAGES TO DIGITAL INPUTS. DRY CONTACT CONNECTIONS ONLY

3.2.7 Analog Inputs

Terminals are provided on the 489 for the input of four 0 to 1 mA, 0 to 20 mA, or 4 to 20 mA current signals (field programmable). This current signal can be used to monitor any external quantity such as: vibration, pressure, field current, etc. The four inputs share one common return. Polarity of these inputs must be observed for proper operation The analog input circuitry is isolated as a group with the Analog Output circuitry and the RTD circuitry. Only one ground reference should be used for the three circuits. Transorbs limit this isolation to ± 36 V with respect to the 489 safety ground.

In addition, the +24 V DC analog input supply is brought out for control power of loop powered transducers. Refer to the Specifications section of this manual for maximum current draw from this supply.

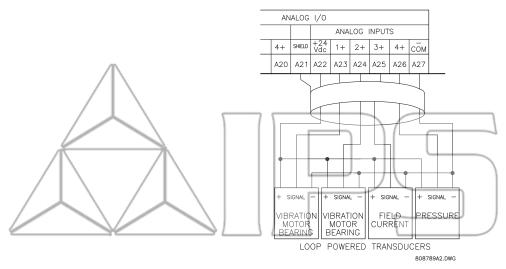


FIGURE 3-16: Loop Powered Transducer Connection

3.2.8 Analog Outputs

The 489 provides four analog output channels, which when ordered, provide a full-scale range of either 0 to 1 mA (into a maximum 10 k Ω impedance), or 4 to 20 mA (into a maximum 1.2K Ω impedance). Each channel can be configured to provide full-scale output sensitivity for any range of any measured parameter.

As shown in the *Typical Wiring Diagram* on page 3–10, these outputs share one common return. The polarity of these outputs must be observed for proper operation. Shielded cable should be used, with only one end of the shield grounded, to minimize noise effects.

The analog output circuitry is isolated as a group with the Analog Input circuitry and the RTD circuitry. Only one ground reference should be used for the three circuits. Transorbs limit this isolation to ± 36 V with respect to the 489 safety ground.

If a voltage output is required, a burden resistor must be connected at the input of the SCADA measuring device. Ignoring the input impedance of the input:

$$R_{LOAD} = \frac{V_{FULL-SCALE}}{I_{MAX}}$$
 (EQ 3.1)

For example, for a 0 to 1 mA input, if 5 V full scale corresponds to 1 mA, then R_{LOAD} = 5 V / 0.001 A = 5000 Ω . For a 4 to 20 mA input, this resistor would be R_{LOAD} = 5 V / 0.020 A = 250 Ω .

3.2.9 RTD Sensor Connections

The 489 can monitor up to 12 RTD inputs for Stator, Bearing, Ambient, or Other temperature monitoring. The type of each RTD is field programmable as: 100 Ω Platinum (DIN 43760), 100 Ω Nickel, 120 Ω Nickel, or 10 Ω Copper. RTDs must be three wire type. Every two RTDs shares a common return.

The 489 RTD circuitry compensates for lead resistance, provided that each of the three leads is the same length. Lead resistance should not exceed 25 Ω per lead for platinum and nickel RTDs and 3 Ω per lead for copper RTDs. Shielded cable should be used to prevent noise pickup in the industrial environment. RTD cables should be kept close to grounded metal casings and avoid areas of high electromagnetic or radio interference. RTD leads should not be run adjacent to or in the same conduit as high current carrying

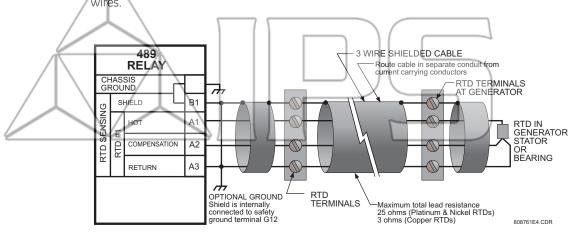


FIGURE 3-17: RTD Wiring



IMPORTANT NOTE: The RTD circuitry is isolated as a group with the Analog Input circuitry and the Analog Output circuitry. Only one ground reference should be used for the three circuits. Transorbs limit this isolation to ± 36 V with respect to the 489 safety ground. If code requires that the RTDs be grounded locally at the generator terminal box, that will also be the ground reference for the analog inputs and outputs.

3.2.10 Output Relays

There are six Form-C output relays (see *Outputs* on page 2–7). Five of the six relays are always non-failsafe, the 6 Service relay is always failsafe. As a failsafe, the 6 Service relay will be energized normally and de-energize when called upon to operate. It will also deenergize when control power to the 489 is lost and therefore, be in its operated state. All other relays, being non-failsafe, will be de-energized normally and energize when called upon to operate. Obviously, when control power is lost to the 489, these relays must be deenergized and therefore, they will be in their non-operated state. Shorting bars in the drawout case ensure that when the 489 is drawn out, no trip or alarm occurs. The 6 Service output will however indicate that the 489 has been drawn out. Each output relay has an LED indicator on the 489 front panel that comes on while the associated relay is in the operated state.

• 1 TRIP: The trip relay should be wired such that the generator is taken offline when conditions warrant. For a breaker application, the NO 1 Trip contact should be wired in series with the Breaker trip coil.

Supervision of a breaker trip coil requires that the supervision circuit be paralleled with the 1 Trip relay output contacts, as shown in the *Typical Wiring Diagram* on page 3–10. With this connection made, the supervision input circuits will place an impedance across the contacts that will draw a current of 2 to 5 mA (for an external supply

voltage from 30 to 250 V DC) through the breaker trip coil. The supervision circuits respond to a loss of this trickle current as a failure condition. Circuit breakers equipped with standard control circuits have a breaker auxiliary contact permitting the trip coil to be energized only when the breaker is closed. When these contacts are open, as detected by the Breaker Status digital input, trip coil supervision circuit is automatically disabled. This logic provides that the trip circuit is monitored only when the breaker is closed.

2 AUXILIARY, 3 AUXILIARY, 4 AUXILIARY: The auxiliary relays may be programmed for numerous functions such as, trip echo, alarm echo, trip backup, alarm or trip differentiation, control circuitry, etc. They should be wired as configuration warrants.

5 ALARM: The alarm relay should connect to the appropriate annunciator or monitoring device.

6 SERVICE: The service relay will operate if any of the 489 diagnostics detect an internal failure or on loss of control power. This output may be monitored with an annunciator, PLC or DCS.

The service relay NC contact may also be wired in parallel with the trip relay on a breaker application. This will provide failsafe operation of the generator; that is, the generator will be tripped offline in the event that the 489 is not protecting it. Simple annunciation of such a failure will allow the operator or the operation computer to either continue, or do a sequenced shutdown.



Relay contacts must be considered unsafe to touch when the system is energized! If the customer requires the relay contacts for low voltage accessible applications, it is their responsibility to ensure proper insulation levels.

3.2.11 IRIG-B

IRIG-B is a standard time-code format that allows stamping of events to be synchronized among connected devices within 1 millisecond. The IRIG-B time codes are serial, width-modulated formats which are either DC level shifted or amplitude modulated (AM). Third party equipment is available for generating the IRIG-B signal. This equipment may use a GPS satellite system to obtain the time reference enabling devices at different geographic locations to be synchronized.

Terminals E12 and F12 on the 489 unit are provided for the connection of an IRIG-B signal.

3.2.12 RS485 Ports

Two independent two-wire RS485 ports are provided. Up to 32 489 relays can be daisy-chained together on a communication channel without exceeding the driver capability. For larger systems, additional serial channels must be added. It is also possible to use commercially available repeaters to increase the number of relays on a single channel to more than 32. A suitable cable should have a characteristic impedance of 120 Ω (e.g. Belden #9841) and total wire length should not exceed 4000 feet (approximately 1200 metres). Commercially available repeaters will allow for transmission distances greater than 4000 ft.

Voltage differences between remote ends of the communication link are not uncommon. For this reason, surge protection devices are internally installed across all RS485 terminals. Internally, an isolated power supply with an optocoupled data interface is used to prevent noise coupling.

NOTE

To ensure that all devices in a daisy-chain are at the same potential, it is imperative that the common terminals of each RS485 port are tied together and grounded only once, at the master. Failure to do so may result in intermittent or failed communications.

The source computer/PLC/SCADA system should have similar transient protection devices installed, either internally or externally, to ensure maximum reliability. Ground the shield at one point only, as shown below, to avoid ground loops.

Correct polarity is also essential. All 489s must be wired with all '+' terminals connected together, and all '-' terminals connected together. Each relay must be daisy-chained to the next one. Avoid star or stub connected configurations. The last device at each end of the daisy chain should be terminated with a 120 Ω ¼ W resistor in series with a 1 nF capacitor across the '+' and '-' terminals. Observing these guidelines will result in a reliable communication system that is immune to system transients.

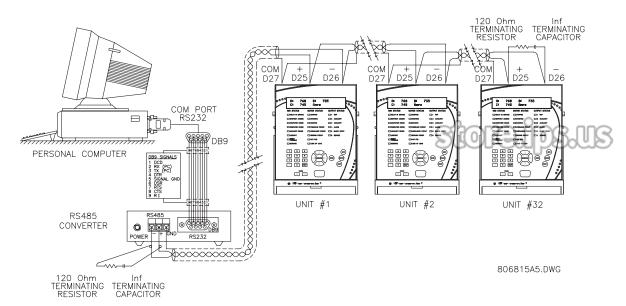


FIGURE 3-18: RS485 Communications Wiring

3.2.13 Dielectric Strength

It may be required to test a complete motor starter for dielectric strength ("flash" or hi-pot") with the 489 installed. The 489 is rated for 1.9 kV AC for 1 second, or 1.6 kV AC for 1 minute (per UL 508) isolation between relay contacts, CT inputs, VT inputs, trip coil supervision, and the safety ground terminal G12. Some precautions are required to prevent damage to the 489 during these tests.

Filter networks and transient protection clamps are used between control power, trip coil supervision, and the filter ground terminal G11. This filtering is intended to filter out high voltage transients, radio frequency interference (RFI), and electromagnetic interference (EMI). The filter capacitors and transient suppressors could be damaged by application continuous high voltage. Disconnect filter ground terminal G11 during testing of control

power and trip coil supervision. CT inputs, VT inputs, and output relays do not require any special precautions. Low voltage inputs (<30 V), RTDs, analog inputs, analog outputs, digital inputs, and RS485 communication ports are not to be tested for dielectric strength under any circumstance (see below).

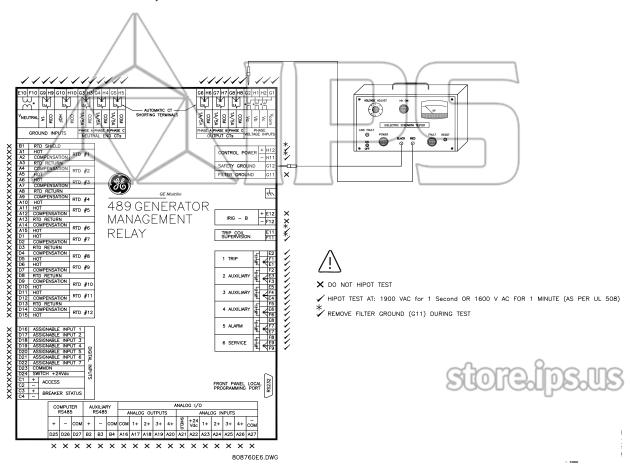


FIGURE 3-19: Testing the 489 for Dielectric Strength



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4.1 Faceplate Interface

4.1.1 Display

All messages appear on a 40-character liquid crystal display. Messages are in plain English and do not require the aid of an instruction manual for deciphering. When the user interface is not being used, the display defaults to the user-defined status messages. Any trip or alarm automatically overrides the default messages and is immediately displayed.

4.1.2 **LED Indicators**

There are three groups of LED indicators. They are 489 Status, Generator Status, and Output Status.

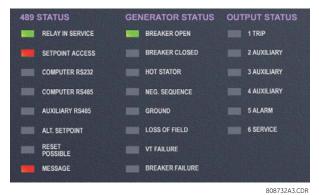


FIGURE 4-1: 489 LED Indicators

489 Status LED Indicators

- 489 IN SERVICE: Indicates that control power is applied, all monitored input/output and internal systems are OK, the 489 has been programmed, and is in protection mode, not simulation mode. When in simulation or testing mode, the LED indicator will flash.
- **SETPOINT ACCESS:** Indicates that the access jumper is installed and passcode protection has been satisfied. Setpoints may be altered and stored.
- **COMPUTER RS232:** Flashes when there is any activity on the RS232 communications port. Remains on continuously if incoming data is valid.
- COMPUTER RS485 / AUXILIARY RS485: Flashes when there is any activity on the computer/auxiliary RS485 communications port. These LEDs remain on continuously if incoming data is valid and intended for the slave address programmed in the relay.
- ALT. SETPOINTS: Flashes when the alternate setpoint group is being edited and the primary setpoint group is active. Remains on continuously if the alternate setpoint group is active. The alternate setpoint group feature is enabled as one of the assignable digital inputs. The alternate setpoints group can be selected by setting the S3 DIGITAL INPUTS ▷ ▼ DUAL SETPOINTS ▷ ▼ ACTIVATE SETPOINT GROUP setpoint to "Group 2".
- **RESET POSSIBLE:** A trip or latched alarm may be reset. Pressing the RESET key clears the trip/alarm.
- MESSAGE: Under normal conditions, the default messages selected during setpoint
 programming are displayed. If any alarm or trip condition is generated, a diagnostic
 message overrides the displayed message and this indicator flashes. If there is more
 than one condition present, MESSAGE ▼ can be used to scroll through the messages.
 Pressing any other key return to the normally displayed messages. While viewing
 normally displayed messages, the Message LED continues to flash if any diagnostic
 message is active.
 - ➤ To return to the diagnostic messages from the normally displayed messages, press the MENU key until the following message is displayed:



Now, press the MESSAGE ▶ key followed by the message ▼ key to scroll through the messages.

Note that diagnostic messages for alarms disappear with the condition while diagnostic messages for trips remain until cleared by a reset.

Generator Status LED Indicators

- **BREAKER OPEN:** Uses the breaker status input signal to indicate that the breaker is open and the generator is offline.
- **BREAKER CLOSED:** Uses the breaker status input signal to indicate that the breaker is closed and the generator is online.

- **HOT STATOR:** Indicates that the generator stator is above normal temperature when one of the stator RTD alarm or trip elements is picked up or the thermal model trip element is picked up.
- **NEG. SEQUENCE:** Indicates that the negative sequence current alarm or trip element is picked up.
- **GROUND:** Indicates that at least one of the ground overcurrent, neutral overvoltage (fundamental), or neutral undervoltage (3rd harmonic) alarm/trip elements is picked up.
- LOSS OF FIELD: Indicates that at least one of the reactive power (kvar) or field-breaker discrepancy alarm/trip elements is picked up.
- VT FAILURE: Indicates that the VT fuse failure alarm is picked up.
- BREAKER FAILURE: Indicates that the breaker failure or trip coil monitor alarm is picked up.

Output Status LED Indicators

- 1 TRIP: The 1 Trip relay has operated (energized).
- 2 AUXILIARY: The 2 Auxiliary relay has operated (energized).
- 3 AUXILIARY: The 3 Auxiliary relay has operated (energized).
- 4 AUXILIARY: The 4 Auxiliary relay has operated (energized).
- 5 ALARM: The 5 Alarm relay has operated (energized).
- 6 SERVICE: The 6 Service relay has operated (de-energized, 6 Service is fail-safe, normally energized).

4.1.3 RS232 Program Port

This port is intended for connection to a portable PC. Setpoint files may be created at any location and downloaded through this port with the EnerVista 489 Setup software. Local interrogation of setpoint and actual values is also possible. New firmware may be downloaded to the 489 flash memory through this port. Upgrading the relay firmware does not require a hardware EEPROM change.

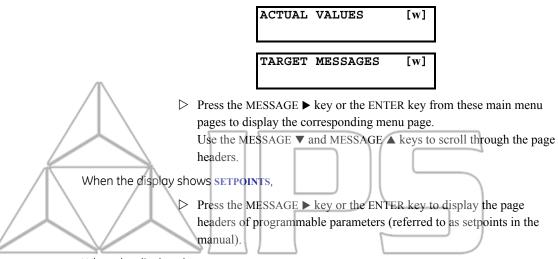
4.1.4 Keypad

Description

The 489 display messages are organized into main menus, pages, and sub-pages. There are three main menus labeled Setpoints, Actual Values, and Target Messages.

Press the MENU key followed by the MESSAGE ▼ key to scroll through the three main menu headers, which appear in sequence as follows:

SETPOINTS	[w]



When the display shows ACTUAL VALUES,

Press the MESSAGE ▶ key or the ENTER key to display the page headers of measured parameters (referred to as actual values in the manual).

When the display shows TARGET MESSAGES,

Press the MESSAGE ▶ key or the ENTER key to display the page headers of event messages or alarm conditions.

Each page is broken down further into logical sub-pages. The MESSAGE ▼ and MESSAGE ▲ keys are used to navigate through the sub-pages. A summary of the setpoints and actual values can be found in the chapters 5 and 6, respectively.

The ENTER key is dual-purpose. It is used to enter the sub-pages and to store altered setpoint values into memory to complete the change. The MESSAGE ▶ key can also be used to enter sub-pages but not to store altered setpoints.

The ESCAPE key is also dual-purpose. It is used to exit the sub-pages and to cancel a setpoint change. The MESSAGE ◀ key can also be used to exit sub-pages and to cancel setpoint changes.

The VALUE keys are used to scroll through the possible choices of an enumerated setpoint. They also decrement and increment numerical setpoints. Numerical setpoints may also be entered through the numeric keypad.

Press the HELP key to display context-sensitive information about setpoints such as the range of values and the method of changing the setpoint.

Help messages will automatically scroll through all messages currently appropriate.

The RESET key resets any latched conditions that are not presently active. This includes resetting latched output relays, latched Trip LEDs, breaker operation failure, and trip coil failure.

The MESSAGE ▼ and MESSAGE ▲ keys scroll through any active conditions in the relay. Diagnostic messages are displayed indicating the state of protection and monitoring elements that are picked up, operating, or latched. When the Message LED is on, there are messages to be viewed with the MENU key by selecting target messages as described earlier.

Entering Alphanumeric Text

Text setpoints have data values that are fixed in length but user-defined in character. They may be comprised of upper case letters, lower case letters, numerals, and a selection of special characters. The editing and storing of a text value is accomplished with the use of the decimal [.], VALUE, and ENTER keys.

Move to message S3 DIGITAL INPUTS ▷ ♥ GENERAL INPUT A ▷ ASSIGN DIGITAL INPUT, and scrolling with the VALUE keys, select "Input 1".
 The relay will display the following message:

ASSIGN DIGITAL INPUT: Input 1

Press the MESSAGE ▼ key to view the INPUT NAME setpoint.
The name of this user-defined input will be changed in this example from the generic "Input A" to something more descriptive.

If an application is to be using the relay as a station monitor, it is more informative to rename this input "Stn. Monitor".

Press the decimal [.] to enter the text editing mode.

The first character will appear underlined as follows:

INPUT NAME: Input A

- ▶ Press the VALUE keys until the character "S" is displayed in the first position.
- Press the decimal [.] key to store the character and advance the cursor to the next position.
- Change the second character to a "t" in the same manner.
- Continue entering characters in this way until all characters of the text "Stn. Monitor" are entered.

Note that a space is selected like a character.

- If a character is entered incorrectly, press the decimal [.] key repeatedly until the cursor returns to the position of the error. Re-enter the character as required.
- Once complete, press the ENTER key to remove the solid cursor and view the result.

Once a character is entered, by pressing the ENTER key, it is automatically saved in Flash Memory, as a new setpoint.

INPUT NAME: Stn. Monitor The 489 does not have '+' or '-' keys. Negative numbers may be entered in one of two manners.

- Immediately pressing one of the VALUE keys causes the setpoint to scroll through its range including any negative numbers.
- After entering at least one digit of a numeric setpoint value, pressing the VALUE keys changes the sign of the value where applicable.

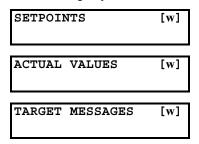
4.1.5 Setpoint Entry

To store any setpoints, terminals C1 and C2 (access terminals) must be shorted (a keyswitch may be used for security). There is also a setpoint passcode feature that restricts access to setpoints. The passcode must be entered to allow the changing of setpoint values. A passcode of "0" effectively turns off the passcode feature - in this case only the access jumper is required for changing setpoints. If no key is pressed for 5 minutes, access to setpoint values will be restricted until the passcode is entered again. To prevent setpoint access before the 5 minutes expires, the unit may be turned off and back on, the access jumper may be removed, or the **SETPOINT ACCESS** setpoint may be changed to "Restricted". The passcode cannot be entered until terminals C1 and C2 (access terminals) are shorted. When setpoint access is allowed, the Setpoint Access LED indicator on the front of the 489 will be lit.

Setpoint changes take effect immediately, even when generator is running. However, changing setpoints while the generator is running is not recommended as any mistake may cause a nuisance trip.

The following procedure may be used to access and alter setpoints. This specific example refers to entering a valid passcode to allow access to setpoints if the passcode was "489".

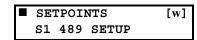
▶ Press the MENU key to access the header of each menu, which will be displayed in the following sequence:



- Press the MENU key until the display shows the header of the setpoints menu.
- Press the MESSAGE ▶ or ENTER key to display the header for the first setpoints page.

The set point pages are numbered, have an 'S' prefix for easy identification and have a name which gives a general idea of the setpoints available in that page.

Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through all the available setpoint page headers.
Setpoint page headers look as follows:



To enter a given setpoints page,

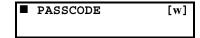
Press the MESSAGE ▶ or ENTER key.

Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through sub-page headers until the required message is reached.

The end of a page is indicated by the message **END OF PAGE**. The beginning of a page is indicated by the message **TOP OF PAGE**.

Each page is broken further into subgroups.

- Press MESSAGE ▼ or MESSAGE ▲ to cycle through subgroups until the desired subgroup appears on the screen.
- Press the MESSAGE ▶ or ENTER key to enter a subgroup.



Each sub-group has one or more associated setpoint messages.

Press the MESSAGE ▼ or MESSAGE ▲ keys to scroll through setpoint messages until the desired message appears.

ENTER PASSCODE FOR ACCESS:

The majority of setpoints are changed by pressing the VALUE keys until the desired value appears, and then pressing ENTER. Numeric setpoints may also be entered through the numeric keys (including decimals). If the entered setpoint is out of range, the original setpoint value reappears. If the entered setpoint is out of step, an adjusted value will be stored (e.g. 101 for a setpoint that steps 95, 100, 105 is stored as 100). If a mistake is made entering the new value, pressing ESCAPE returns the setpoint to its original value. Text editing is a special case described in detail in *Entering Alphanumeric Text* on page 4–5. Each time a new setpoint is successfully stored, a message will flash on the display stating

NEW SETPOINT HAS BEEN STORED.

▶ Press the 4, 8, 9 keys, then press ENTER. The following flash message is displayed:

> NEW SETPOINT HAS BEEN STORED

and the display returns to:

SETPOINT ACCESS: PERMITTED

Press ESCAPE or MESSAGE ■ to exit the subgroup. Pressing ESCAPE or MESSAGE ■ numerous times will always return the cursor to the top of the page.

4.1.6 Diagnostic Messages

Diagnostic messages are automatically displayed for any active conditions in the relay such as trips, alarms, or asserted logic inputs. These messages provide a summary of the present state of the relay. The Message LED flashes when there are diagnostic messages available; press the MENU key until the relay displays **TARGET MESSAGES**, then press the MESSAGE ▶ key, followed by the MESSAGE ▼ key, to scroll through the messages. For additional information and a complete list of diagnostic messages, refer to *Diagnostic Messages* on page 6–32.

4.1.7 Self-Test Warnings

The 489 relay performs self test diagnostics at initialization (after power up), and continuously as a background task to ensure every testable unit of the hardware and software is functioning correctly. There are two types of self-test warnings indicating either a minor or major problem. Minor problems indicate a problem with the relay that does not compromise protection. Major problems indicate a very serious relay problem which comprises all aspects of relay operation.

Upon detection of either a minor or a major problem the relay will:

- De-energize the self-test warning relay
- Light the self-test warning LED
- Flash a diagnostic message periodically on the display screen

The 489 self-test warnings are shown below.



Table 4-1: Self-Test Warnings

Message	Severity	Description
Self-Test Warning 1 Replace Immediately	Major	This warning is caused by detection of a corrupted location in the program memory as determined by a CRC error checking code. Any function of the relay is susceptible to malfunction from this failure.
Self-Test Warning 2 Replace Immediately	Major	This warning is caused by a failure of the analog to digital converter. The integrity of system input measurements is affected by this failure.
Self-Test Warning 3 Replace Immediately	Major	This warning is caused by a failure of the analog to digital converter. The integrity of system input measurements is affected by this failure.
Self-Test Warning 5 Replace Immediately	Major	This warning is caused by out of range reading of self test RTD 13. The integrity of system input measurements is affected by this failure.
Self-Test Warning 6 Replace Immediately	Major	This warning is caused by out of range reading of self test RTD 14. The integrity of system input measurements is affected by this failure.
Self-Test Warning 7 Replace Immediately	Major	This warning is caused by out of range reading of self test RTD15. The integrity of system input measurements is affected by this failure.

Table 4–1: Self-Test Warnings

	Message	Severity	Description
	Self-Test Warning 8 Replace Immediately	Major	This warning is caused by out of range reading of self test RTD16. The integrity of system input measurements is affected by this failure.
	Clock Not Set Program Date/Time	Minor	Occurs if the clock has not been set.
	Unit Temp. Exceeded Service/CheckAmbient	Minor	Caused by the detection of unacceptably low (less than –40°C) or high (greater than 85°C) temperatures detected inside the unit.
	Unit Not Calibrated Replace Immediately	Minor	This warning occurs when the relay has not been factory calibrated.
	Relay Not Configured Consult User Manual	Minor	This warning occurs when the 489 CT Primary or Generator parameters are not set.
	Service Required Schedule Maintenance	Minor	This warning is caused by a failure of the Real Time Clock circuit. The ability of the relay to maintain the current date and time is lost.

4.1.8 Flash Messages

Flash messages are warning, error, or general information messages displayed in response to certain key presses. The length of time these messages remain displayed can be programmed in S1 RELAY SETUP $\triangleright \nabla$ PREFERENCES $\triangleright \nabla$ DEFAULT MESSAGE CYCLE TIME. The factory default flash message time is 4 seconds. For additional information and a complete list of flash messages, refer to Flash Messages on page 6–33.

4.2 EnerVista Software Interface

4.2.1 Overview

The front panel provides local operator interface with a liquid crystal display. The EnerVista 489 Setup software provides a graphical user interface (GUI) as one of two human interfaces to a 489 device. The alternate human interface is implemented via the device's faceplate keypad and display (see the first section in this chapter).

The EnerVista 489 Setup software provides a single facility to configure, monitor, maintain, and trouble-shoot the operation of relay functions, connected over serial communication networks. It can be used while disconnected (i.e. off-line) or connected (i.e. on-line) to a 489 device. In off-line mode, setpoint files can be created for eventual downloading to the device. In on-line mode, you can communicate with the device in real-time.

This no-charge software, provided with every 489 relay, can be run from any computer supporting Microsoft Windows[®] 95 or higher. This chapter provides a summary of the basic EnerVista 489 Setup software interface features. The EnerVista 489 Setup help file provides details for getting started and using the software interface.

With the EnerVista 489 Setup running on your PC, it is possible to

- Program and modify setpoints
- Load/save setpoint files from/to disk
- Read actual values and monitor status
- Perform waveform capture and log data
- Plot, print, and view trending graphs of selected actual values
- Download and playback waveforms
- Get help on any topic

4.2.2 Hardware

Communications from the EnerVista 489 Setup to the 489 can be accomplished three ways: RS232, RS485, and Ethernet (requires the MultiNet adapter) communications. The following figures below illustrate typical connections for RS232 and RS485 communications. For additional details on Ethernet communications, please see the MultiNet manual (GE Publication number GEK-106498).



FIGURE 4–2: Communications using The Front RS232 Port



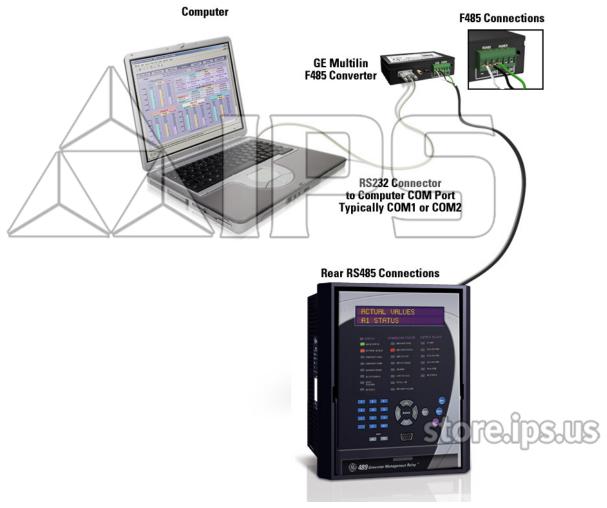


FIGURE 4–3: Communications using Rear RS485 Port

4.2.3 Installing the EnerVista 489 Setup Software

The following minimum requirements must be met for the EnerVista 489 Setup software to operate on your computer.

- Pentium class or higher processor (Pentium II 400 MHz or better recommended)
- Microsoft Windows 95, 98, 98SE, ME, NT 4.0 (SP4 or higher), 2000, XP
- Internet Explorer version 4.0 or higher (required libraries)
- 128 MB of RAM (256 MB recommended)
- Minimum of 200 MB hard disk space

A list of qualified modems for serial communications is shown below:

- US Robotics external 56K Faxmodem 5686
- US Robotics external Sportster 56K X2
- PCTEL 2304WT V.92 MDC internal modem

After ensuring these minimum requirements, use the following procedure to install the EnerVista 489 Setup software from the enclosed GE EnerVista CD.

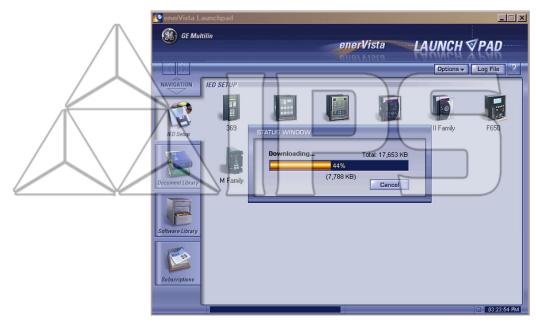
- Click the **Install Now** button and follow the installation instructions to install the no-charge EnerVista software on the local PC.
- ▶ When installation is complete, start the EnerVista Launchpad application.
- Click the **IED Setup** section of the **Launch Pad** window.



- ➢ In the EnerVista Launch Pad window, click the Add Product button and select the "489 Generator Management Relay" from the Install Software window as shown below.
- Select the "Web" option to ensure the most recent software release, or select "CD" if you do not have a web connection.
- Click the **Add Now** button to list software items for the 489.



EnerVista Launchpad will obtain the latest installation software from the Web or CD and automatically start the installation process. A status window with a progress bar will be shown during the downloading process.



- Select the complete path, including the new directory name, where the EnerVista 489 Setup software will be installed.
- ➢ Click on Next to begin the installation. The files will be installed in the directory indicated and the installation program will automatically create icons and add EnerVista 489 Setup software to the Windows start menu.
- Click Finish to end the installation. The 489 device will be added to the list of installed IEDs in the EnerVista Launchpad window, as shown below.



4.3 Connecting EnerVista 489 Setup to the Relay

4.3.1 Configuring Serial Communications

Before starting, verify that the serial cable is properly connected to either the RS232 port on the front panel of the device (for RS232 communications) or to the RS485 terminals on the back of the device (for RS485 communications). See *Hardware* on page 4–10 for connection details.

This example demonstrates an RS232 connection. For RS485 communications, the GE Multilin F485 converter will be required. Refer to the F485 manual for additional details. To configure the relay for Ethernet communications, see *Configuring Ethernet Communications* on page 4–17.

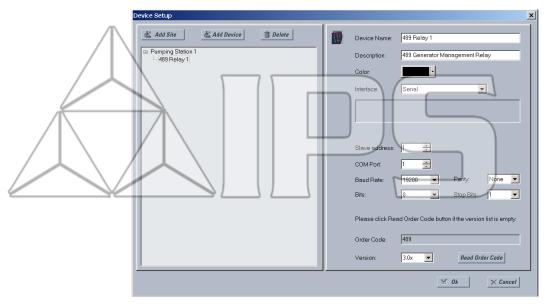
 ➢ Install and start the latest version of the EnerVista 489 Setup software (available from the GE EnerVista CD).
 See the previous section for the installation procedure.

- Click on the **Device Setup** button to open the Device Setup window.
- Click the **Add Site** button to define a new site.
- ▷ Enter the desired site name in the Site Name field.
 If desired, a short description of site can also be entered along with the display order of devices defined for the site.
 In this example, we will use "Pumping Station 1" as the site name.
- Click the **OK** button when complete.

The new site will appear in the upper-left list in the EnerVista 489 Setup window.

- Click the **Add Device** button to define the new device.
- Enter the desired name in the **Device Name** field and a description (optional) of the site.

➢ Select "Serial" from the Interface drop-down list. This will display a number of interface parameters that must be entered for proper RS232 functionality.



- Enter the physical communications parameters (baud rate and parity setpoints) in their respective fields.

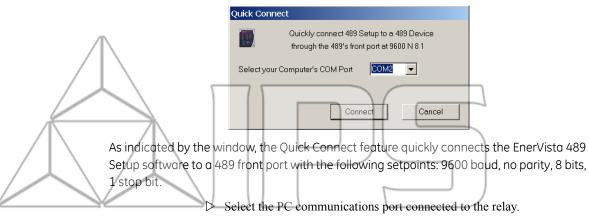
 Note that when communicating to the relay from the front port, the default communications setpoints are a baud rate of 9600, with slave address of 1, no parity, 8 bits, and 1 stop bit. **These values cannot be changed**.
- Click the Read Order Code button to connect to the 489 device and upload the order code.
 If a communications error occurs, ensure that the 489 serial communications values entered in the previous step correspond to the relay setting values.
- Click **OK** when the relay order code has been received. The new device will be added to the Site List window (or Online window) located in the top left corner of the main EnerVista 489 Setup window.

The 489 Site Device has now been configured for serial communications. Proceed to *Connecting to the Relay* on page 4–19 to begin communications.

4.3.2 Using the Quick Connect Feature

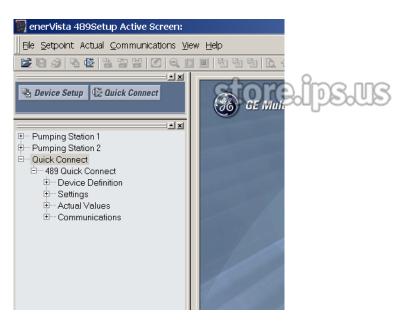
The Quick Connect button can be used to establish a fast connection through the front panel RS232 port of a 489 relay.

Press the Quick Connect button.The following window will appear:



Press the **Connect** button.

The EnerVista 489 Setup software will display a window indicating the status of communications with the relay. When connected, a new Site called "Quick Connect" will appear in the Site List window. *The properties of this new site cannot be changed*.



The 489 Site Device has now been configured via the Quick Connect feature for serial communications. Proceed to *Connecting to the Relay* on page 4–19 to begin communications.

4.3.3 Configuring Ethernet Communications

▶ Before starting, verify that the Ethernet cable is properly connected to the RJ-45 Ethernet port.

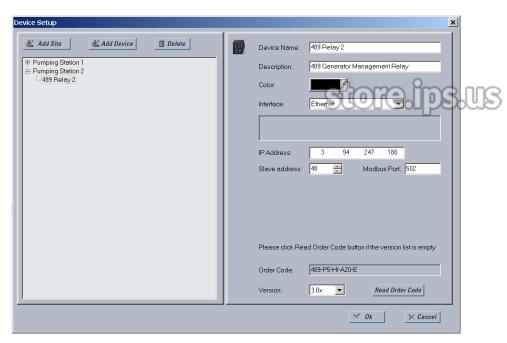
- ➢ Install and start the latest version of the EnerVista 489 Setup software (available from the GE EnerVista CD).
 See the previous section for the installation procedure.
- Click on the **Device Setup** button to open the Device Setup window.
- Click the **Add Site** button to define a new site.
- Enter the desired site name in the Site Name field. If desired, a short description of site can also be entered along with the display order of devices defined for the site. In this example, we will use "Pumping Station 2" as the site name.
- Click the **OK** button when complete.

The new site will appear in the upper-left list.

(optional).

Click the Add Device button to define the new device.

Select "Ethernet" from the Interface drop-down list.
This will display a number of interface parameters that must be entered for proper Ethernet functionality.



- Enter the IP address assigned to the relay.
- Click the **Read Order Code** button to connect to the 489 device and upload the order code.
 - If a communications error occurs, ensure that the 489 Ethernet communications values entered in the previous step correspond to the relay setting values.

Click **OK** when the relay order code has been received. The new device will be added to the Site List window (or Online window) located in the top left corner of the main EnerVista 489 Setup window.

The 489 Site Device has now been configured for Ethernet communications. Proceed to the following section to begin communications.

4.3.4 Connecting to the Relay

Now that the communications parameters have been properly configured, the user can easily connect to the relay.

- Expand the Site list by double clicking on the site name or clicking on the «+» box to list the available devices for the given site (for example, in the "Pumping Station 1" site shown below).
- Expand the desired device trees by clicking the «+» box. The following list of headers is shown for each device:
- Device Definitions
- Setpoints
- Actual Values
- Commands
- Communications
 - Expand the **Setpoints > Protection > Current Elements** list item and select the Phase Overcurrent tab to open the Phase Overcurrent setpoint window as shown below:

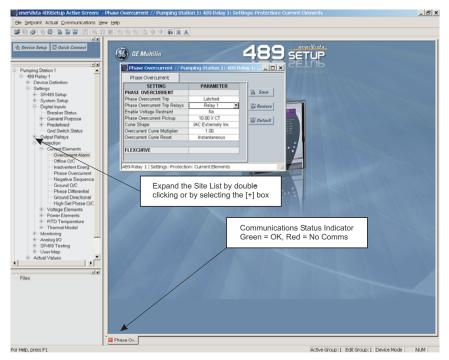


FIGURE 4-4: Main Window after Connection

The Phase Overcurrent setpoint window will open with a corresponding status indicator on the lower left of the EnerVista 489 Setup window.

▷ If the status indicator is red, verify that the serial cable is properly connected to the relay, and that the relay has been properly configured for communications (steps described earlier).

Setpoints can now be edited, printed, or changed according to user specifications. Other setpoint and commands windows can be displayed and edited in a similar manner. Actual values windows are also available for display. These windows can be locked, arranged, and resized at will.

Note



Refer to the EnerVista 489 Setup help file for additional information about using the software.



4.4 Working with Setpoints and Setpoint Files

4.4.1 Engaging a Device

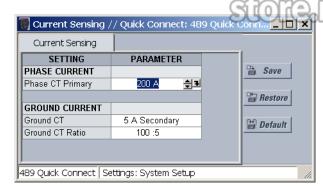
The EnerVista 489 Setup software may be used in on-line mode (relay connected) to directly communicate with a 489 relay. Communicating relays are organized and grouped by communication interfaces and into sites. Sites may contain any number of relays selected from the SR or UR product series.

4.4.2 Entering Setpoints

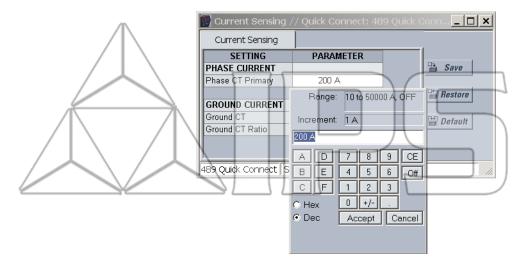
The System Setup page will be used as an example to illustrate the entering of setpoints. In this example, we will be changing the current sensing setpoints.

- Establish communications with the relay.
- Select the Setpoint > System Setup menu item.
 This can be selected from the device setpoint tree or the main window menu bar.
- > Select the **Current Sensing** menu item.
- Select the **PHASE CT PRIMARY** setpoint by clicking anywhere in the parameter box.

This will display three arrows: two to increment/decrement the value and another to launch the numerical calculator.



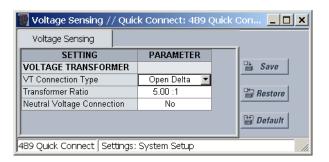
Click the arrow at the end of the box to display a numerical keypad interface that allows the user to enter a value within the setpoint range displayed near the top of the keypad:



- Click **Accept** to exit from the keypad and keep the new value.
- Click on Cancel to exit from the keypad and retain the old value.

For setpoints requiring non-numerical pre-set values (e.g. **VT CONNECTION TYPE** below, in the Voltage Sensing window),

- Click anywhere within the setpoint value box to display a drop-down selection menu arrow.
- Click on the arrow to select the desired setpoint.



For setpoints requiring an alphanumeric text string (e.g. message scratchpad messages), the value may be entered directly within the setpoint value box.

- ▶ In the Setpoint / System Setup dialog box, click on **Save** to save the values into the 489.
- Click **Yes** to accept any changes.
- Click **No**, and then **Restore** to retain previous values and exit.

4.4.3 Using Setpoint Files

Overview

The EnerVista 489 Setup software interface supports three ways of handling changes to relay setpoints:

- In **off-line** mode (relay disconnected) to create or edit relay setpoint files for later download to communicating relays.
 - Directly modifying relay setpoints while **connected** to a communicating relay, then saving the setpoints when complete.
- Creating/editing setpoint files while *connected* to a communicating relay, then saving them to the relay when complete.

Settings files are organized on the basis of file names assigned by the user. A settings file contains data pertaining to the following types of relay settings:

- Device Definition
- Product Setup
- System Setup
- Digital Inputs
- Output Relays
- Voltage Elements
- Power Elements
- RTD Temperature
- Thermal Model
- Monitoring Functions
- Analog Inputs and Outputs
- Relay Testing
- User Memory Map Setting Tool

Factory default values are supplied and can be restored after any changes.

The EnerVista 489 Setup display relay setpoints with the same hierarchy as the front panel display. For specific details on setpoints, refer to Chapter 5.

Downloading and Saving Setpoints Files

Setpoints must be saved to a file on the local PC before performing any firmware upgrades. Saving setpoints is also highly recommended before making any setpoint changes or creating new setpoint files.

The EnerVista 489 Setup window, setpoint files are accessed in the Setpoints List control bar window or the Files window. Use the following procedure to download and save setpoint files to a local PC.

- Ensure that the site and corresponding device(s) have been properly defined and configured as shown in *Connecting EnerVista 489 Setup to the Relay* on page 4–15.
- > Select the desired device from the site list.



Select the **File > Read Settings from Device** menu item to obtain settings information from the device.

After a few seconds of data retrieval, the software will request the name and destination path of the setpoint file. The corresponding file extension will be automatically assigned.

Press Save to complete the process.
 A new entry will be added to the tree, in the File pane, showing path and file name for the setpoint file.

Adding Setpoints Files to the Environment

The EnerVista 489 Setup software provides the capability to review and manage a large group of setpoint files. Use the following procedure to add a new or existing file to the list.

> In the files pane, right-click on 'Files'

Select the Add Existing Setting File item as shown:



The Open dialog box will appear, prompting for a previously saved setting file. As for any other Windows[®] application,

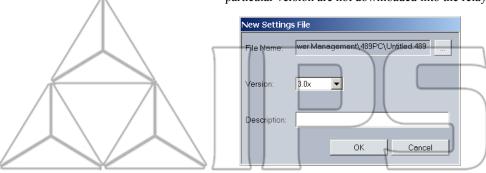
- Click Open.The new file and complete path will be added to the file list.

Creating a New Setpoint File

The EnerVista 489 Setup software allows the user to create new setpoint files independent of a connected device. These can be uploaded to a relay at a later date. The following procedure illustrates how to create new setpoint files.

▷ In the File pane, right click on 'File'.

Select the **New Settings File** item. The EnerVista 489 Setup software displays the following box, allowing for the configuration of the setpoint file for the correct firmware version. It is important to define the correct firmware version to ensure that setpoints not available in a particular version are not downloaded into the relay.

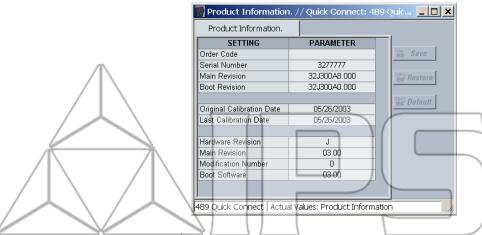


- > Select the Firmware **Version** for the new setpoint file.
- ➢ For future reference, enter some useful information in the **Description** box to facilitate the identification of the device and the purpose of the file.
- ▶ To select a file name and path for the new file, click the button beside the Enter File Name box.
- Select the file name and path to store the file, or select any displayed file name to update an existing file.
 All 489 setpoint files should have the extension '489' (for example, 'motor1.489').
- Click Save and OK to complete the process.
 Once this step is completed, the new file, with a complete path, will be added to the EnerVista 489 Setup software environment.

Upgrading Setpoint Files to a New Revision

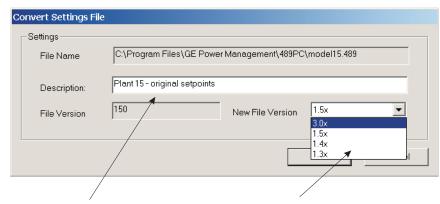
It is often necessary to upgrade the revision code for a previously saved setpoint file after the 489 firmware has been upgraded (for example, this is required for firmware upgrades). This is illustrated in the following procedure.

- Establish communications with the 489 relay.
- Select the **Actual > Product Information** menu item and record the Software Revision identifier of the relay firmware as shown below.



- Load the setpoint file to be upgraded into the EnerVista 489 Setup environment as described in *Adding Setpoints Files to the Environment* on page 4–24.
- ▷ In the File pane, select the saved setpoint file.
- ▶ From the main window menu bar, select the File > Properties menu item and note the version code of the setpoint file.
 If this version (e.g. 4.0X shown below) is different than the Software Revision code noted in step 2, select a New File Version that matches the Software Revision code from the pull-down menu.

For example, if the software revision is 3.00 and the current setpoint file revision is 1.50, change the setpoint file revision to "3.0X", as shown below.



Enter any special comments about the setpoint file here.

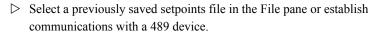
Select the desired setpoint version from this menu. The 3.0x indicates versions 3.00, 3.01, 3.02, etc.

▶ When complete, click Convert to convert the setpoint file to the desired revision.

A dialog box will request confirmation. See *Loading Setpoints from a File* on page 4–28 for instructions on loading this setpoint file into the 489.

Printing Setpoints and Actual Values

The EnerVista 489 Setup software allows the user to print partial or complete lists of setpoints and actual values. Use the following procedure to print a list of setpoints:



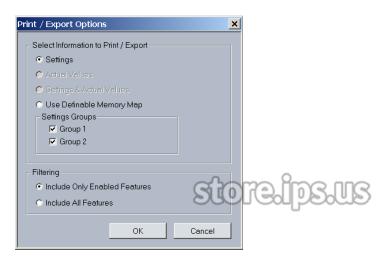
From the main window, select the **File > Print Settings** menu item.

The Print/Export Options dialog box will appear.

> Select Settings in the upper section.

Select either Include All Features (for a complete list) or Include Only Enabled Features (for a list of only those features which are currently used) in the filtering section.

Click OK.



The process for **File > Print Preview Settings** is identical to the steps above.

Setpoints lists can be printed in the same manner by right clicking on the desired file (in the file list) or device (in the device list) and selecting the **Print Device Information** or **Print Settings File** options.

A complete list of actual values can also be printed from a connected device with the following procedure:

- Establish communications with the desired 489 device.
- From the main window, select the **File > Print Settings** menu item.

The Print/Export Options dialog box will appear.

- Select Actual Values in the upper section.
- Select either Include All Features (for a complete list) or Include Only Enabled Features (for a list of only those features which are currently used) in the filtering section.
- Click OK.

Actual values can be printed in the same manner by right clicking on the desired device (in the device list) and selecting the **Print Device Information** option.

Loading Setpoints from a File



An error message will occur when attempting to download a setpoint file with a revision number that does not match the relay firmware. If the firmware has been upgraded since saving the setpoint file, see *Upgrading Setpoint Files to a New Revision* on page 4–25 for instructions on changing the revision number of a setpoint file.

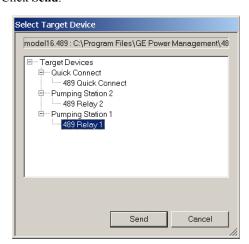
The following procedure illustrates how to load setpoints from a file. Before loading a setpoint file, it must first be added to the EnerVista 489 Setup environment as described in Adding Setpoints Files to the Environment on page 4–24.

Select the previously saved setpoint file from the File pane of the EnerVista 489 Setup software main window.

- Select the **File > Properties** menu item and verify that the corresponding file is fully compatible with the hardware and firmware version of the target relay.
 - If the versions are not identical, see *Upgrading Setpoint Files to a New Revision* on page 4–25 for details on changing the setpoints file version.
- **▷** Select the **Write Settings to Device** item.

The software will prompt for a target device.

- ➢ Select the desired device.
- Click Send.



If there is an incompatibility, an error of the following type will occur.



If there are no incompatibilities between the target device and the Setpoints file, the data will be transferred to the relay. An indication of the percentage completed will be shown in the bottom of the main menu.



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4.5 Upgrading Relay Firmware

4.5.1 Description

To upgrade the 489 firmware, follow the procedures listed in this section. Upon successful completion of this procedure, the 489 will have new firmware installed with the original setpoints.

The latest firmware files are available from the GE Multilin website at

http://www.GEmultilin.com.

4.5.2 / Saving Setpoints to a File

Before upgrading firmware, it is very important to save the current 489 settings to a file on your PC. After the firmware has been upgraded, it will be necessary to load this file back into the 489.

Refer to *Downloading and Saving Setpoints Files* on page 4–23 for details on saving relay setpoints to a file.

4.5.3 Loading New Firmware

Loading new firmware into the 489 flash memory is accomplished as follows:

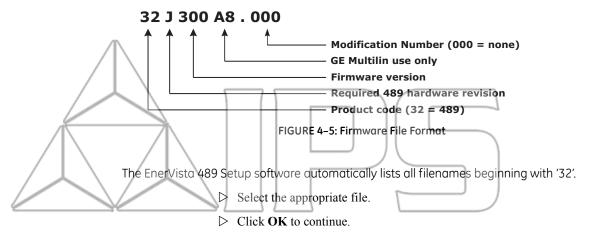
- Connect the relay to the local PC and save the setpoints to a file as shown in *Downloading and Saving Setpoints Files* on page 4–23.
- Select the Communications > Update Firmware menu item. The following warning message will appear.



Select Yes to proceed or No to cancel the process.
 Do not proceed unless you have saved the current setpoints

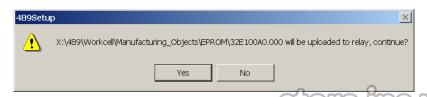
An additional message will be displayed to ensure the PC is connected to the relay front port, as the 489 cannot be upgraded via the rear RS485 ports.

The EnerVista 489 Setup software will request the new firmware file. Locate the file to load into the 489. The firmware filename has the following format:



The software will prompt with another Upload Firmware Warning window. This will be the final chance to cancel the firmware upgrade before the flash memory is erased.

Click **Yes** to continue or **No** to cancel the upgrade.



The EnerVista 489 Setup software now prepares the 489 to receive the new firmware file. The 489 will display a message indicating that it is in Upload Mode. While the file is being loaded into the 489, a status box appears showing how much of the new firmware file has been transferred and how much is remaining, as well as the upgrade status. The entire transfer process takes approximately five minutes.

The EnerVista 489 Setup software will notify the user when the 489 has finished loading the file.

Carefully read any displayed messages and click **OK** to return the main screen.

Note



Cycling power to the relay is recommended after a firmware upgrade.

After successfully updating the 489 firmware, the relay will not be in service and will require setpoint programming. To communicate with the relay, the following settings will have to be manually programmed.

MODBUS COMMUNICATION ADDRESS
BAUD RATE
PARITY (if applicable)

When communications is established, the saved setpoints must be reloaded back into the relay. See *Loading Setpoints from a File* on page 4–28 for details.

Modbus addresses assigned to firmware modules, features, settings, and corresponding data items (i.e. default values, min/max values, data type, and item size) may change slightly from version to version of firmware.

The addresses are rearranged when new features are added or existing features are enhanced or modified. The **EEPROM DATA ERROR** message displayed after upgrading/downgrading the firmware is a resettable, self-test message intended to inform users that the Modbus addresses have changed with the upgraded firmware. This message does not signal any problems when appearing after firmware upgrades.



4.6 Advanced EnerVista 489 Setup Features

4.6.1 Triggered Events

While the interface is in either on-line or off-line mode, data generated by triggered specified parameters can be viewed and analyzed via one of the following:

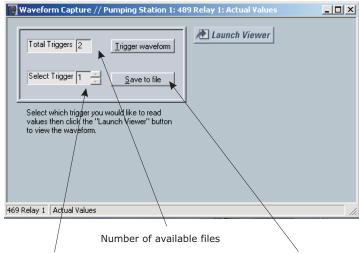
- **Event Recorder**: The event recorder captures contextual data associated with the last 256 events, listed in chronological order from most recent to the oldest.
- Oscillography: The oscillography waveform traces provide a visual display of power system and relay operation data captured during specific triggered events.

4.6.2 Waveform Capture (Trace Memory)

The EnerVista 489 Setup software can be used to capture waveforms (or view trace memory) from the 489 relay at the instance of a trip. A maximum of 128 cycles can be captured and the trigger point can be adjusted to anywhere within the set cycles. A maximum of 16 waveforms can be buffered (stored) with the buffer/cycle trade-off.

The following waveforms can be captured:

- Phase A, B, and C currents (I_a , I_b , and I_c)
- Neutral end A, B, and C currents (Ineutral_a, Ineutral_b, and Ineutral_c)
- Ground currents (Ia)
- Phase A-N, B-N, and C-N voltages ($\emph{\textbf{V}}_{a}$, $\emph{\textbf{V}}_{b}$, and $\emph{\textbf{V}}_{c}$)
 - ▶ With EnerVista 489 Setup running and communications established, select the Actual > Waveform Capture menu item to open the waveform capture setup window:



Files to be saved or viewed

Save waveform to a file

Click on **Trigger Waveform** to trigger a waveform capture.

The waveform file numbering starts with the number zero in the 489; therefore, the maximum trigger number will always be one less then the total number triggers available.

Click on the **Save to File** button to save the selected waveform to the local PC.

A new window will appear requesting for file name and path.

The file is saved as a CSV (comma delimited values) file, which can be viewed and manipulated with compatible third-party software.

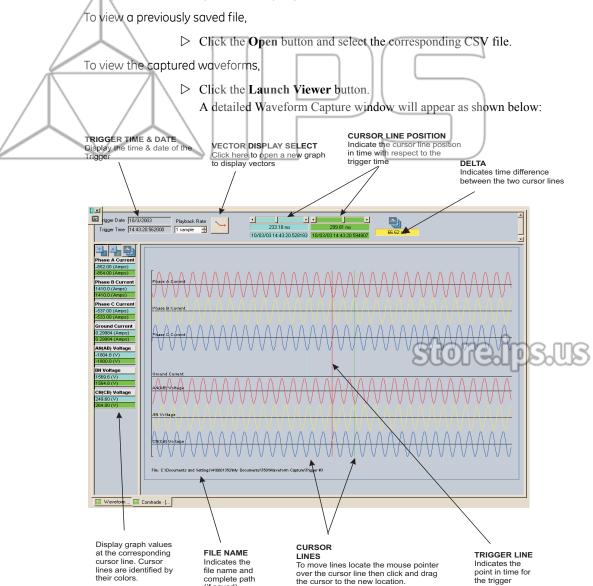


FIGURE 4-6: Waveform Capture Window Attributes

The red vertical line indicates the trigger point of the relay.

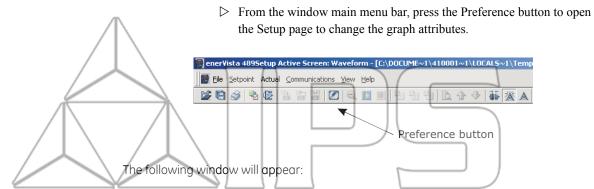
The date and time of the trigger is displayed at the top left corner of the window. To match the captured waveform with the event that triggered it,

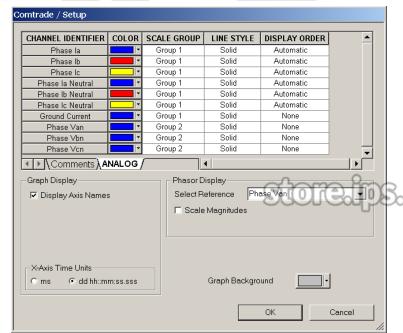
- Make note of the time and date shown in the graph.
- Find the event that matches the same time and date in the event recorder.

The event record will provide additional information on the cause and the system

conditions at the time of the event.

Additional information on how to download and save events is shown in *Event Recorder* on page 4–40.





- ▶ Change the Color of each graph as desired, and select other options, as required, by checking the appropriate boxes.
- Click **OK** to store these graph attributes, and to close the window.

The Waveform Capture window will reappear with the selected graph attributes available for use.

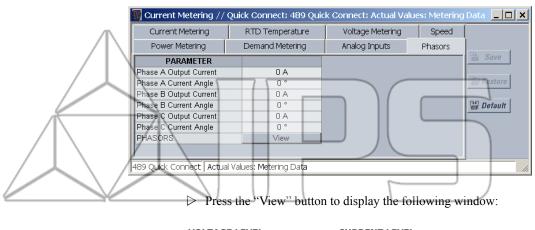
4.6.3 Phasors

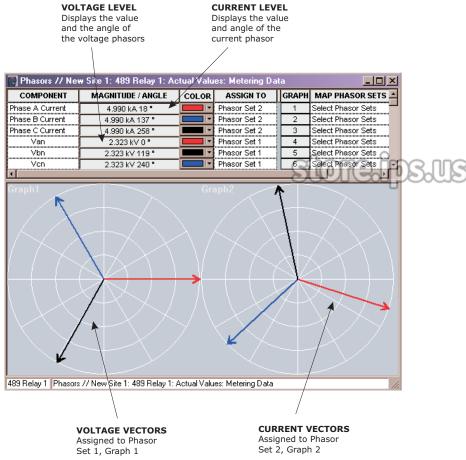
The EnerVista 489 Setup software can be used to view the phasor diagram of three-phase currents and voltages. The phasors are for: Phase Voltages Va, Vb, and Vc; Phase Currents Ia, Ib, and Ic.

▶ With the EnerVista 489 Setup software running and communications established, open the Actual Values > Metering Data window.

Click on the Phasors tab.

The EnerVista 489 Setup software will display the following window:





The 489 Generator Management Relay was designed to display lagging angles. Therefore, if a system condition would cause the current to lead the voltage by 45°, the 489 relay will display such angle as 315° Lag instead of 45° Lead.



When the currents and voltages measured by the relay are zero, the angles displayed by the relay and those shown by the EnerVista 489 Setup software are not fixed values.

Trending (Data Logger) 4.6.4

The trending or data logger feature is used to sample and record up to eight actual values at an interval defined by the user. Several parameters can be trended and graphed at sampling periods ranging from 1 second up to 1 hour. The parameters which can be trended by the EnerVista 489 Setup software are:

Currents/Voltages:

Phase Currents A, B, and C

Generator Load

Negative-Sequence Current

Ground Current and Neutral Current

Differential Currents A, B, and C

System Frequency

Voltages Vab, Vbc, Vca Van, Vbn & Vcn

Power:

Power Factor

Real (kW) Reactive (kvar), and Apparent (kVA) Power

Positive Watthours

Positive and Negative Varhours

• Temperature:

Hottest Stator RTD Thermal Capacity Used RTDs 1 through 12

Demand:

Current

Peak Current

Reactive Power

Peak Reactive Power

Apparent Power

Peak Apparent Power

Others:

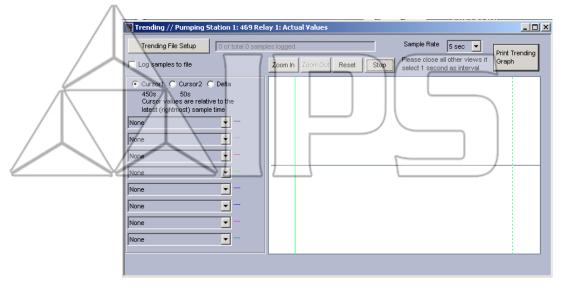
Analog Inputs 1, 2, 3, and 4 Tachometer



With EnerVista 489 Setup running and communications established,

Select the **Actual Values** > **Trending** menu item to open the trending window.

The following window will appear.



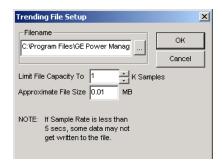
To prepare for new trending,

- Select Stop to stop the data logger and Reset to clear the screen.
- Select the graphs to be displayed through the pull-down menu beside each channel description.
- Select the Sample Rate through the pull-down menu.

If you want to save the information captured by trending,

- Check the box besides **Log Samples to File**.

 The following dialog box will appear requesting for file name and path. The file is saved as 'csv' (comma delimited values) file, which can be viewed and manipulated with compatible third-party software.
- Ensure that the sample rate is not less than 5 seconds, otherwise, some data may not get written to the file.



To limit the size of the saved file,

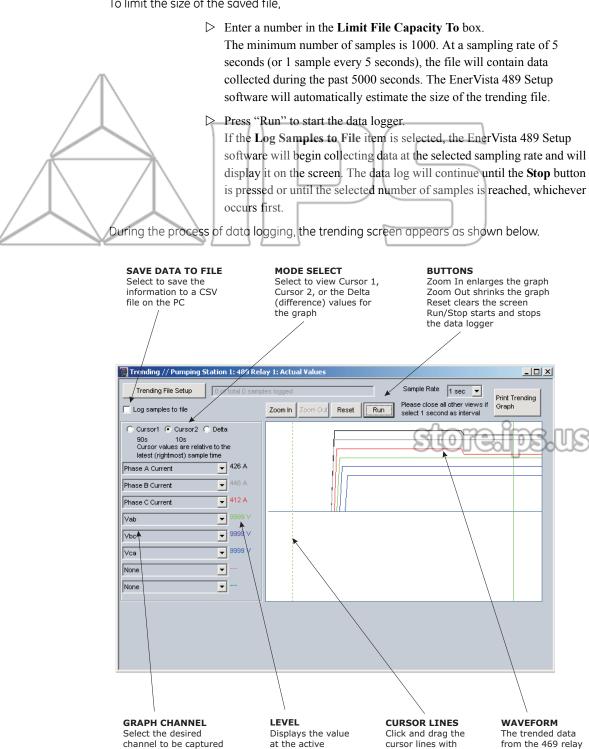


FIGURE 4-7: Trending Screen

the left mouse button

cursor line

from the pull-down menu

4.6.5 Event Recorder

The 489 event recorder can be viewed through the EnerVista 489 Setup software. The event recorder stores generator and system information each time an event occurs (e.g. breaker failure). A maximum of 256 events can be stored. Each event is assigned an event number, from E001 to E256. When the E256 is reached, E001 is assigned to the next event. Refer to Event Recorder on page 6–28 for additional information on the event recorder.

Use the following procedure to view the event recorder with EnerVista 489 Setup:

With EnerVista 489 Setup running and communications established,

Select the Actual > A4 Event Recorder item from the main menu. This displays the Event Recorder window indicating the list of recorded events, with the most current event displayed first.

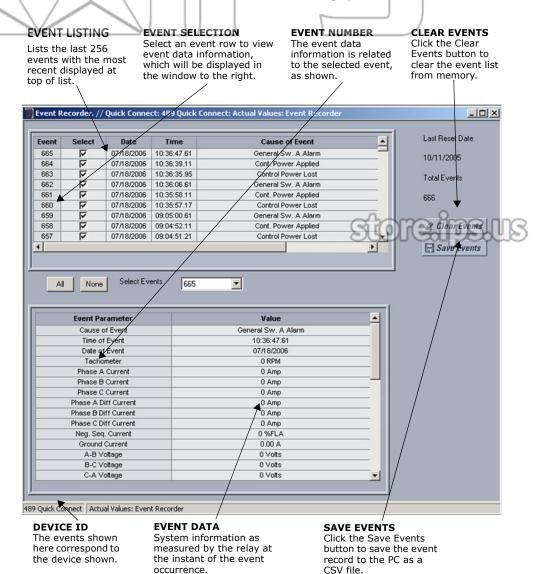


FIGURE 4-8: Event Recorder Window (shown unconnected)

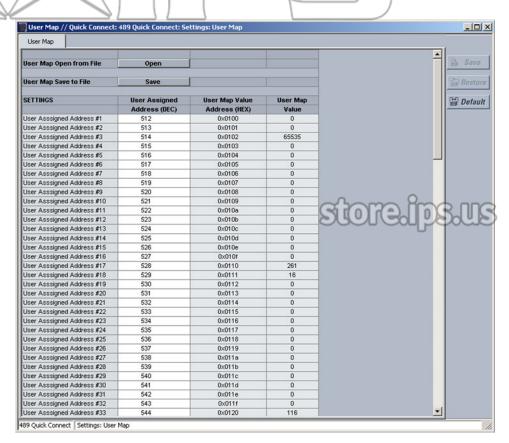
To view detailed information for a given event and the system information at the moment of the event occurrence.

Change the event number on the **Select Event** box.



The EnerVista 489 Setup software provides a means to program the 489 User Map (Modbus addresses 0180h to 01F7h). Refer to GE Publication GEK-106491: **489**Communications Guide for additional information on the User Map.

- Select a connected device in EnerVista 489 Setup.
- Select the Setpoint > User Map menu item to open the following window.



This window allows the desired addresses to be written to User Map locations. The User Map values that correspond to these addresses are then displayed.

4.6.7 Viewing Actual Values

You can view real-time relay data such as input/output status and measured parameters. From the main window menu bar, selecting Actual Values opens a window with tabs, each tab containing data in accordance with the following list:

1. Generator and System Status:

- Generator status either stopped, starting, or running. It includes values such as generator load, thermal capacity used, generator speed, and instantaneous values of power system quantities.
- The status of digital inputs.
- Last trip information, including values such as cause of last trip, time and date of trip, generator speed and load at the time of trip, pre-trip temperature measurements, pre-trip analog inputs values, and pre-trip instantaneous values of power system quantities.
- Active alarms.
- Relay date and time.
- Present blocking conditions.
- General system status indication including the status of output relays, active pickup, alarm and trip conditions.

2. **Metering Data**:

- Instantaneous current measurements including phase, differential, unbalance, ground, average, generator load, and differential currents.
- RTD Temperatures including hottest RTDs.
- Instantaneous phase to phase and phase to ground voltages (depending on the VT connections), average voltage, and system frequency.
- Generator Speed
- Power Quantities including Apparent, Real and Reactive Power.
- Current and power demand including peak values.
- Analog inputs
- Vector information.

3. Generator Learned Data:

- Average Generator Load
- Average Negative-Sequence Current
- Phase-Phase Voltage
- RTD Maximum Values

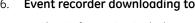
4. Maintenance data.

This is useful statistical information that may be used for preventive maintenance. It includes:

- Trip counters
- General counter such as Number of Breaker Operations.
- Timers such as Generator Running Hours.
- 5. **RTD Learned Data** includes the maximum temperature measured by each of the 12

6. Event recorder downloading tool.

- 7. Product information including model number, firmware version, additional product information, and calibration dates.
- 8. Oscillography and Data Logger downloading tool.



Selecting an actual values window also opens the actual values tree from the corresponding device in the site list and highlights the current location in the hierarchy.

For complete details on actual values, refer to Chapter 6.

To view a separate window for each group of actual values, select the desired item from the tree, and double click with the left mouse button. Each group will be opened on a separate tab. The windows can be re-arranged to maximize data viewing as shown in the following figure (showing actual current, voltage, and generator status values tiled in the same window):

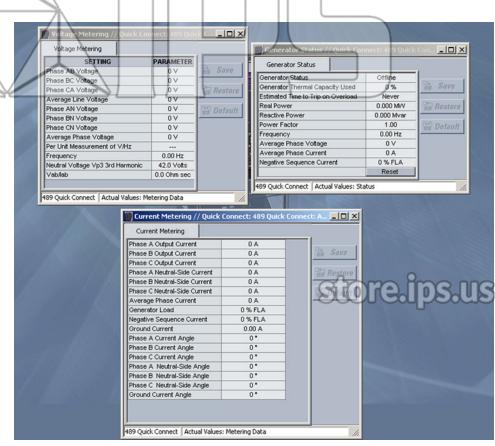


FIGURE 4-9: Actual Values Display (shown unconnected)

4.7 Using EnerVista Viewpoint with the 489

4.7.1 Plug and Play Example

EnerVista Viewpoint is an optional software package that puts critical 489 information on any PC with plug-and-play simplicity. EnerVista Viewpoint connects instantly to the 489 via serial, ethernet or modem and automatically generates detailed overview, metering, power, demand, energy and analysis screens. Installing EnerVista Launchpad (see previous section) allows the user to install a fifteen-day trial version of EnerVista Viewpoint. After the fifteen day trial period you will need to purchase a license to continue using EnerVista Viewpoint. Information on license pricing can be found at http://www.EnerVista.com.

- Install the EnerVista Viewpoint software from the GE EnerVista CD.
- Ensure that the 489 device has been properly configured for either serial or Ethernet communications (see previous sections for details).
- Click the **Viewpoint** window in EnerVista to log into EnerVista Viewpoint.

At this point, you will be required to provide a login and password if you have not already done so.



FIGURE 4-10: EnerVista Viewpoint Main Window

- Click the **Device Setup** button to open the Device Setup window.
- Click the **Add Site** button to define a new site.
- Enter the desired site name in the Site Name field.
 If desired, a short description of site can also be entered along with the display order of devices defined for the site.
- Click the **OK** button when complete. The new site will appear in the upper-left list in the EnerVista 489 Setup window
- Click the **Add Device** button to define the new device.

- Enter the desired name in the **Device Name** field and a description (optional) of the site.
- Select the appropriate communications interface (Ethernet or Serial) and fill in the required information for the 489. See *Connecting EnerVista* 489 Setup to the Relay on page 4−15 for details.

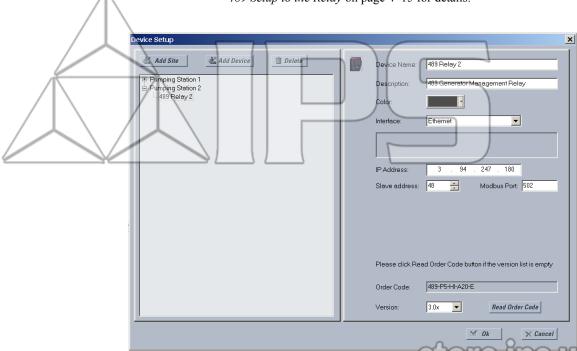


FIGURE 4-11: Device Setup Screen (Example)

- Click the Read Order Code button to connect to the 489 device and upload the order code. If an communications error occurs, ensure that communications values entered in the previous step correspond to the relay setting values.
- Click **OK** when complete.
- ▶ From the EnerVista main window, select the IED Dashboard item to open the Plug and Play IED dashboard.
 An icon for the 489 will be displayed.

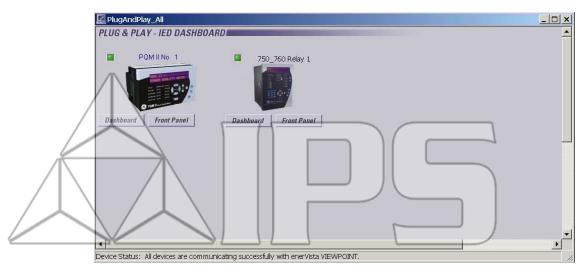


FIGURE 4–12: 'Plug and Play' Dashboard

Click the **Dashboard** button below the 489 icon to view the device information.

We have now successfully accessed our 489 through EnerVista Viewpoint.



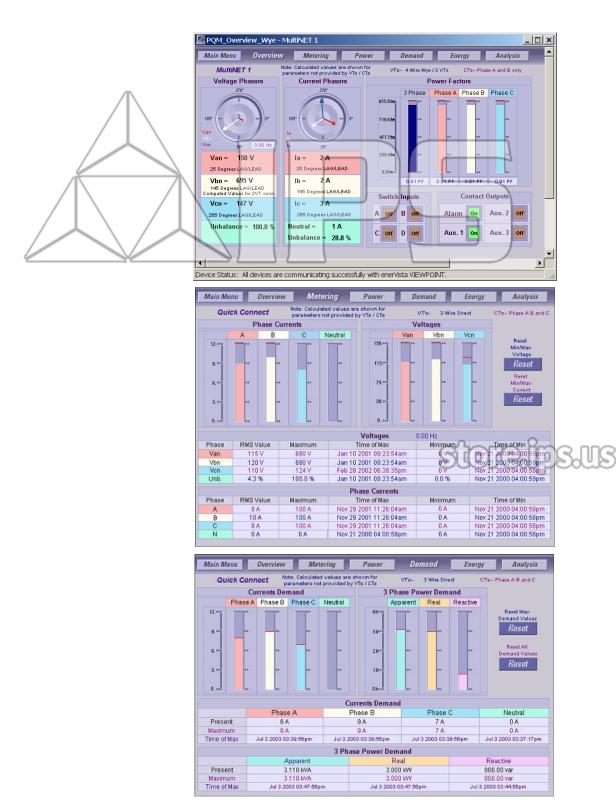


FIGURE 4-13: EnerVista Plug and Play Screens

For additional information on EnerVista viewpoint, please visit the EnerVista website at http://www.EnerVista.com.



store.ips.us

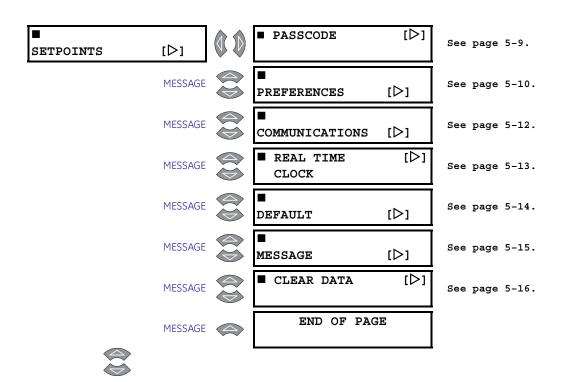


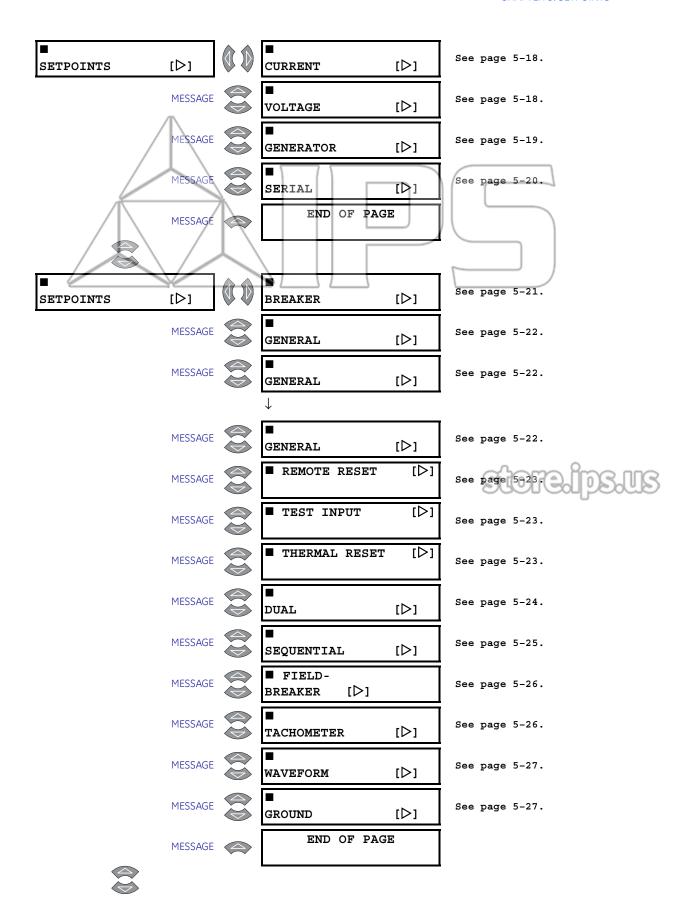


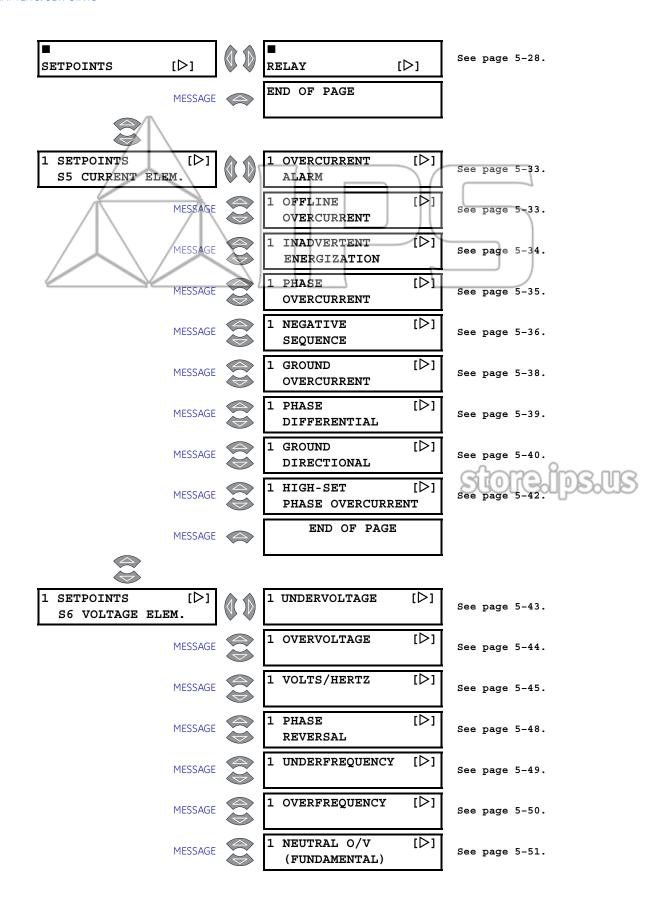
5.1 Overview

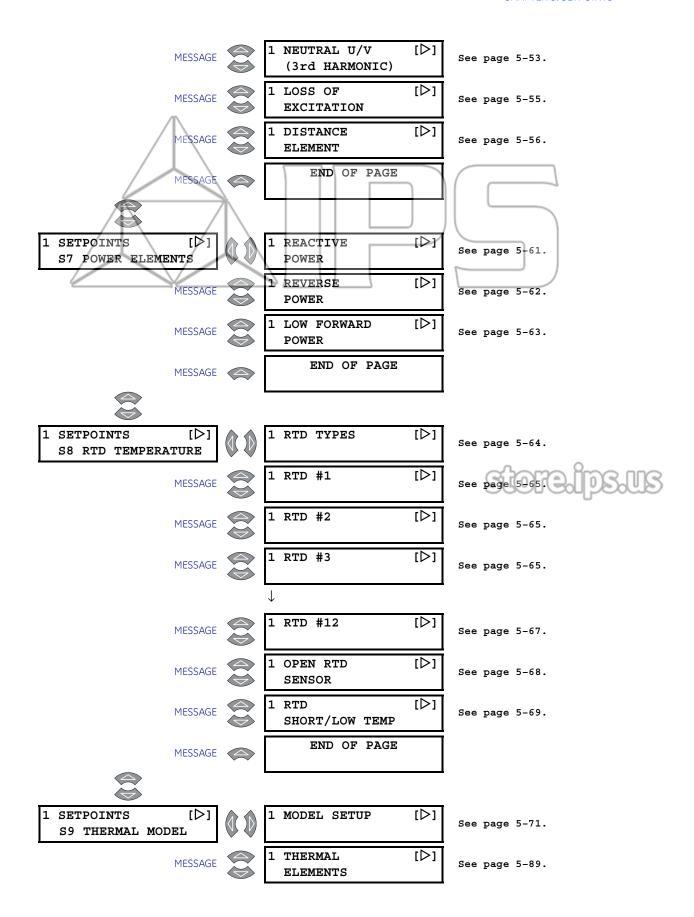
5.1.1 Setpoint Message Map

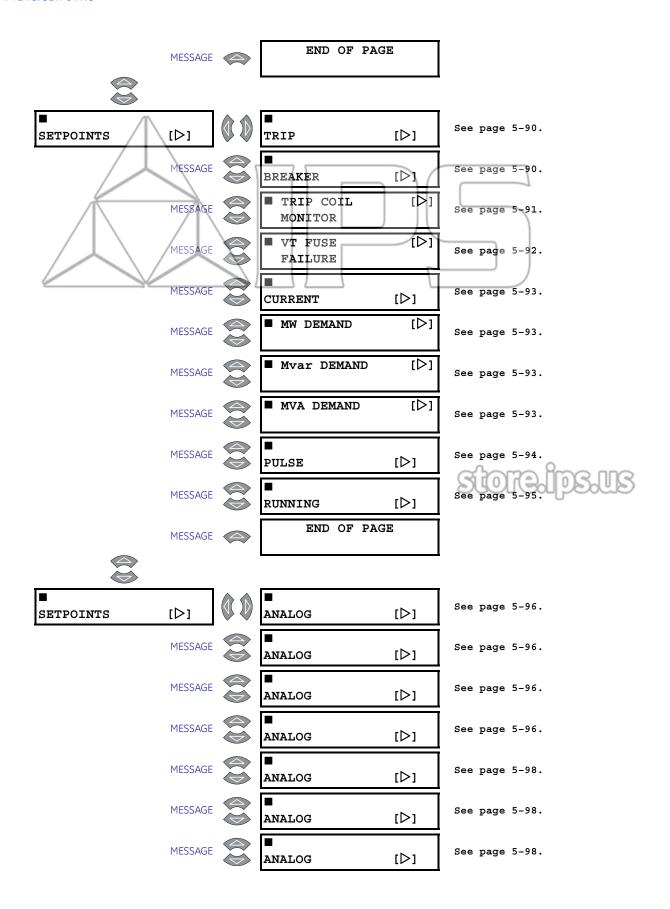
The 489 has a considerable number of programmable setpoints which makes it extremely flexible. The setpoints have been grouped into a number of pages and sub-pages as shown below. Each page of setpoints (e.g. **S2 SYSTEM SETUP**) has a section which describes in detail all the setpoints found on that page.

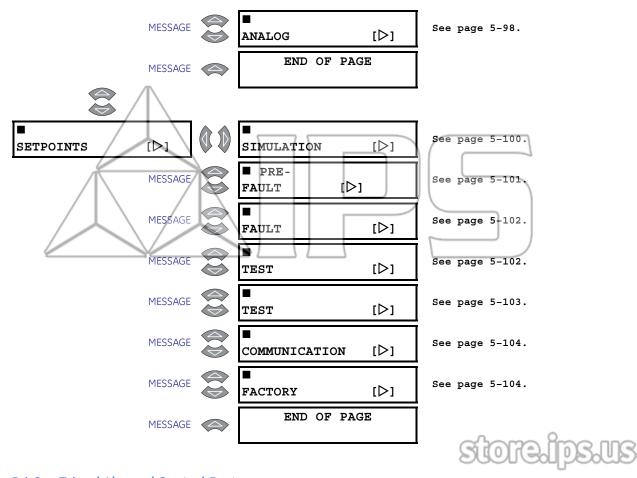












5.1.2 Trips / Alarms/ Control Features

The 489 Generator Management Relay has three basic function categories: TRIPS, ALARMS, and CONTROL.

Trips

A 489 trip feature may be assigned to any combination of the four output relays: 1 Trip, 2 Auxiliary, 3 Auxiliary, and 4 Auxiliary. If a Trip becomes active, the appropriate LED (indicator) on the 489 faceplate illuminates to indicate which output relay has operated. Each trip feature may be programmed as *latched* or *unlatched*. Once a latched trip feature becomes active, the RESET key must be pressed to reset that trip. If the condition that caused the trip is still present (for example, hot RTD) the trip relay(s) will not reset until the condition disappears. On the other hand, if an unlatched trip feature becomes active, that trip resets itself (and associated output relay(s)) after the condition that caused the trip ceases and the Breaker Status input indicates that the breaker is open. If there is a lockout time, the trip relay(s) will not reset until the lockout time has expired. Immediately prior to issuing a trip, the 489 takes a snapshot of generator parameters and stores them as pretrip values, allowing for troubleshooting after the trip. The cause of last trip message is updated with the current trip and the 489 display defaults to that message. All trip features are automatically logged and date and time stamped as they occur. In addition, all trips are counted and logged as statistics such that any long term trends may be identified.

Note that a lockout time will occur due to overload trip (see *Model Setup* on page 5–71 for additional details).

Alarms



A 489 alarm feature may be assigned to operate any combination of four output relays: 2 Auxiliary, 3 Auxiliary, 4 Auxiliary, and 5 Alarm. When an alarm becomes active, the appropriate LED (indicator) on the 489 faceplate will illuminate when an output relay(s) has operated. Each alarm feature may be programmed as latched or unlatched. Once a latched alarm feature becomes active, the reset key must be pressed to reset that alarm. If the condition that has caused the alarm is still present (for example, hot RTD) the Alarm relay(s) will not reset until the condition is no longer present. If on the other hand, an unlatched alarm feature becomes active, that alarm will reset itself (and associated output relay(s)) as soon as the condition that caused the alarm ceases. As soon as an alarm occurs, the alarms messages are updated to reflect the alarm and the 489 display defaults to that message. Since it may not be desirable to log all alarms as events, each alarm feature may be programmed to log as an event or not. If an alarm is programmed to log as an event, when it becomes active, it is automatically logged as a date and time stamped event.

Control

A 489 control feature may be assigned to operate any combination of five output relays: 1 Trip, 2 Auxiliary, 3 Auxiliary, 4 Auxiliary, and 5 Alarm. The combination of relays available for each function is determined by the suitability of each relay for that particular function. The appropriate LED (indicator) on the 489 faceplate will illuminate when an output relay(s) has been operated by a control function. Since it may not be desirable to log all control function as events, each control feature may be programmed to log as an event or not. If a control feature is programmed to log as an event, each control relay event is automatically logged with a date and time stamp.

5.1.3 Relay Assignment Practices

There are six output relays. Five of the relays are always non-failsafe, the other (Service) is failsafe and dedicated to annunciate internal 489 faults (these faults include setpoint corruption, failed hardware components, loss of control power, etc.). The five remaining relays may be programmed for different types of features depending on what is required. One of the relays, 1 Trip, is intended to be used as a trip relay wired to the unit trip breaker. Another relay, 5 Alarm, is intended to be used as the main alarm relay. The three remaining relays, 2 Auxiliary, 3 Auxiliary, and 4 Auxiliary, are intended for special requirements.

When assigning features to relays 2, 3, and 4, it is a good idea to decide early on what is required since features that may be assigned may conflict. For example, if relay 2 is to be dedicated as a relay for sequential tripping, it cannot also be used to annunciate a specific alarm condition.

In order to ensure that conflicts in relay assignments do not occur, several precautions have been taken. All trips default to the 1 Trip output relay and all alarms default to the 5 Alarm relay. It is recommended that relay assignments be reviewed once all the setpoints have been programmed.

5.1.4 Dual Setpoints

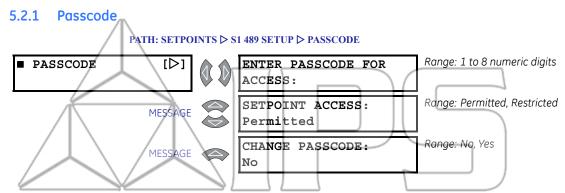
The 489 has dual settings for the current, voltage, power, RTD, and thermal model protection elements (setpoints pages S5 to S9). These setpoints are organized in two groups: the main group (Group 1) and the alternate group (Group 2). Only one group of settings is active in the protection scheme at a time. The active group can be selected using the **ACTIVATE SETPOINT GROUP** setpoint or an assigned digital input in the S3 Digital Inputs setpoints page. The LED indicator on the faceplate of the 489 will indicate when the alternate setpoints are active in the protection scheme. Independently, the setpoints in either group can be viewed and/or edited using the **EDIT SETPOINT GROUP** setpoint. Headers for each setpoint message subgroup that has dual settings will be denoted by a superscript number indicating which setpoint group is being viewed or edited. Also, when a setpoint that has dual settings is stored, the flash message that appears will indicate which setpoint group setting has been changed.

If only one setting group is required, edit and activate only Group 1 (that is, do not assign a digital input to Dual Setpoints, and do not alter the <u>ACTIVATE SETPOINT GROUP</u> setpoint or <u>EDIT SETPOINT GROUP</u> setpoint in <u>S3 DIGITAL INPUTS</u>).

5.1.5 Commissioning

Tables for recording of 489 programmed setpoints are available as a Microsoft Word document from the GE Multilin website at http://www.GEmultilin.com. See the Support Documents section of the 489 Generator Management Relay page for the latest version. This document is also available in print from the GE Multilin literature department (request publication number GET-8445).

5.2 S1 489 Setup



A passcode access security feature is provided with the 489. The passcode is defaulted to "0" (without the quotes) at the time of shipping. Passcode protection is ignored when the passcode is "0". In this case, the setpoint access jumper is the only protection when programming setpoints from the front panel keypad and setpoints may be altered using the RS232 and RS485 serial ports without access protection. If however, the passcode is changed to a non-zero value, passcode protection is enabled. The access jumper must be installed and the passcode must be entered, to program setpoints from the front panel keypad. The passcode must also be entered individually from each serial communications port to gain setpoint programming access from that port.

The ENTER PASSCODE FOR ACCESS setpoint is seen only if the passcode is not 0 and SETPOINT ACCESS is "Restricted". The SETPOINT ACCESS and CHANGE PASSWORD SETPOINT ACCESS is "Permitted".

To enable passcode protection on a new relay, follow the procedure below:

- ▶ Press ENTER then MESSAGE DOWN until CHANGE PASSCODE message is displayed.
- Select Yes and follow directions to enter a new passcode 1 to 8 digits in length.

Once a new passcode (other than "0") is programmed, it must be entered to gain setpoint access whenever setpoint access is restricted. Assuming that a non-zero passcode has been programmed and setpoint access is restricted, then selecting the passcode subgroup causes the **ENTER PASSCODE AGAIN** message to appear.

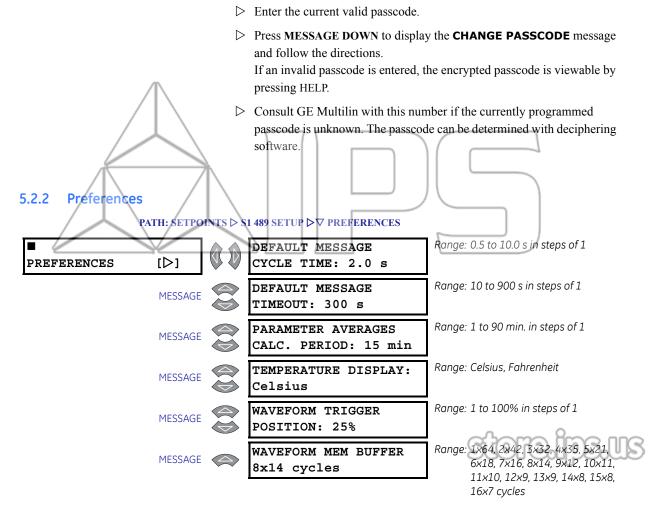
▷ Enter the correct passcode. A flash message will advise if the code is incorrect and allow a retry. If it is correct and the setpoint access jumper is installed, the SETPOINT ACCESS: Permitted message appears.

Setpoints can now be entered.

Exit the passcode message with the **ESCAPE** key and program the appropriate setpoints.

If no keypress occurs for 30 minutes, access will be disabled and the passcode must be re-entered. Removing the setpoint access jumper or setting **SETPOINT ACCESS** to **Restricted** also disables setpoint access immediately.

If a new passcode is required, gain setpoint access as follows:



Some of the 489 characteristics can be modified to suit different situations. Normally the **S1 489 SETUP** DV **PREFERENCES** setpoints group will not require any changes.

- DEFAULT MESSAGE CYCLE TIME: If multiple default messages are chosen, the display automatically cycles through these messages. The messages display time can be changed to accommodate different reading rates.
- DEFAULT MESSAGE TIMEOUT: If no keys are pressed for a period of time then the relay
 automatically scans through a programmed set of default messages. This time can be
 modified to ensure messages remain on the screen long enough during programming
 or reading of actual values.
- PARAMETER AVERAGES CALCULATION PERIOD: The period of time over which the
 parameter averages are calculated may be adjusted with this setpoint. The
 calculation is a sliding window.
- **TEMPERATURE DISPLAY:** Measurements of temperature may be displayed in either Celsius or Fahrenheit. Each actual value temperature message will be denoted by either °C for Celsius or °F for Fahrenheit. RTD setpoints are always displayed in Celsius.
- WAVEFORM TRIGGER: The trigger setpoint allows the user to adjust how many pretrip and post-trip cycles are stored in the waveform memory when a trip occurs. A

value of 25%, for example, when the **waveform memory buffer** is " 7×16 " cycles, would produce a waveform of 4 pre-trip cycles and 12 post-trip cycles.

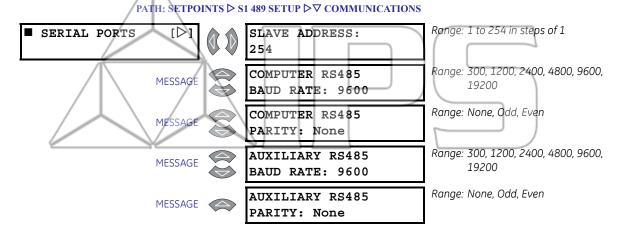
WAVEFORM MEMORY BUFFER: Selects the partitioning of the waveform memory. The first number indicates the number of events and the second number, the number of cycles. The relay captures 12 samples per cycle. When more waveform captures occur than the available storage, the oldest data will be discarded.



5.2.3 Communications

Serial Communications

The following setpoints appear when the relay is ordered with the regular enhanced (E) option.



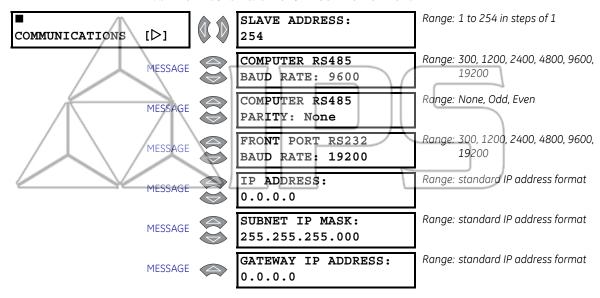
The 489 is equipped with 3 independent serial communications ports supporting a subset of Modbus RTU protocol. The front panel RS232 has a fixed baud rate of 9600 and a fixed data frame of 1 start/8 data/1stop/no parity. The front port is intended for local use only and will respond regardless of the slave address programmed. The front panel RS232 program port may be connected to a personal computer running the EnerVista 489 Setup software. This program may be used for downloading and uploading setpoint files, viewing measured parameters, and upgrading the 489 firmware to the latest revision.

For RS485 communications, each relay must have a unique address from 1 to 254. Address 0 is the broadcast address monitored by all relays. Addresses do not have to be sequential but no two units can have the same address or errors will occur. Generally, each unit added to the link will use the next higher address starting at 1. Baud rates can be selected as 300, 1200, 2400, 4800, 9600, or 19200. The data frame is fixed at 1 start, 8 data, and 1 stop bits, while parity is optional. The computer RS485 port is a general purpose port for connection to a DCS, PLC, or PC. The Auxiliary RS485 port may also be used as another general purpose port or it may be used to talk to Auxiliary GE Multilin devices in the future.

Ethernet Communications

The following setpoints appear when the relay is ordered with the Ethernet (T) option.

PATH: SETPOINTS ▷ S1 489 SETUP ▷ ♡ COMMUNICATIONS



The IP addresses are used with the Modbus protocol. Enter the dedicated IP, subnet IP, and gateway IP addresses provided by the network administrator.

To ensure optimal response from the relay, the typical connection timeout should be set as indicated in the following table:

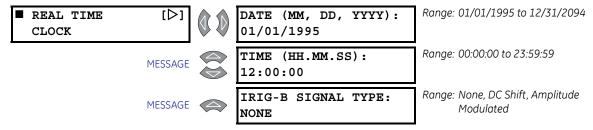
TCP/IP sessions	Timeout setting		
up to 2	2 seconds		
up to 4	3 seconds		



The RS485 COM2 port is disabled if the Ethernet option is ordered.

5.2.4 Real Time Clock

PATH: SETPOINTS ▷ S1 489 SETUP ▷▽ REAL TIME CLOCK



For events that are recorded by the event recorder to be correctly time/date stamped, the correct time and date must be entered. A battery backed internal clock runs continuously even when power is off. It has the same accuracy as an electronic watch approximately ± 1 minute per month. It must be periodically corrected either manually through the front

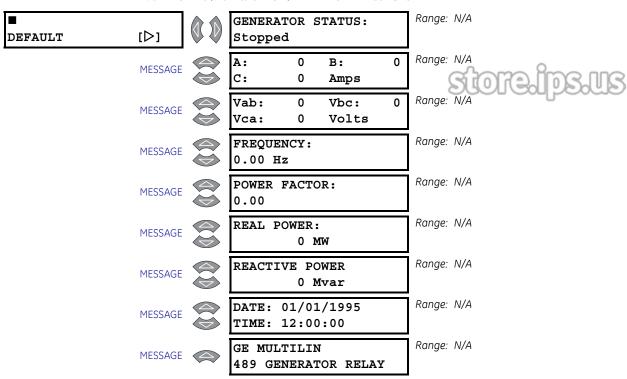
panel or via the clock update command over the RS485 serial link. If the approximate time an event occurred without synchronization to other relays is sufficient, then entry of time/date from the front panel keys is adequate.

If the RS485 serial communication link is used then all the relays can keep time in synchronization with each other. A new clock time is pre-loaded into the memory map via the RS485 communications port by a remote computer to each relay connected on the communications channel. The computer broadcasts (address 0) a "set clock" command to all relays. Then all relays in the system begin timing at the exact same instant. There can be up to 100 ms of delay in receiving serial commands so the clock time in each relay is ± 100 ms, \pm the absolute clock accuracy in the PLC or PC. See the chapter on Communications for information on programming the time preload and synchronizing commands.

An IRIG-B signal receiver may be connected to 489 units with hardware revision G or higher. The relay will continuously decode the time signal and set its internal time correspondingly. The "signal type" setpoint must be set to match the signal provided by the receiver.

5.2.5 Default Messages

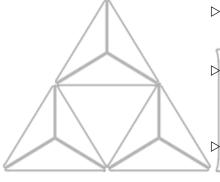
PATH: SETPOINTS ▷ S1 489 SETUP ▷ ♡ DEFAULT MESSAGES



The 489 displays default messages after a period of keypad inactivity. Up to 20 default messages can be selected for display. If more than one message is chosen, they will automatically scroll at a rate determined by the S1 489 SETUP > PREFERENCES > DEFAULT MESSAGE CYCLE TIME setpoint. Any actual value can be selected for display. In addition, up to 5 user-programmable messages can be created and displayed with the message

scratchpad. For example, the relay could be set to alternately scan a generator identification message, the current in each phase, and the hottest stator RTD. Currently selected default messages can be viewed in **DEFAULT MESSAGES** subgroup.

Default messages can be added to the end of the default message list, as follows:



- Enter the correct passcode at \$1 489 SETUP ➤ PASSCODE ➤ ENTER PASSCODE FOR ACCESS to allow setpoint entry (unless it has already been entered or is "0", defeating the passcode security feature).
- Select the message to be add to the default message list using the MESSAGE keys.

The selected message can be any actual value or message scratchpad message.

▶ Press ENTER.

The **PRESS [ENTER] TO ADD DEFAULT MESSAGES** message will be displayed for 5 seconds:

▶ Press ENTER again while this message is displayed to add the current message to the end of the default message list.

If the procedure was followed correctly, the **DEFAULT MESSAGE HAS BEEN ADDED** flash message is displayed:

Do verify that the message was added, view the last message under the S1 489 SETUP D⊽ DEFAULT MESSAGES menu.

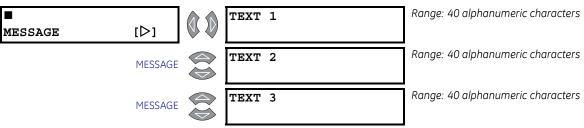
Default messages can be removed from the default message list, as follows:

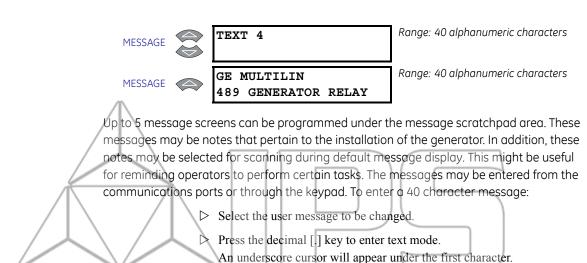
- Enter the correct passcode at \$1 489 SETUF ➤ PASSCODE ➤ ENTER PASSCODE FOR ACCESS to allow setpoint entry (unless the passcode has already been entered or unless the passcode is "0" defeating the passcode security feature).
- Select the message to remove from the default message list under the S1 489 SETUP ▷ ▼ DEFAULT MESSAGES menu.
- Select the default message to remove and press ENTER.
 The relay will display PRESS [ENTER] TO REMOVE MESSAGE.
- ▶ Press ENTER while this message is displayed to remove the current message out of the default message list.

If the procedure was followed correctly, the **DEFAULT MESSAGE HAS BEEN REVOVED** flash message is displayed.

5.2.6 Message Scratchpad

PATH: SETPOINTS \triangleright S1 489 SETUP $\triangleright \nabla$ MESSAGE SCRATCHPAD





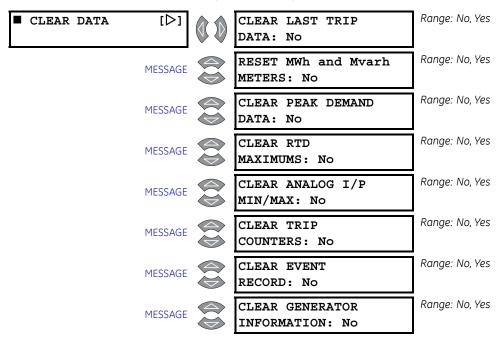
- Use the VALUE keys to display the desired character.

 A space is selected like a character.
- Press the [.] key to advance to the next character.
 To skip over a character press the [.] key.
 If an incorrect character is accidentally stored, press the [.] key enough times to scroll the cursor around to the character.
- ▶ When the desired message is displayed press the ENTER key to store or the ESCAPE key to abort.
- The message is now permanently stored.

 Press ESCAPE to cancel the altered message.

5.2.7 Clear Data

PATH: SETPOINTS ▷ S1 489 SETUP ▷▽ CLEAR DATA



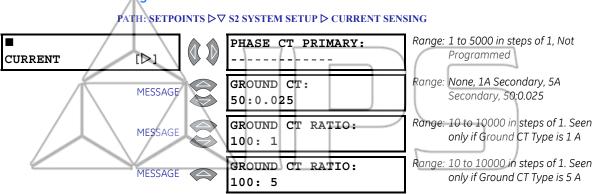
MESSAGE CLEAR BREAKER
INFORMATION: No

These commands may be used to clear various historical data.

- CLEAR LAST TRIP DATA: The Last Trip Data may be cleared by executing this
 command.
- **CLEAR MWh and Mvarh METERS:** Executing this command will clear the MWh and Mvarh metering to zero.
- CLEAR PEAK DEMAND DATA: Execute this command to clear peak demand values.
- CLEAR RTD MAXIMUMS: All maximum RTD temperature measurements are stored and updated each time a new maximum temperature is established. Execute this command to clear the maximum values.
- CLEAR ANALOG I/P MIN/MAX: The minimum and maximum analog input values are stored for each Analog Input. Those minimum and maximum values may be cleared at any time.
- **CLEAR TRIP COUNTERS:** There are counters for each possible type of trip. Those counters may be cleared by executing this command.
- **CLEAR EVENT RECORD:** The event recorder saves the last 256 events, automatically overwriting the oldest event. If desired, all events can be cleared using this command to prevent confusion with old information.
- CLEAR GENERATOR INFORMATION: The number of thermal resets and the total generator running hours can be viewed in actual values. On a new installation, or if new equipment is installed, this information is cleared through this setpoint.
- CLEAR BREAKER INFORMATION: The total number of breaker operations can be viewed in actual values. On a new installation or if maintenance work is done on the breaker, this accumulator can be cleared with this setpoint.

5.3 S2 System Setup

5.3.1 Current Sensing



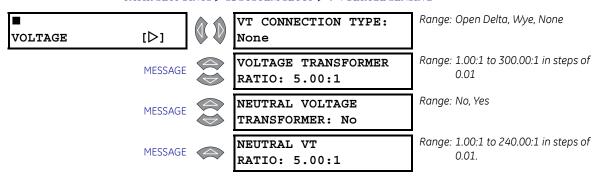
As a safeguard, the **PHASE CT PRIMARY** and **GENERATOR PARAMETERS** setpoints are defaulted to "-----" when shipped, indicating that the 489 was never programmed. Once these values are entered, the 489 will be in service. Select the Phase CT so that the maximum fault current does not exceed 20 times the primary rating. When relaying class CTs are purchased, this precaution helps prevent CT saturation under fault conditions. The secondary value of 1 or 5 A **must** be specified when ordering so the proper hardware will be installed. The **PHASE CT PRIMARY** setpoint applies to both the neutral end CTs as well as the output CTs.

For high resistance grounded systems, sensitive ground current detection is possible if the 50:0.025 Ground CT is used. To use the 50:0.025 CT input, set **GROUND CT** to "50:0.025". No additional ground CT messages will appear. On solid or low resistance grounded systems, where fault currents may be quite large, the 489 1 A/5 A secondary Ground CT input should be used. Select the Ground CT primary so that potential fault current does not exceed 20 times the primary rating. When relaying class CTs are purchased, this precaution will ensure that the Ground CT does not saturate under fault conditions.

The 489 uses a nominal CT primary rating of 5 A for calculation of pickup levels.

5.3.2 Voltage Sensing

PATH: SETPOINTS ▷ S2 SYSTEM SETUP ▷▽ VOLTAGE SENSING





The NEUTRAL VT RATIO setpoint is seen only if NEUTRAL VOLTAGE TRANSFORMER setpoint is "Yes".

The voltage transformer connections and turns ratio are entered here. The VT should be selected such that the secondary phase-phase voltage of the VTs is between 70.0 and 135.0 V when the primary is at generator rated voltage.

The Neutral VT ratio must be entered here for voltage measurement across the neutral grounding device. Note that the neutral VT input is not intended to be used at continuous voltages greater than 240 V. If the voltage across the neutral input is less than 240 V during fault conditions, an auxiliary voltage transformer is not required. If this is not the case, use an auxiliary VT to drop the fault voltage below 240 V. The NEUTRAL VT RATIO entered must be the total effective ratio of the grounding transformer and any auxiliary step up or step down VT.

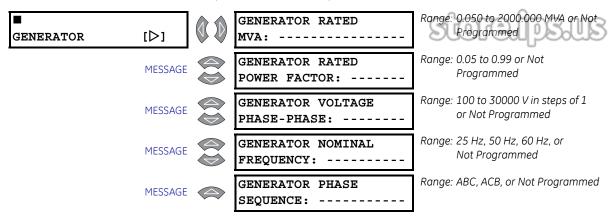
For example, if the distribution transformer ratio is 13200:480 and the auxiliary VT ratio is 600:120, the **NEUTRAL VT RATIO** setpoint is calculated as:

NEUTRAL VT RATIO = Distribution Transformer Ratio × Auxiliary VT Ratio : 1
=
$$\frac{13200}{480} \times \frac{600}{120}$$
 : 1 = 137.50 : 1
(EQ 0.1)

Therefore, set **NEUTRAL VT RATIO** to 137.50:1

5.3.3 Generator Parameters

PATH: SETPOINTS ▷ ♥ S2 SYSTEM SETUP ▷ ♥ GENERATOR PARAMETERS



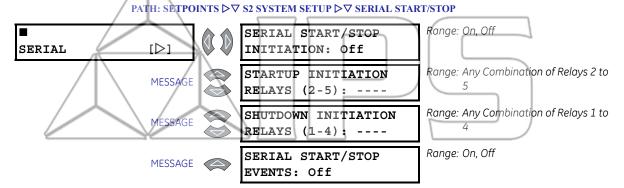
As a safeguard, when a unit is received from the factory, the **PHASE CT PRIMARY** and Generator Parameters setpoints will be defaulted to "------", indicating they are not programmed. The 489 indicates that it was never programmed. Once these values are entered, the 489 will be in service. All elements associated with power quantities are programmed in per unit values calculated from the rated MVA and power factor. The generator full load amps (FLA) is calculated as

Generator FLA =
$$\frac{\text{Generator Rated MVA}}{\sqrt{3} \times \text{Generator Rated Phase-Phase Voltage}}$$
 (EQ 0.2)

All voltage protection features that require a level setpoint are programmed in per unit of the rated generator phase-phase voltage. The nominal system frequency must be entered here. This setpoint allows the 489 to determine the internal sampling rate for maximum accuracy. If the sequence of phase rotation for a given system is ACB rather than the

standard ABC, the system phase sequence setpoint may be used to accommodate this rotation. This setpoint allows the 489 to properly calculate phase reversal and negative sequence quantities.

5.3.4 Serial Start/Stop Initiation



If enabled, this feature will allow the user to initiate a generator startup or shutdown via the RS232/RS485 communication ports. Refer to GE publication number GEK-106495: 489 *Communications Guide* for command formats. When a startup command is issued, the auxiliary relay(s) assigned for starting control will be activated for 1 second to initiate startup. When a stop command is issued, the assigned relay(s) will be activated for 1 second to initiate a shutdown.



5.4 S3 Digital Inputs

5.4.1 Description

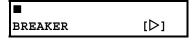
The 489 has nine (9) digital inputs for use with external contacts. Two of the 489 digital inputs have been pre-assigned as inputs having a specific function. The Access Switch does not have any setpoint messages associated with it. The Breaker Status input, may be configured for either an 'a' or 'b' auxiliary contact. The remaining seven digital inputs are assignable; that is to say, each input may be assigned to any of a number of different functions. Some of those functions are very specific, others may be programmed to adapt to user requirements.



Terminals C1 and C2 *must* be shorted to allow changing of any setpoint values from the front panel keypad. This safeguard is in addition to the setpoint passcode feature, which functions independently (see the si 489 SETUP \triangleright PASSCODE menu). The access switch has no effect on setpoint programming from the RS232 and RS485 serial communications ports.

5.4.2 Breaker Status

PATH: SETPOINTS ▷ ♥ S3 DIGITAL INPUTS ▷ BREAKER STATUS





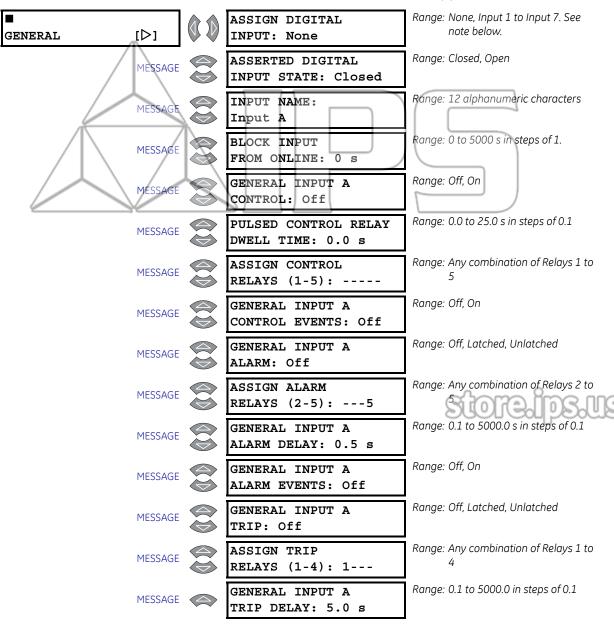
BREAKER STATUS: Breaker Auxiliary b Range: Breaker Auxiliary a, Breaker Auxiliary b



This input is necessary for all installations. The 489 determines when the generator is online or offline based on the Breaker Status input. Once 'Breaker Auxiliary a' is chosen, terminals C3 and C4 will be monitored to detect the state of the machine main breaker, open signifying the breaker is open and shorted signifying the breaker is closed. Once "Breaker Auxiliary b" is chosen, terminals C3 and C4 will be monitored to detect the state of the breaker, shorted signifying the breaker is open and open signifying the breaker is closed.

5.4.3 General Input A to G

PATH: SETPOINTS ▷∇ S3 DIGITAL INPUTS ▷∇ GENERAL INPUT A(G)





If an input is assigned to the Tachometer function, it may not be assigned via the **ASSIGN DIGITAL INPUT** setpoint.

The seven General Input functions are flexible enough to meet most of the desired digital input requirements. The asserted state and the name of the digital inputs are programmable. To disable the input functions when the generator is offline, until some time after the generator is brought online, a block time should be set. The input functions will be enabled once the block delay has expired. A value of "0 s" for the **BLOCK INPUT FROM ONLINE** block time indicates that the input functions are always enabled while the generator is offline as well as online.

Inputs may be configured for control, alarm, or trip. If the control feature is enabled, the assigned output relay(s) operate when the input is asserted. If the PULSED CONTROL RELAY DWELL TIME is set to "0", the output relay(s) operate only while the input is asserted. However, if a dwell time is assigned, the output relay(s) operate as soon as the input is asserted for a period of time specified by the setpoint. If an alarm or trip is enabled and the input is asserted, an alarm or trip will occur after the specified delay.



Once an input is assigned to the Remote Reset function, shorting that input will reset any latched trips or alarms that may be active, provided that any thermal lockout time has expired and the condition that caused the alarm or trip is no longer present.

If an input is assigned to the tachometer function, it may not be used here.

5.4.5 Test Input

PATH: SETPOINTS ▷▽ S3 DIGITAL INPUTS ▷▽ TEST INPUT



Once the 489 is in service, it may be tested from time to time as part of a regular maintenance schedule. The unit will have accumulated statistical information relating historically to generator and breaker operation. This information includes: last trip data, peak demand data, MWh and Mvarh metering, parameter averages, RTD maximums, analog input minimums and maximums, number of trips, number of trips by type, number of breaker operations, the number of thermal resets, total generator running hours, and the event record. When the unit is under test and one of the inputs is assigned to the Test Input function, shorting that input will prevent all of this data from being corrupted or updated.

If an input is assigned to the tachometer function, it may not be used here.

5.4.6 Thermal Reset

PATH: SETPOINTS $\triangleright \nabla$ S3 DIGITAL INPUTS $\triangleright \nabla$ THERMAL RESET

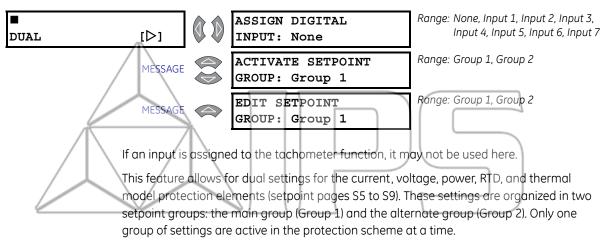


During testing or in an emergency, it may be desirable to reset the thermal memory used to zero. If an input is assigned to the Thermal Reset function, shorting that input will reset the thermal memory used to zero. All Thermal Resets will be recorded as events.

If an input is assigned to the tachometer function, it may not be used here.

5.4.7 **Dual Setpoints**

PATH: SETPOINTS $\triangleright \nabla$ S3 DIGITAL INPUTS $\triangleright \nabla$ DUAL SETPOINTS



When accessing the Group 2 setpoints, the block character (**a**) for the setpoints menu header will be replaced by the number two (**2**) as indicated below.

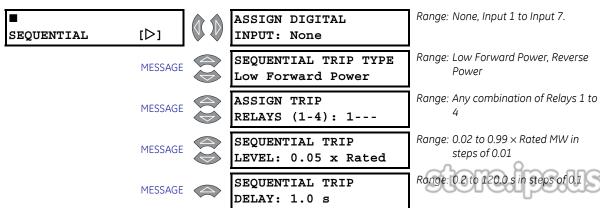
The following chart illustrates the available Group 2 (alternate group) setpoints

2 SETPOINTS [>] S5 CURRENT ELEM.	2 SETPOINTS [>] S6 VOLTAGE ELEM.	2 SETPOINTS [>] S7 POWER ELEMENTS	2 SETPOINTS [>] S8 RTD TEMPERA- TURE	2 SETPOINTS [D] S9 THERMAL MODEL
2 OVERCURRENT [>] ALARM	2 UNDERVOLTAGE [>]	2 REACTIVE [D] POWER	2 RTD [▷]	2 MODEL [D] SETUP
2 OFFLINE [>] OVERCURRENT	2 OVERVOLTAGE [▷]	2 REVERSE [▷] POWER	2 RTD #1 [▷]	2 THERMAL [D] ELEMENTS
2 INADVERTENT [>] ENERGIZATION	2 VOLTS/HERTZ [▷]	2 LOW [>] FORWARD POWER	\downarrow	
2 PHASE [D] OVERCURRENT	2 PHASE [>] REVERSAL		2 RTD #12 [▷]	
2 NEGATIVE [D] SEQUENCE	2 UNDERFREQUENCY [▷]		2 OPEN [▷] RTD SENSOR	
2 GROUND [>] OVERCURRENT	2 OVERFREQUENCY [>]		2 RTD [▷] SHORT/LOW TEMP	
2 PHASE [D] DIFFERENTIAL	2 NEUTRAL [▷] OVERVOLTAGE (Fund)			
2 GROUND [▷] DIRECTIONAL	2 NEUTRAL U/ V [▷] (3rd HARMONIC)			
2 HIGH-SET [>] PHASE OVERCURRENT	2 LOSS [>] OF EXCITATION			
	2 DISTANCE [>] ELEMENT			

The active group can be selected using the **ACTIVATE SETPOINT GROUP** setpoint or the assigned digital input (shorting that input will activate the alternate set of protection setpoints, Group 2). In the event of a conflict between the **ACTIVATE SETPOINT GROUP** setpoint or the assigned digital input, Group 2 will be activated. The LED indicator on the faceplate of the 489 will indicate when the alternate setpoints are active in the protection scheme. Changing the active setpoint group will be logged as an event. Independently, the setpoints in either group can be viewed and/or edited using the **EDIT SETPOINT GROUP** setpoint. Headers for each setpoint message subgroup that has dual settings will be denoted by a superscript number indicating which setpoint group is being viewed or edited. Also, when a setpoint that has dual settings is stored, the flash message that appears will indicate which setpoint group setting has been changed.

5.4.8 Sequential Trip

PATH: SETPOINTS ▷∇ S3 DIGITAL INPUTS ▷∇ SEQUENTIAL TRIP



If an input is assigned to the tachometer function, it may not be used here.

During routine shutdown and for some less critical trips, it may be desirable to use the sequential trip function to prevent overspeed. If an input is assigned to the sequential trip function, shorting that input will enable either a low forward power or reverse power function. Once the measured 3-phase total power falls below the low forward power level, or exceeds the reverse power level for the period of time specified, a trip will occur. This time delay will typically be shorter than that used for the standard reverse power or low forward power elements. The level is programmed in per unit of generator rated MW calculated from the rated MVA and rated power factor. If the VT type is selected as None, the sequential trip element will operate as a simple timer. Once the input has been shorted for the period of time specified by the delay, a trip will occur.

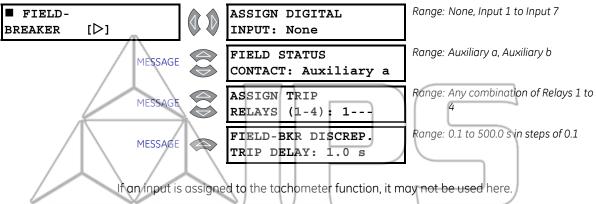


The minimum magnitude of power measurement is determined by the phase CT minimum of 2% rated CT primary. If the level for reverse power is set below that level, a trip will only occur once the phase current exceeds the 2% cutoff.

Users are cautioned that a reverse power element may not provide reliable indication when set to a very low setting, particularly under conditions of large reactive loading on the generator. Under such conditions, low forward power is a more reliable element.

5.4.9 Field-Breaker

PATH: SETPOINTS ▷ ♥ S3 DIGITAL INPUTS ▷ ♥ FIELD-BREAKER DISCREPANCY



The field-breaker discrepancy function is intended for use with synchronous generators. If a digital input is assigned to this function, any time the field status contact indicates the field is not applied and the breaker status input indicates that the generator is online, a trip will occur once the time delay has expired. The time delay should be used to prevent possible nuisance tripping during shutdown. The field status contact may be chosen as "Auxiliary a", open signifying the field breaker or contactor is open and shorted signifying the field breaker or contact may be chosen as "Auxiliary b", shorted signifying the field breaker or contactor is open and open signifying it is closed.

5.4.10 Tachometer



PATH: SETPOINTS ▷▽ S3 DIGITAL INPUTS ▷▽ TACHOMETER

			, , , , , , , , , , , , , , , , , , , ,	
■ TACHOMETER	[▷]	1	ASSIGN DIGITAL INPUT: None	Range: None, Inputs 4 to 7.
	MESSAGE		RATED SPEED: 3600 RPM	Range: 100 to 3600 RPM in steps of 1
	MESSAGE		TACHOMETER ALARM: Off	Range: Off, Latched, Unlatched
	MESSAGE		ASSIGN ALARM RELAYS (2-5):5	Range: Any combination of Relays 2 to 5
	MESSAGE		TACHOMETER ALARM SPEED: 110% Rated	Range: 101 to 175% in steps of 1
	MESSAGE		TACHOMETER ALARM DELAY: 1 s	Range: 1 to 250 s in steps of 1
	MESSAGE		TACHOMETER ALARM EVENTS: Off	Range: On, Off
	MESSAGE		TACHOMETER TRIP: Off	Range: Off, Latched, Unlatched
	MESSAGE		ASSIGN TRIP RELAYS (1-4): 1	Range: Any combination of Relays 1 to 4

MESSAGE

TACHOMETER TRIP
SPEED: 110% Rated

Range: 101 to 175% in steps of 1

Range: 1 to 250 s in steps of 1

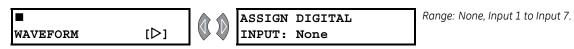
Range: 1 to 250 s in steps of 1

One of assignable digital inputs 4 to 7 may be assigned to the tachometer function to measure mechanical speed. The time between each input closure is measured and converted to an RPM value based on one closure per revolution. If an overspeed trip or alarm is enabled, and the measured RPM exceeds the threshold setpoint for the time specified by the delay, a trip or alarm will occur. The RPM value can be viewed with the A2 METERING DATA $\triangleright \nabla$ Speed $\triangleright \nabla$ Tachometer actual value.

For example, an inductive proximity probe or hall effect gear tooth sensor may be used to sense the key on the generator. The probe could be powered from the +24V from the digital input power supply. The NPN transistor output could be taken to one of the assignable digital inputs assigned to the tachometer function.

5.4.11 Waveform Capture

PATH: SETPOINTS ▷▽ S3 DIGITAL INPUTS ▷▽ WAVEFORM CAPTURE

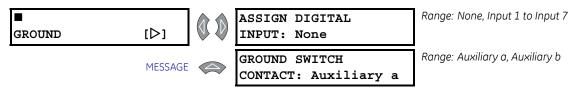


If an input is assigned to the tachometer function, it may not be used here.

This feature may be used to trigger the waveform capture from an external contact. When one of the inputs is assigned to the Waveform Capture function, shorting that input will trigger the waveform.

5.4.12 Ground Switch Status

PATH: SETPOINTS ▷ ♥ S3 DIGITAL INPUTS ▷ ♥ GND SWITCH STATUS



If an input is assigned to the tachometer function, it may not be used here.

This function is used to detect the status of a grounding switch for the generator for which the relay is installed. Refer to *Stator Ground Fault* on page A–1 for additional details.

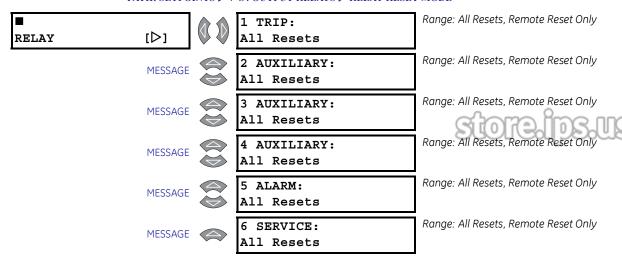
5.5 S4 Output Relays

5.5.1 Description

Five of the six output relays are always non-failsafe; the 6 Service relay is always failsafe. As a failsafe, the 6 Service relay will be energized normally and de-energize when called upon to operate. It will also de-energize when control power to the 489 is lost and therefore, be in its operated state. All other relays, being non-failsafe, will be de-energized normally and energize when called upon to operate. Obviously, when control power is lost to the 489, the output relays must be de-energized and therefore, they will be in their non-operated state. Shorting bars in the drawout case ensure that when the 489 is drawn out, no trip or alarm occurs. The 6 Service output will however indicate that the 489 has been drawn out.

5.5.2 Relay Reset Mode

PATH: SETPOINTS ▷ ♥ S4 OUTPUT RELAYS ▷ RELAY RESET MODE



Unlatched trips and alarms will reset automatically once the condition is no longer present. Latched trip and alarm features may be reset at any time, providing that the condition that caused the trip or alarm is no longer present and any lockout time has expired. If any condition may be reset, the Reset Possible LED will be lit. The relays may be programmed to All Resets which allows reset from the front keypad or the remote reset digital input or the communications port. Optionally, they may be programmed to reset by the Remote Reset Only (by the remote reset digital input or the communications port).

For example, selected trips such as Instantaneous Overcurrent and Ground Fault may be assigned to output relay 2 so that they may only be reset via. the Remote Reset digital input or the communication port. The Remote Reset terminals would be connected to a keyswitch so that only authorized personnel could reset such a critical trip.

- Assign only Short Circuit and Ground Fault to relay 2.
- Program relay 2 to Remote Reset Only.

5.6 S5 Current Elements

5.6.1 Inverse Time Overcurrent Curve Characteristics

Description

The 489 inverse time overcurrent curves may be either ANSI, IEC, or GE Type IAC standard curve shapes. This allows for simplified coordination with downstream devices. If however, none of these curve shapes is adequate, the FlexCurve $^{\text{TM}}$ may be used to customize the inverse time curve characteristics. Definite time is also an option that may be appropriate if only simple protection is required.

Table 5-1: 489 Overcurrent Curve Types

ANSI	IEC	GE Type IAC	Other	
Extremely Inverse	Curve A (BS142)	Extremely Inverse	FlexCurve™	
Very Inverse	Curve B (BS142)	Very Inverse	Definite Time	
Normally Inverse	Curve C (BS142)	Inverse		
Moderately Inverse	Short Inverse	Short Inverse		

A multiplier setpoint allows selection of a multiple of the base curve shape that is selected with the curve shape setpoint. Unlike the electromechanical time dial equivalent, trip times are directly proportional to the time multiplier setting value. For example, all trip times for a multiplier of 10 are 10 times the multiplier 1 or base curve values. Setting the multiplier to zero results in an instantaneous response to all current levels above pickup.



Regardless of the trip time that results from the curve multiplier setpoint, the 489 cannot trip any quicker than one to two cycles plus the operate time of the output relay.

Time overcurrent tripping time calculations are made with an internal "energy capacity" memory variable. When this variable indicates that the energy capacity has reached 100%, a time overcurrent trip is generated. If less than 100% is accumulated in this variable and the current falls below the dropout threshold of 97 to 98% of the pickup value, the variable must be reduced. Two methods of this resetting operation are available, "Instantaneous" and "Linear". The Instantaneous selection is intended for applications with other relays, such as most static units, which set the energy capacity directly to zero when the current falls below the reset threshold. The Linear selection can be used where the 489 must coordinate with electromechanical units. With this setting, the energy capacity variable is decremented according to the following equation.

$$T_{RESET} = \frac{E \times M \times C_R}{100}$$
 (EQ 0.3)

where: T_{RESET} = reset time in seconds

E = energy capacity reached (in %)

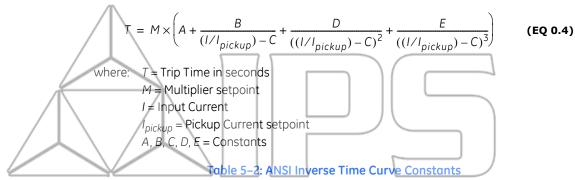
M = curve multiplier

C_R= characteristic constant (5 for ANSI, IAC, Definite Time and FlexCurves™, 8 for

IEC curves)

ANSI Curves

The ANSI time overcurrent curve shapes conform to industry standard curves and fit into the ANSI C37.90 curve classifications for extremely, very, normally, and moderately inverse. The 489 ANSI curves are derived from the formula:



ANSI Curve Shape	Constants					
	A	В	С	D	E	
Extremely Inverse	0.0399	0.2294	0.5000	3.0094	0.7222	
Very Inverse	0.0615	0.7989	0.3400	-0.2840	4.0505	
Normally Inverse	0.0274	2.2614	0.3000	-4.1899	9.1272	
Moderately Inverse	0.1735	0.6791	0.8000	-0.0800	0.1271	

IEC Curves

For European applications, the relay offers the four standard curves defined in IEC 255-4 and British standard BS142. These are defined as IEC Curve A, IEC Curve B, IEC Curve C, and Short Inverse. The formula for these curves is:

$$T = M \times \left(\frac{K}{(I/I_{pickup})^{E} - 1}\right)$$
 (EQ 0.5)

where: T = Trip Time in seconds

M = Multiplier setpoint

I = Input Current

 I_{pickup} = Pickup Current setpoint

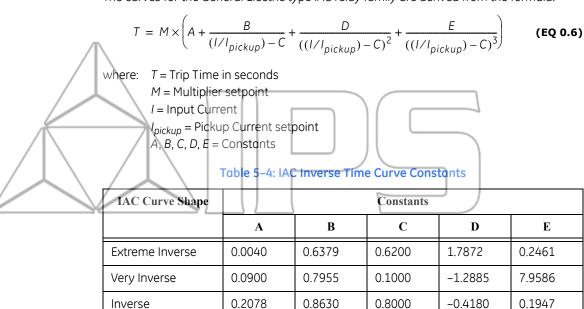
K, E = Constants

Table 5-3: IEC (BS) Inverse Time Curve Constants

IEC (BS) Curve Shape	Constants		
	K	E	
IEC Curve A (BS142)	0.140	0.020	
IEC Curve B (BS142)	13.500	1.000	
IEC Curve C (BS142)	80.000	2.000	
Short Inverse	0.050	0.040	

IAC Curves

The curves for the General Electric type IAC relay family are derived from the formula:



FlexCurve™

Short Inverse

The custom FlexCurve™ has setpoints for entering times to trip at the following current levels: 1.03, 1.05, 1.1 to 6.0 in steps of 0.1 and 6.5 to 20.0 in steps of 0.5. The relay then converts these points to a continuous curve by linear interpolation between data points. To enter a custom FlexCurve™, read off each individual point from a time overcurrent coordination drawing and enter it into a table as shown. Then transfer each individual point to the 489 using either the EnerVista 489 Setup software or the front panel keys and display.

0.0609

0.0428

0.6200

-0.0010

0.0221

Table 5–5: FlexCurve™ Trip Times

					7 111100		
Pickup I/I _{pkp}	Trip Time (ms)						
1.03		2.9		4.9		10.5	
1.05		3.0		5.0		11.0	
1.1		3.1		5.1		11.5	
1.2		3.2		5.2		12.0	
1.3		3.3		5.3		12.5	
1,4		3.4		5.4		13.0	
1.5		3.5		5.5		13.5	
1.6		3.6		5.6		14.0	
1.7		3.7		5.7		14.5	
1.8		3.8		5.8		15.0	
1.9		3.9		5.9		15.5	
2.0		4.0		6.0		16.0	
2.1		4.1		6.5	~5	16.5	8
2.2		4.2		7.0	SU	17.0	
2.3		4.3		7.5		17.5	
2.4		4.4		8.0		18.0	
2.5		4.5		8.5		18.5	
2.6		4.6		9.0		19.0	
2.7		4.7		9.5		19.5	
2.8		4.8		10.0		20.0	
		-					

Definite Time Curve

The definite time curve shape causes a trip as soon as the pickup level is exceeded for a specified period of time. The base definite time curve delay is 100 ms. The curve multiplier of 0.00 to 1000.00 makes this delay adjustable from instantaneous to 100.00 seconds in steps of 1 ms.

$$T = M \times 100 \text{ ms}, \text{ when } I > I_{pickup}$$
 (EQ 0.7)

where: T = Trip Time in seconds

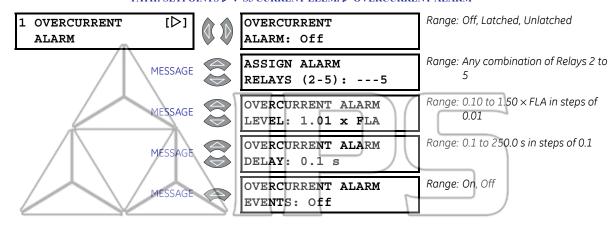
M = Multiplier Setpoint

I = Input Current

 I_{pickup} = Pickup Current Setpoint

5.6.2 Overcurrent Alarm

PATH: SETPOINTS ▷ ♥ S5 CURRENT ELEM. ▷ OVERCURRENT ALARM



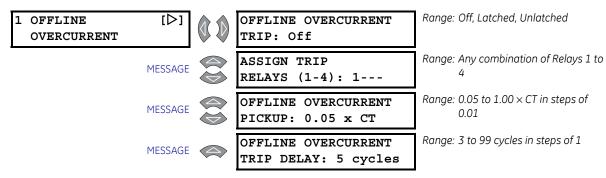
If enabled as Latched or Unlatched, the Overcurrent Alarm will function as follows: If the average generator current (RMS) measured at the output CTs exceeds the level programmed for the period of time specified, an alarm will occur. If programmed as unlatched, the alarm will reset itself when the overcurrent condition is no longer present. If programmed as latched, once the overcurrent condition is gone, the reset key must be pressed to reset the alarm. The generator FLA is calculated as:

Generator FLA =
$$\frac{\text{Generator Rated MVA}}{\sqrt{3} \times \text{Generator Rated Phase-Phase Voltage}}$$
 (EQ 0.8)

5.6.3 Offline Overcurrent

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PATH: SETPOINTS ▷▽ S5 CURRENT ELEM. ▷▽ OFFLINE OVERCURRENT



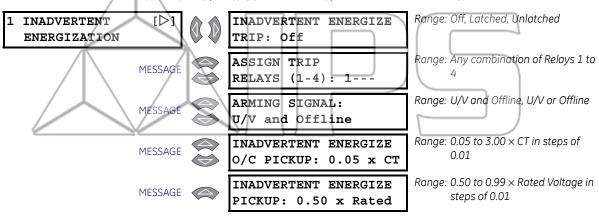
When a synchronous generator is offline, there should be no measurable current flow in any of the three phases unless the unit is supplying its own station load. Also, since the generator is not yet online, differentiation between system faults and machine faults is easier. The offline overcurrent feature is active only when the generator is offline and uses the neutral end CT measurements (Ia, Ib, Ic). It may be set much more sensitive than the differential element to detect high impedance phase faults. Since the breaker auxiliary contacts wired to the 489 Breaker Status input may not operate at exactly the same time as the main breaker contacts, the time delay should be coordinated with the difference of the operation times. In the event of a low impedance fault, the differential element will still shutdown the generator quickly.



If the unit auxiliary transformer is on the generator side of the breaker, the pickup level must be set greater than the unit auxiliary load.

5.6.4 Inadvertent Energization

PATH: SETPOINTS $\triangleright \nabla$ S5 CURRENT ELEM. $\triangleright \nabla$ INADVERTENT ENERG.



The logic diagram for the inadvertent energization protection feature is shown below. The feature may be armed when all of the phase voltages fall below the undervoltage pickup level *and* the unit is offline. This would be the case when the VTs are on the generator side of the disconnect device. If however, the VTs are on the power system side of the disconnect device, the feature should be armed if all of the phase voltages fall below the undervoltage pickup level *or* the unit is offline. When the feature is armed, if any one of the phase currents measured at the output CTs exceeds the overcurrent level programmed, a trip will occur.



This feature requires 5 seconds to arm, 250 ms to disarm.

Protection can be provided for poor synchronization by using the "U/V or Offline" arming signal. During normal synchronization, there should be relatively low current measured. If however, synchronization is attempted when conditions are not appropriate, a large current that is measured within 250 ms after the generator is placed online would result in a trip.

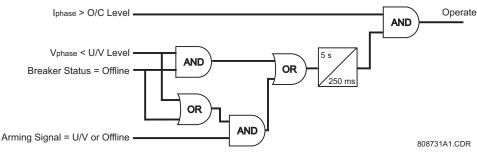
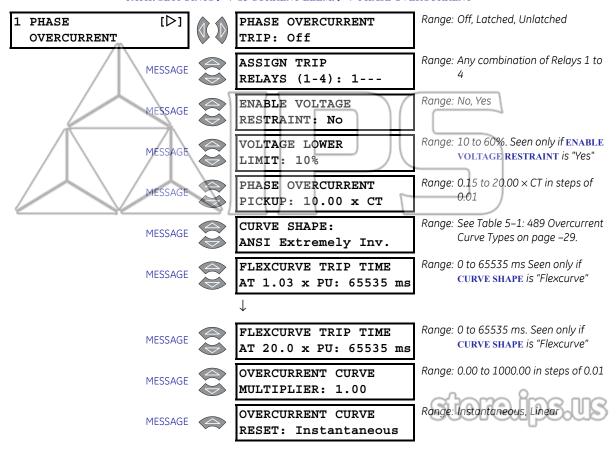


FIGURE 5-1: Inadvertent Energization Logic

5.6.5 Phase Overcurrent

PATH: SETPOINTS ▷▽ S5 CURRENT ELEM. ▷▽ PHASE OVERCURRENT



If the primary system protection fails to properly isolate phase faults, the voltage restrained overcurrent acts as system backup protection. The magnitude of each phase current measured at the output CTs is used to time out against an inverse time curve. The 489 inverse time curve for this element may be either ANSI, IEC, or GE Type IAC standard curve shapes. This allows for simplified coordination with downstream devices. If these curve shapes are not adequate, FlexCurves™ may be used to customize the inverse time curve characteristics.

The voltage restraint feature lowers the pickup value of each phase time overcurrent element in a fixed relationship (see figure below) with the corresponding input voltage to a minimum pickup of $0.15 \times CT$. The **voltage Lower Limit** setpoint prevents very rapid tripping prior to primary protection clearing a fault when voltage restraint is enabled and severe close-in fault has occurred. If voltage restraint is not required, select "No" for this setpoint. If the VT type is selected as "None" or a VT fuse loss is detected, the voltage restraint is ignored and the element operates as simple phase overcurrent.



A fuse failure is detected within 99 ms; therefore, any voltage restrained overcurrent trip should have a time delay of 100 ms or more or nuisance tripping on fuse loss could occur.

For example, to determine the voltage restrained phase overcurrent pickup level under the following situation:

PHASE OVERCURRENT PICKUP: "2.00 × CT"

- ENABLE VOLTAGE RESTRAINT: "Yes"
- VOLTAGE LOWER LIMIT: 10%
- Phase-Phase Voltage / Rated Phase-Phase Voltage = 0.4 p.u. V

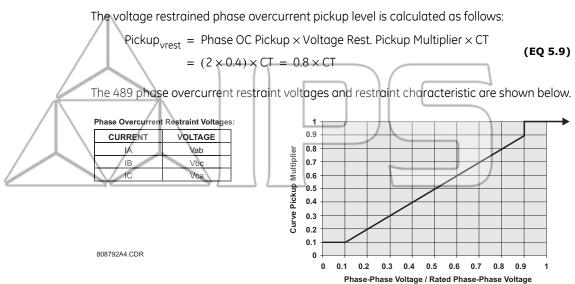
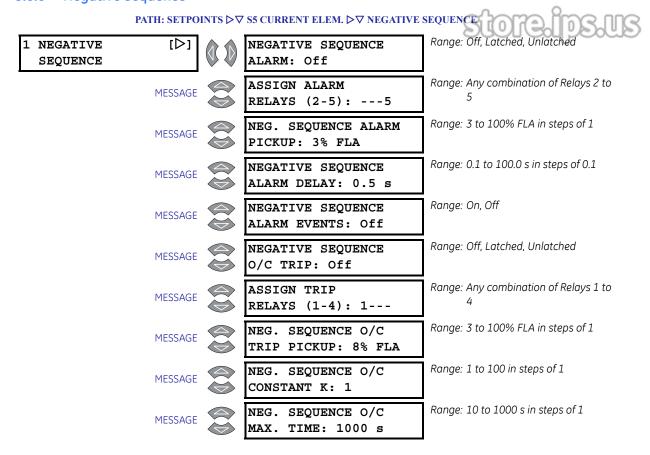


FIGURE 5-2: Voltage Restraint Characteristic

5.6.6 Negative Sequence



MESSAGE (

NEG. SEQUENCE O/C RESET RATE: 227.0 s Range: 0.0 to 999.9 s in steps of 0.01

Rotor heating in generators due to negative sequence current is a well known phenomenon. Generators have very specific capability limits where unbalanced current is concerned (see ANSI C50.13). A generator should have a rating for both continuous and also short time operation when negative sequence current components are present.

The short time negative-sequence capability of the generator is defined as follows:

$$K = I_2^2 T$$

(EQ 5.10)

where:

K= constant from generator manufacturer depending on size and design; $l_2=$ negative sequence current as a percentage of generator rated FLA as measured at the output CTs;

t = time in seconds when l_2 > pickup (minimum 250 ms, maximum defined by setpoint).

The 489 has a definite time alarm and inverse time overcurrent curve trip to protect the generator rotor from overheating due to the presence of negative sequence currents. Pickup values are negative sequence current as a percent of generator rated full load current. The generator FLA is calculated as:

Generator FLA =
$$\frac{\text{Generator Rated MVA}}{\sqrt{3} \times \text{Rated Generator Phase-Phase Voltage}}$$
 (EQ 5.11)

Negative sequence overcurrent maximum time defines the maximum time that any value of negative sequence current in excess of the pickup value will be allowed to persist before a trip is issued. The reset rate provides a thermal memory of previous unbalance conditions. It is the linear reset time from the threshold of trip.



Unusually high negative sequence current levels may be caused by incorrect phase CT wiring.

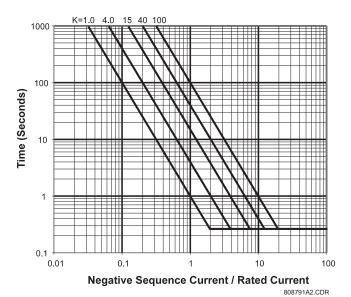
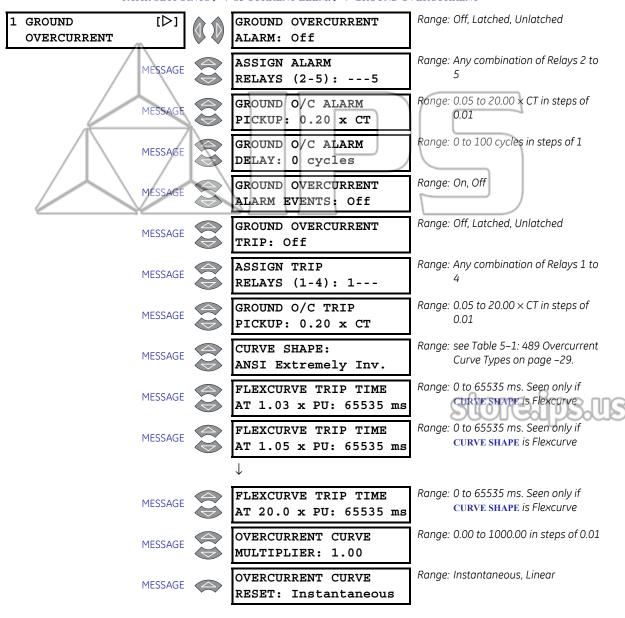


FIGURE 5–3: Negative-Sequence Inverse Time Curves

5.6.7 Ground Overcurrent

PATH: SETPOINTS ▷▽ S5 CURRENT ELEM. ▷▽ GROUND OVERCURRENT

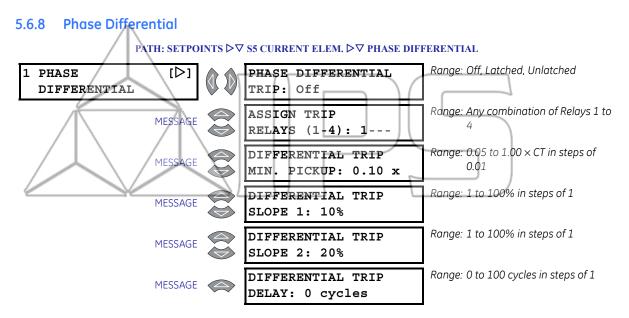


The 489 ground overcurrent feature consists of both an alarm and a trip element. The magnitude of measured ground current is used to time out against the definite time alarm or inverse time curve trip. The 489 inverse time curve for this element may be either ANSI, IEC, or GE Type IAC standard curve shapes. This allows for simplified coordination with downstream devices. If however, none of these curves shapes is adequate, the FlexCurveTM may be used to customize the inverse time curve characteristics. If the Ground CT is selected as "None", the ground overcurrent protection is disabled.



The pickup level for the ground current elements is programmable as a multiple of the CT. The 50:0.025 CT is intended for very sensitive detection of ground faults and its nominal CT rating for the 489 is 50:0.025.

For example, if the ground CT is 50:0.025, a pickup of 0.20 would be $0.20 \times 50 = 10$ A primary. If the ground CT is 50:0.025, a pickup of 0.05 would be $0.05 \times 50 = 2.5$ A primary.



The 489 differential element consists of the well known, dual slope, percent restraint characteristic. A differential signal is derived from the phasor sum of the currents on either side of the machine. A restraint signal is derived from the average of the magnitudes of these two currents. An internal flag (DIFF) is asserted when the differential signal crosses the operating characteristic as defined by the magnitude of the restraint signal. The DIFF flag produces a relay operation.

External faults near generators typically result in very large time constants of dc components in the fault currents. This creates a real danger of CT saturation.

The external fault currents will be large and the CTs will initially reproduce the fault current without distortion. Consequently the relay will see a large restraint signal coupled with a small differential signal. This condition is used as an indication of the possible onset of ac saturation of the CTs.

Magnetizing Inrush current due to the energizing of a step-up transformer or a sudden change of load, could cause a large dc offset on even very small currents that would saturate poor quality or mismatched CTs within a few power system cycles.

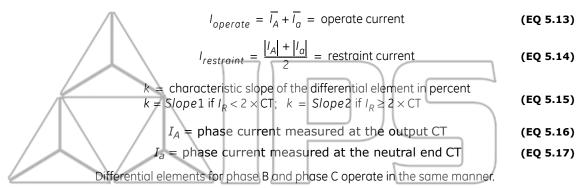
In order to provide additional security against maloperations during these events, an internal flag, SC, is set when either an ac or a dc saturation condition is indicated. Once the SC flag has been set, a comparison of the phase angles of the currents on either side of the generator is carried out. An external fault is inferred if the phase comparison indicates both currents are flowing in the same direction. An internal fault is inferred if the phase comparison indicates that the currents are flowing in opposite directions. In this case an internal flag, DIR, is set.

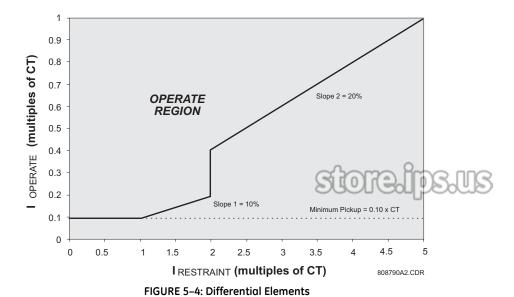
If the SC flag is not set, then the relay will operate for a DIFF flag alone. If the SC flag is set then the directional flag supervises the differential flag. The requirement for both the DIFF flag and the DIR flag during the period where CT saturation is likely therefore enhances the security of the scheme.

The differential element for phase A will operate when:

$$I_{operate} > k \times I_{restraint}$$
 (EQ 5.12)

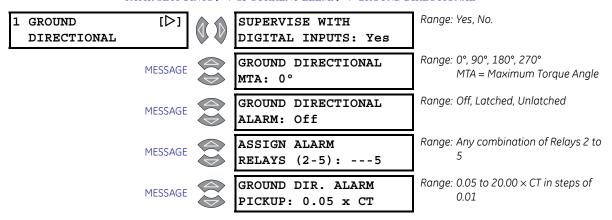
where the following hold:

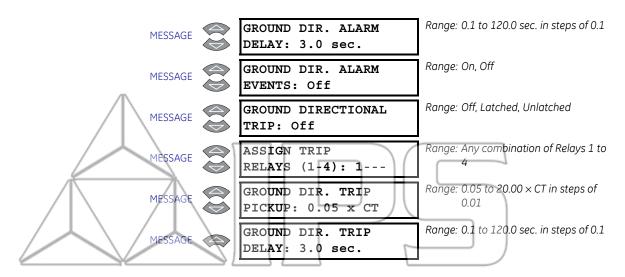




5.6.9 Ground Directional

PATH: SETPOINTS $\triangleright \nabla$ S5 CURRENT ELEM. $\triangleright \nabla$ GROUND DIRECTIONAL







The **SUPERVISE WITH DIGITAL INPUTS** setpoint is seen only if a digital input assigned to Ground Switch Status.

The 489 detects ground directional by using two measurement quantities: V_0 and I_0 . The angle between these quantities determines if a ground fault is within the generator or not. This function should be coordinated with the 59GN element (95% stator ground protection) to ensure proper operation of the element. Particularly, this element should be faster. This element must use a core balance CT to derive the I_0 signal. Polarity is critical in this element. The protection element is blocked for neutral voltages, V_0 , below 2.0 V secondary.



The pickup level for the ground current elements is programmed as a multiple of ground CT. The 50:0.025 CT is intended for measuring very small ground fault currents when connected to a sensitive ground CT having the same ratio.

For example, a pickup to 0.2xCT translates into 0.2x0.0025A = 0.5mA secondary on the terminals of the sensitive ground CT, with a relay measuring 0.2x5A = 1 A primary. A pickup setting of 0.05xCT would lead to 0.05x0.0025A = 0.125mA secondary, or 0.05x5A = 0.25A primary current.

It is strongly recommended not to exceed the CT continuous rating of 150mA for long periods of time during tests.

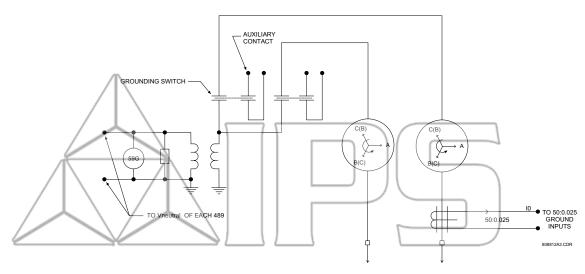
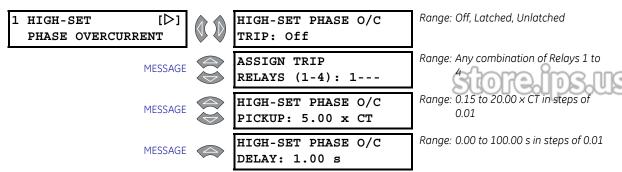


FIGURE 5-5: Ground Directional Detection

5.6.10 High-Set Phase OC

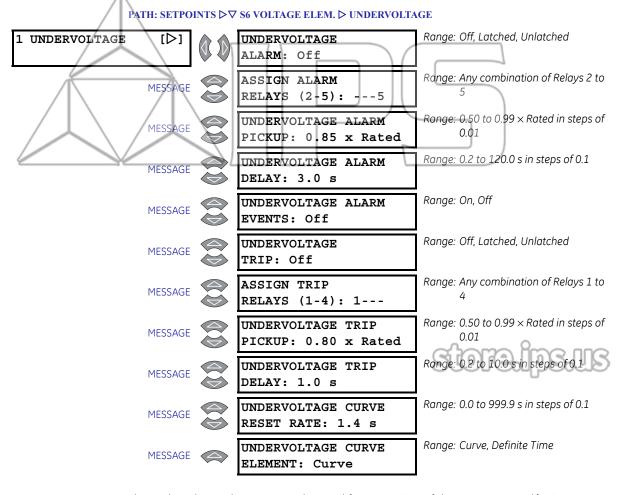
PATH: SETPOINTS ▷▽ S5 CURRENT ELEM. ▷▽ HIGH-SET PHASE OVERCURRENT



If any individual phase current exceeds the pickup level for the specified trip time a trip will occur if the feature is enabled. The element operates in both online and offline conditions. This element can be used as a backup feature to other protection elements. In situations where generators are connected in parallel this element would be set above the maximum current contribution from the generator on which the protection is installed. With this setting, the element would provide proper selective tripping. The basic operating time of the element with no time delay is 50 ms at 50/60 Hz.

5.7 S6 Voltage Elements

5.7.1 Undervoltage



The undervoltage elements may be used for protection of the generator and/or its auxiliary equipment during prolonged undervoltage conditions. They are active only when the generator is online. The alarm element is definite time and the trip element can be definite time or a curve. When the magnitude of the average phase-phase voltage is less than the pickup \times the generator rated phase-phase voltage, the element will begin to time out. If the time expires, a trip or alarm will occur.

The curve reset rate is a linear reset time from the threshold of trip. If the VT type is selected as None, VT fuse loss is detected, or the magnitude of $l_1 < 7.5\%$ CT, the undervoltage protection is disabled. The pickup levels are insensitive to frequency over the range of 5 to 90 Hz.

The formula for the undervoltage curve is:

$$T = \frac{D}{1 - V/V_{pickup}}, \text{ when } V < V_{pickup}$$
 (EQ 5.18)

where: T = trip time in seconds

D = **UNDERVOLTAGE TRIP DELAY** setpoint V = actual average phase-phase voltage $V_{pickup} =$ **UNDERVOLTAGE TRIP PICKUP** setpoint

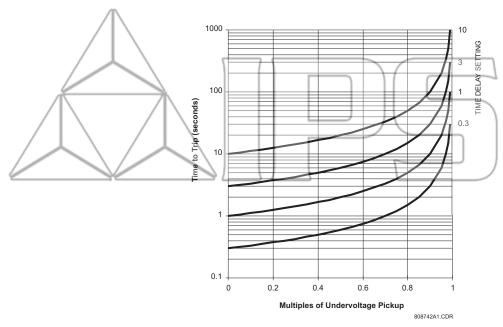


FIGURE 5-6: Undervoltage Curves

5.7.2 Overvoltage

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM ▷▽ OVERVOLTAGE

PATH: SETPOINTS ▷ ∨ S6 VOLTAGE ELEM. ▷ ∨ OVERVOLTAGE						
1 OVERVOLTAGE	[▷]	(1)	OVERVOLTAGE ALARM: Off	Range: Off, Latched, Unlatched		
M	1ESSAGE		ASSIGN ALARM RELAYS (2-5):5	Range: Any combination of Relays 2 to 5		
M	1ESSAGE		OVERVOLTAGE ALARM PICKUP: 1.15 x Rated	Range: 1.01 to 1.50 × Rated in steps of 0.01		
M	1ESSAGE		OVERVOLTAGE ALARM DELAY: 3.0 s	Range: 0.2 to 120.0 s in steps of 0.1		
M	1ESSAGE		OVERVOLTAGE ALARM EVENTS: Off	Range: On, Off		
M	1ESSAGE		OVERVOLTAGE TRIP: Off	Range: Off, Latched, Unlatched		
M	1ESSAGE		ASSIGN TRIP RELAYS (1-4): 1	Range: Any combination of Relays 1 to 4		
M	1ESSAGE		OVERVOLTAGE TRIP PICKUP: 1.20 x Rated	Range: 1.01 to 1.50 × Rated in steps of 0.01		
M	1ESSAGE		OVERVOLTAGE TRIP DELAY: 1.0 s	Range: 0.1 to 10.0 s in steps of 0.1		

MESSAGE



OVERVOLTAGE CURVE

Range: 0.0 to 999.9 s in steps of 0.1

MESSAGE



OVERVOLTAGE CURVE ELEMENT: Curve

Range: Curve, Definite Time

The overvoltage elements may be used for protection of the generator and/or its auxiliary equipment during prolonged overvoltage conditions. They are always active (when the generator is offline or online). The alarm element is definite time and the trip element can be either definite time or an inverse time curve. When the average of the measured phase-phase voltages rises above the pickup level x the generator rated phase-phase voltage, the element will begin to time out. If the time expires, a trip or alarm will occur. The reset rate is a linear reset time from the threshold of trip. The pickup levels are insensitive to frequency over the range of 5 to 90 Hz.

The formula for the curve is:

$$T = \frac{D}{(V/V_{pickup}) - 1}, \text{ when } V > V_{pickup}$$
 (EQ 5.19)

where: T = trip time in seconds

D = OVERVOLTAGE TRIP DELAY setpoint

V = actual average phase-phase voltage

V_{pickup}= **OVERVOLTAGE TRIP PICKUP** setpoint

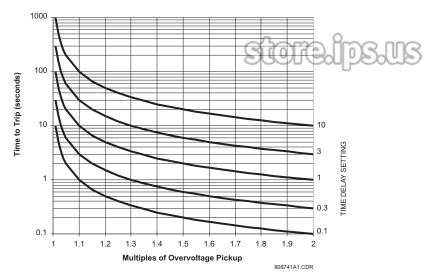


FIGURE 5-7: Overvoltage Curves

5.7.3 Volts/Hertz

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ VOLTS/HERTZ

1 VOLTS/HERTZ [▷]



VOLTS/HERTZ ALARM: Off Range: Off, Latched, Unlatched

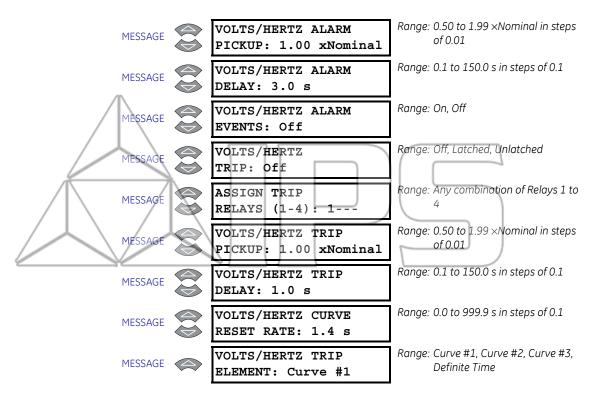
MESSAGE



ASSIGN ALARM
RELAYS (2-5): ---5

Range: Any combination of Relays 2 to

5



The Volts Per Hertz elements may be used generator and unit transformer protection. They are active as soon as the magnitude and frequency of V_{ab} is measurable. The alarm element is definite time; the trip element can be definite time or a curve. Once the V/Hz measurement V_{ab} exceeds the pickup level for the specified time, a trip or alarm will occur. The reset rate is a linear reset time from the threshold of trip and should be set to match cooling characteristics of the protected equipment. The measurement of V/Hz will be accurate through a frequency range of 5 to 90 Hz. Settings less than 1.00 only apply for special generators such as short circuit testing machines.

The formula for Volts/Hertz Curve 1 is:

$$T = \frac{D}{\left(\frac{V/F}{(V_{nom}/F_s) \times \text{Pickup}}\right)^2 - 1}, \text{ when } \frac{V}{F} > \text{Pickup}$$
 (EQ 5.20)

where: T = trip time in seconds

D = VOLTS/HERTZ TRIP DELAY setpoint

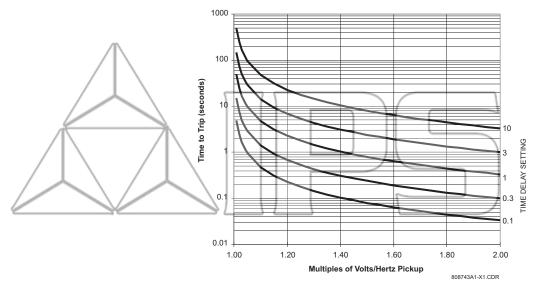
V = RMS measurement of Vab

F =frequency of Vab

 V_{NOM} = generator voltage setpoint F_S = generator frequency setpoint

Pickup = VOLTS/HERTZ TRIP PICKUP setpoint

The V/Hz Curve 1 trip curves are shown below for delay settings of 0.1, 0.3, 1, 3, and 10 seconds.



The formula for Volts/Hertz Curve 2 is:

$$T = \frac{D}{\frac{V/F}{(V_{nom}/F_s) \times \text{Pickup}} - 1}, \text{ when } \frac{V}{F} > \text{Pickup}$$
 (EQ 5.21)

where: T = trip time in seconds

D = VOLTS/HERTZ TRIP DELAY setpoint

V = RMS measurement of Vab

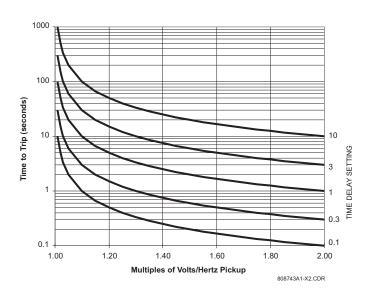
F =frequency of Vab

 V_{NOM} = generator voltage setpoint

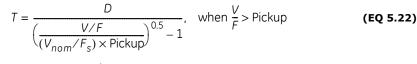
 F_S = generator frequency setpoint

Pickup = VOLTS/HERTZ TRIP PICKUP setpoint

The V/Hz Curve 2 trip curves are shown below for delay settings of 0.1, 0.3, 1, 3, and 10 seconds.



The formula for Volts/Hertz Curve 3 is:



where: T = trip time in seconds

D = VOLTS/HERTZ TRIP DELAY setpoint

V = RMS measurement of Vab

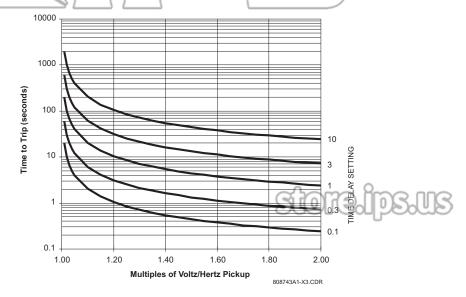
F =frequency of Vab

 V_{NOM} = generator voltage setpoint

 F_S = generator frequency setpoint

Pickup = **VOLTS/HERTZ TRIP PICKUP** setpoint

The V/Hz Curve 3 trip curves are shown below for delay settings of 0.1, 0.3, 1, 3, and 10 seconds.



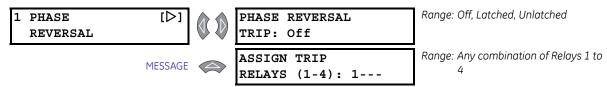


Volts/Hertz is calculated per unit as follows:

Volts/Hertz = $\frac{\text{phase-phase voltage/rated phase-phase voltage}}{\text{frequency/rated frequency}}$

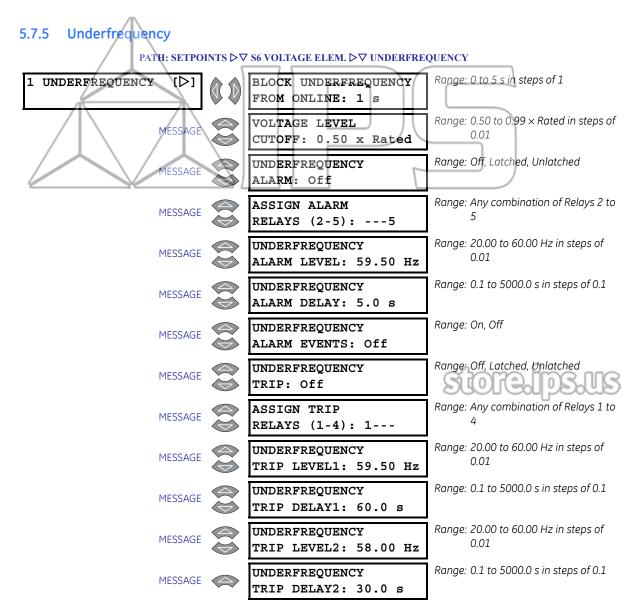
5.7.4 Phase Reversal

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ PHASE REVERSAL



The 489 can detect the phase rotation of the three phase voltages. A trip will occur within 200 ms if the Phase Reversal feature is turned on, the generator is offline, each of the phase-phase voltages is greater than 50% of the generator rated phase-phase voltage

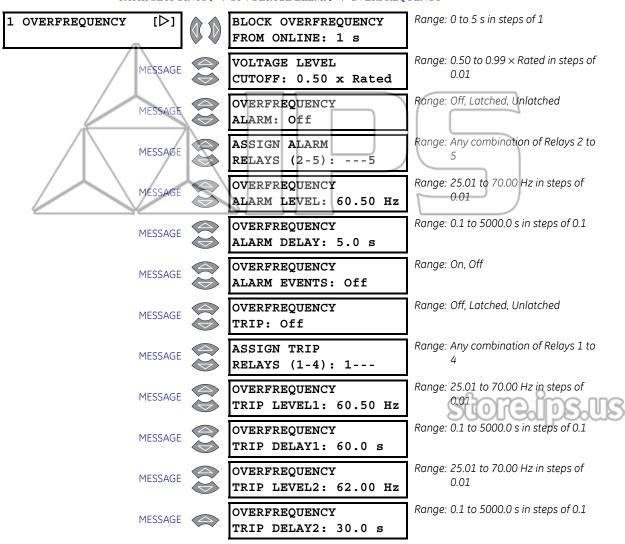
and the phase rotation is not the same as the setpoint. Loss of VT fuses cannot be detected when the generator is offline and could lead to maloperation of this element. If the VT type is selected as "None", the phase reversal protection is disabled.



It may be undesirable to enable the underfrequency elements until the generator is online. This feature can be blocked until the generator is online and the block time expires. From that point forward, the underfrequency trip and alarm elements will be active. A value of zero for the block time indicates that the underfrequency protection is active as soon as voltage exceeds the cutoff level (programmed as a multiple of the generator rated phase-phase voltage). Frequency is then measured. Once the frequency of Vab is less than the underfrequency setpoints, for the period of time specified, a trip or alarm will occur. There are dual level and time setpoints for the trip element.

5.7.6 Overfrequency

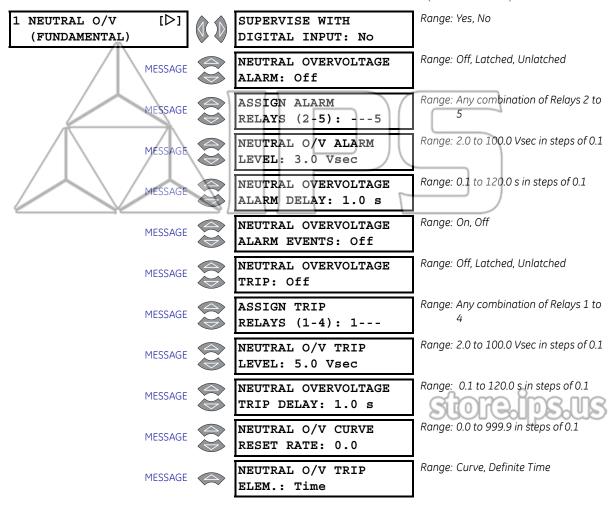
PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ OVERFREQUENCY



It may be undesirable to enable the overfrequency elements until the generator is online. This feature can be blocked until the generator is online and the block time expires. From that point forward, the overfrequency trip and alarm elements will be active. A value of zero for the block time indicates that the overfrequency protection is active as soon as voltage exceeds the cutoff level (programmed as a multiple of the generator rated phase-phase voltage). Frequency is then measured. Once the frequency of Vab exceeds the overfrequency setpoints, for the period of time specified, a trip or alarm will occur. There are dual level and time setpoints for the trip element.

5.7.7 Neutral Overvoltage

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ NEUTRAL O/V (FUNDAMENTAL)





The **SUPERVISE WITH DIGITAL INPUT** setpoint is seen only if a digital input assigned to Ground Switch Status.

The neutral overvoltage function responds to fundamental frequency voltage at the generator neutral. It provides ground fault protection for approximately 95% of the stator windings. 100% protection is provided when this element is used in conjunction with the Neutral Undervoltage (3rd harmonic) function. The alarm element is definite time and the trip element can be either definite time or an inverse time curve. When the neutral voltage rises above the pickup level the element will begin to time out. If the time expires an alarm or trip will occur. The reset rate is a linear reset time from the threshold of trip. The alarm and trip levels are programmable in terms of Neutral VT secondary voltage.

The formula for the curve is:

$$T = \frac{D}{(V/V_{pickup}) - 1} \quad \text{when } V > V_{pickup}$$
 (EQ 5.23)

where T = trip time in seconds

D = NEUTRAL OVERVOLTAGE TRIP DELAY setpoint

V = neutral voltage

 $V_{pickup} = NEUTRAL O/V TRIP LEVEL setpoint$

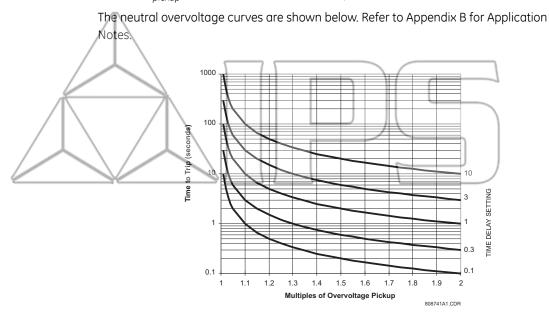


FIGURE 5-8: Neutral Overvoltage Curves

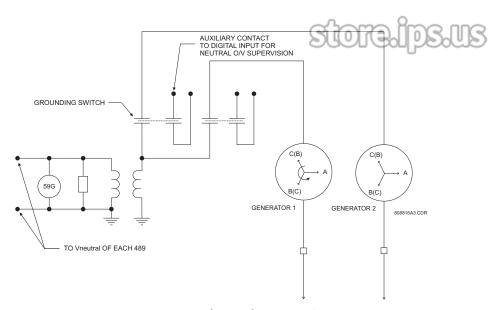


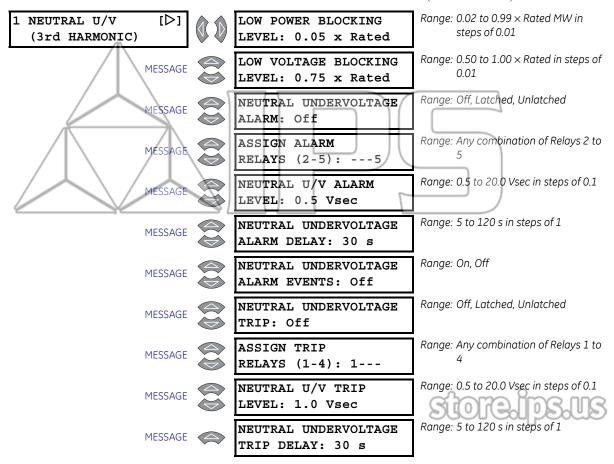
FIGURE 5–9: Neutral Overvoltage Detection



If the ground directional element is enabled, the Neutral Overvoltage element should be coordinated with it. In cases of paralleled generator grounds through the same point, with individual ground switches, per sketch below, it is recommended to use a ground switch status function to prevent maloperation of the element.

5.7.8 Neutral Undervoltage

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ NEUTRAL U/V (3RD HARMONIC)





The Low power blocking level, neutral U/V alarm level, and neutral U/V trip level setpoints are seen only if the S2 SYSTEM SETUP $\triangleright \triangledown$ voltage $\triangleright \triangledown$ vt connection setpoint is "Delta"

The neutral undervoltage function responds to 3rd harmonic voltage measured at the generator neutral and output terminals. When used in conjunction with the Neutral Overvoltage (fundamental frequency) function, it provides 100% ground fault protection of the stator windings.

For Wye connected VTs:

Since the amount of third harmonic voltage that appears in the neutral is both load and machine dependent, the protection method of choice is an adaptive method. If the phase VT connection is wye, the following formula is used to create an adaptive neutral undervoltage pickup level based on the amount of third harmonic that appears at the generator terminals.

$$\frac{V_{N3}}{(V_{P3}/3) + V_{N3}} \le 0.15$$
 which simplifies to $V_{P3} \ge 17V_{N3}$ (EQ 5.24)

The 489 tests the following permissives prior to testing the basic operating equation to ensure that V_{N3} ' should be of a measurable magnitude for an unfaulted generator:

$$V_{P3}' > 0.25 \text{ V} \text{ and } V_{P3}' \ge \text{Threshold} \times 17 \times \frac{\text{Neutral VT Ratio}}{\text{Phase VT Ratio}}$$
 (EQ 5.25)

where: V_{N3} = magnitude of the third harmonic voltage at generator neutral;

 V_{P3} = magnitude of the third harmonic voltage at the generator terminals

 V_{P3} = VT secondary magnitude of the third harmonic voltage measured at the generator terminals:

 V_{N3} = VT sec. magnitude of 3rd harmonic voltage at generator neutral; Threshold = 0.15 V for the alarm element and 0.1875 V for the trip element

For Open Delta connected VTs:

If the phase VT connection is open delta, it is not possible to measure the third harmonic voltages at the generator terminals and a simple third harmonic neutral undervoltage element is used. The level is programmable in terms of Neutral VT secondary voltage. In order to prevent nuisance tripping at low load or low generator voltages, two blocking functions are provided. They apply to both the alarm and trip functions. When used as a simple undervoltage element, settings should be based on measured 3rd harmonic neutral voltage of the healthy machine.

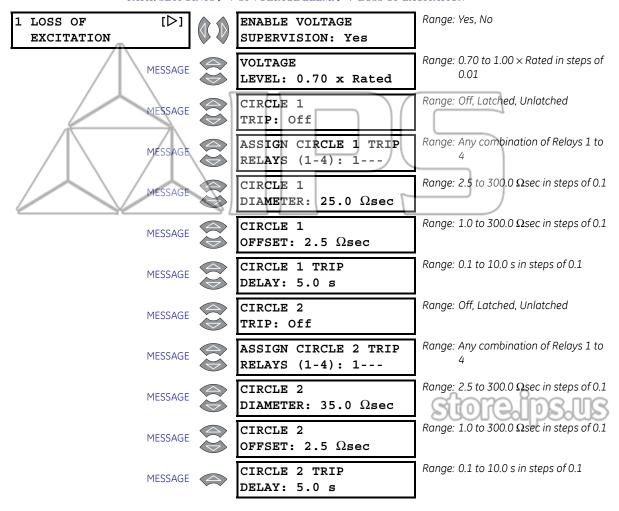


This method of using 3rd harmonic voltages to detect stator ground faults near the generator neutral has proved feasible on generators with unit transformers. Its usefulness in other generator applications is unknown.



5.7.9 Loss of Excitation

PATH: SETPOINTS $\triangleright \nabla$ S6 VOLTAGE ELEM. $\triangleright \nabla$ LOSS OF EXCITATION





The VOLTAGE LEVEL setpoint is seen only if ENABLE VOLTAGE SUPERVISION is set to "Yes".

Loss of excitation is detected with an impedance element. When the impedance falls within the impedance circle for the specified delay time, a trip will occur if it is enabled. Circles 1 and/or 2 can be tuned to a particular system. The larger circle diameter should be set to the synchronous reactance of the generator, x_d , and the circle offset to the generator transient reactance x_d' 2. Typically the smaller circle (if used) is set to minimum time with a diameter set to $0.7x_d$ and an offset of x_d' 2. This feature is blocked if voltage supervision is enabled and the generator voltage is above the **voltage Level** setpoint. The trip feature is supervised by minimum current of $0.05 \times \text{CT}$. Note that the Loss of Excitation element will be blocked if there is a VT fuse failure or if the generator is offline. Also, it uses output CT inputs.

The secondary phase-phase loss of excitation impedance is defined as:

$$Z_{loe} = \frac{V_{AB}}{I_A - I_B} = M_{loe} \angle \theta_{loe}$$
 (EQ 5.26)

where: Z_{loe} = secondary phase-to-phase loss of excitation impedance $M_{loe} \angle \theta_{loe}$ = Secondary impedance phasor (magnitude and angle)

All relay quantities are in terms of secondary impedances. The formula to convert primary impedance quantities to secondary impedance quantities is provided below.

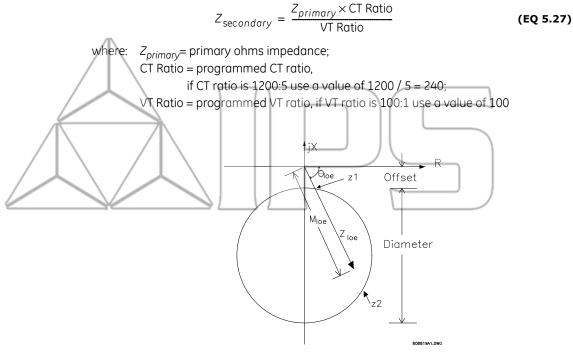
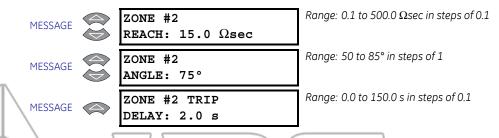


FIGURE 5-10: Loss of Excitation R-X Diagram

5.7.10 Distance Element

Store.lps.lls

PATH: SETPOINTS ▷▽ S6 VOLTAGE ELEM. ▷▽ DISTANCE ELEMENT Range: None, Delta/Wye DISTANCE [▷] STEP UP TRANSFORMER ELEMENT SETUP: None Range: On, Off FUSE FAILURE MESSAGE SUPERVISION: On Range: Off, Latched, Unlatched ZONE #1 MESSAGE TRIP: Off Range: Any combination of Relays 1 to ASSIGN ZONE #1 TRIP MESSAGE RELAYS (1-4): 1---Range: 0.1 to 500.0 Ω sec in steps of 0.1 ZONE #1 MESSAGE REACH: 10.0 Ω sec Range: 50 to 85° in steps of 1 ZONE #1 MESSAGE ANGLE: 75° Range: 0.0 to 150.0 s in steps of 0.1 ZONE #1 TRIP MESSAGE DELAY: 0.4 s Range: Off, Latched, Unlatched ZONE #2 MESSAGE TRIP: Off Range: Any combination of Relays 1 to ASSIGN ZONE #2 TRIP MESSAGE RELAYS (1-4): 1---



The distance protection function (ANSI device 21) implements two zones of mho phase-to-phase distance protection (six elements total) using the conventional phase comparator approach, with the polarizing voltage derived from the pre-fault positive sequence voltage of the protected loop. This protection is intended as backup for the primary line protection. The elements make use of the neutral-end current signals and the generator terminal voltage signals (see figure below), thus providing some protection for internal and unit transformer faults. In systems with a delta-wye transformer (DY330°), the appropriate transformations of voltage and current signals are implemented internally to allow proper detection of transformer high-side phase-to-phase faults. The reach setting is the positive sequence impedance to be covered, per phase, expressed in secondary ohms. The same transformation shown for the Loss of Excitation element can be used to calculate the desired settings as functions of the primary-side impedances.

The elements have a basic operating time of 150 ms. A VT fuse failure could cause a maloperation of a distance element unless the element is supervised by the VTFF element. In order to prevent nuisance tripping the elements require a minimum phase current of $0.05 \times CT$.

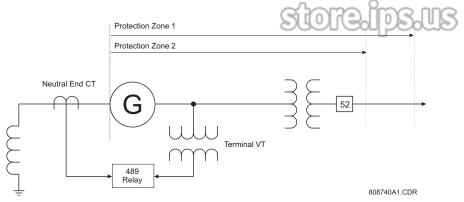


FIGURE 5-11: Distance Element Setup

The 489 phase distance element is intended to provide backup protection for phase-to-phase faults on the electric power system. This element uses the phase-to-phase voltage measured at the generator terminals and phase currents measured at the neutral side of the generator. As such this element will provide coverage for the generator step-up transformer and will also provide a degree of protection for stator phase-to-phase faults.

The element has a offset mho characteristic as shown in FIGURE 5–12: Distance Element Characteristics on page –59. Offset in the third quadrant is 1/8th of the forward reach to provide better resistive fault coverage for close-in faults. The element provides a separate measurement in three loops for AB, BC, and CA faults. There is a setting for specification of

the step-up transformer connection. If this setting is chosen as "None", then it is assumed that the transformer is Wye-Wye connected or that there is no step-up transformer. In this case the element will use the following operating quantities.

Element	Voltage	Current
AB	Va – Vb	Ia – Ib
ВС	Vb – Vc	lb – lc
CA	Vc - Va	lc - la

If this setting is chosen as "Delta/Wye" then it is assumed that the transformer is Yd1 or Yd11. In this case the following operating quantities are used.

Element	Voltage	Current
AB	(Vab - Vca) / √3	$\sqrt{3} \times Ia$
ВС	(Vbc – Vab) / $\sqrt{3}$	$\sqrt{3} \times lb$
CA	(Vca – Vbc) / √3	$\sqrt{3} \times IC$

The first zone is typically used to provide a backup protection for a step-up transformer and generator system bus protection (generator impedance should not be included into reach setting). The reach is set to cover the step-up transformer impedance with some margin, say 25%. The time delay should be coordinated with step up transformer and bus backup protection.

The second zone reach is typically set to cover the longest transmission line or feeder leaving the generating station. Care must be taken for possible under-reaching effects due to the fault contribution from other lines or generators. The element is intended for backup protection and therefore time delay should always be included. This element is typically set to coordinate with the longest operating time of the system distance relays protecting lines leaving station.

The measuring point of the element is defined by the location of the VT and CT as shown in FIGURE 5–11: Distance Element Setup on page –57. Therefore, the impedance of the stepup transformer should be included and the impedance of the generator should not be included. Care should also be taken to ensure the apparent impedance seen by the element when the machine is operating at worst-case load and power factor does not encroach into the operating characteristic. The reach setting is in secondary ohms. The minimum operating time of the element is 150 ms to coordinate with VTFF operating time (99 ms).

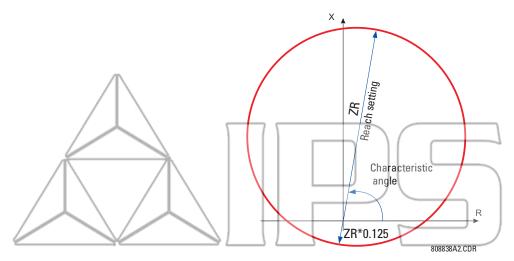


FIGURE 5–12: Distance Element Characteristics

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5.8 S7 Power Elements

5.8.1 Power Measurement Conventions

Generation of power will be displayed on the 489 as positive watts. By convention, an induction generator normally requires reactive power from the system for excitation. This is displayed on the 489 as negative vars. A synchronous generator on the other hand has its own source of excitation and can be operated with either lagging or leading power factor. This is displayed on the 489 as positive vars and negative vars, respectively. All power quantities are measured from the phase-phase voltage and the currents measured at the output CTs.

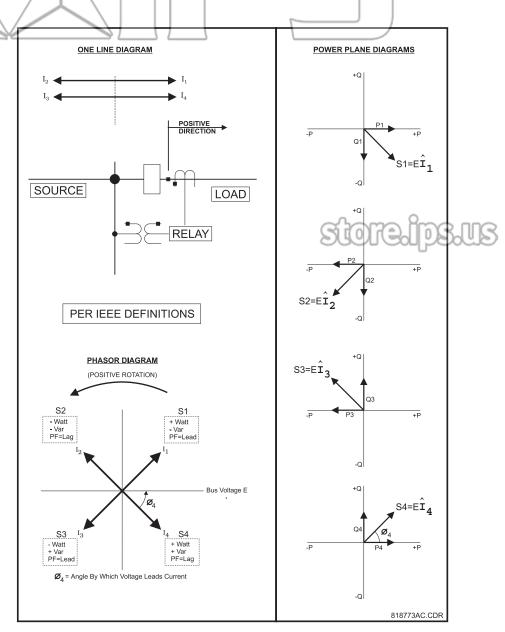
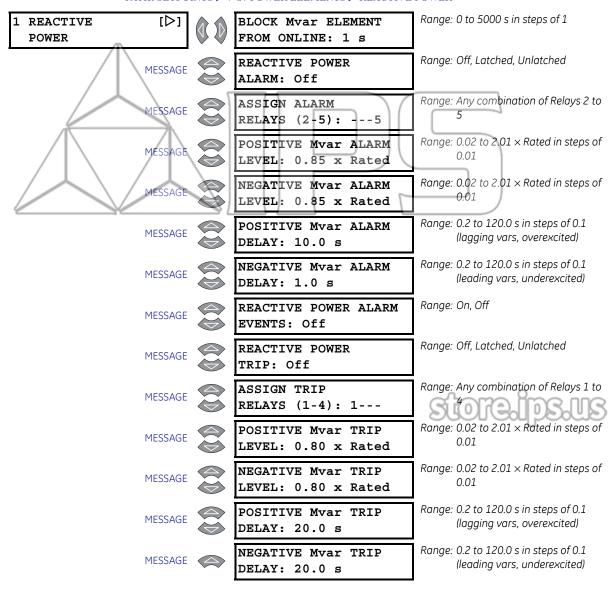


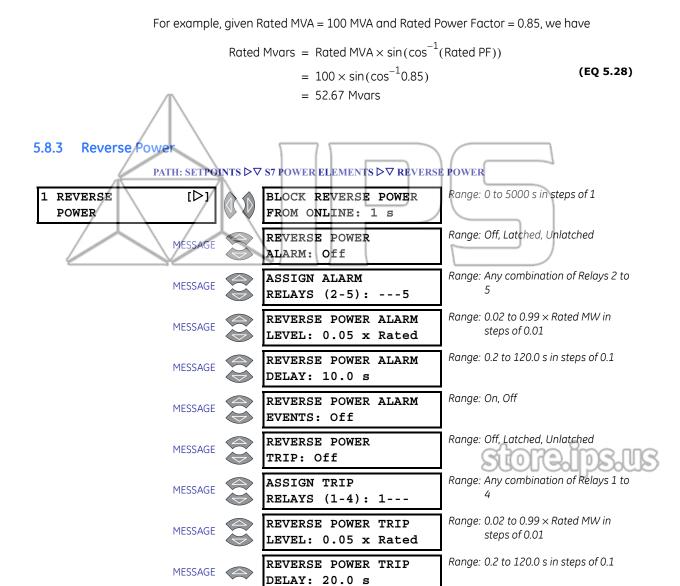
FIGURE 5-13: Power Measurement Conventions

5.8.2 Reactive Power

PATH: SETPOINTS ▷ ♥ S7 POWER ELEMENTS ▷ REACTIVE POWER



In a motor/generator application, it may be desirable not to trip or alarm on reactive power until the machine is online and the field has been applied. Therefore, this feature can be blocked until the machine is online and adequate time has expired during which the field had been applied. From that point forward, the reactive power trip and alarm elements will be active. A value of zero for the block time indicates that the reactive power protection is active as soon as both current and voltage are measured regardless of whether the generator is online or offline. Once the 3-phase total reactive power exceeds the positive or negative level, for the specified delay, a trip or alarm will occur indicating a positive or negative Mvar condition. The level is programmed in per unit of generator rated Mvar calculated from the rated MvA and rated power factor. The reactive power elements can be used to detect loss of excitation. If the VT type is selected as "None" or VT fuse loss is detected, the reactive power protection is disabled. Rated Mvars for the system can be calculated as follows:

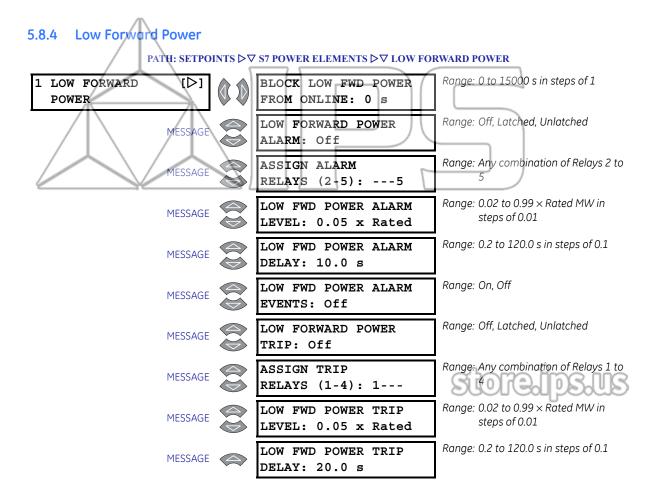


If enabled, once the magnitude of 3-phase total power exceeds the Pickup Level in the reverse direction (negative MW) for a period of time specified by the Delay, a trip or alarm will occur. The level is programmed in per unit of generator rated MW calculated from the rated MVA and rated power factor. If the generator is accelerated from the power system rather than the prime mover, the reverse power element may be blocked from start for a specified period of time. A value of zero for the block time indicates that the reverse power protection is active as soon as both current and voltage are measured regardless of whether the generator is online or offline. If the VT type is selected as "None" or VT fuse loss is detected, the reverse power protection is disabled.



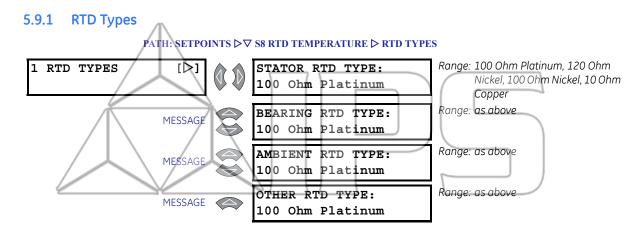
The minimum magnitude of power measurement is determined by the phase CT minimum of 2% rated CT primary. If the level for reverse power is set below that level, a trip or alarm will only occur once the phase current exceeds the 2% cutoff.

Users are cautioned that a reverse power element may not provide reliable indication when set to a very low setting, particularly under conditions of large reactive loading on the generator. Under such conditions, low forward power is a more reliable element.



If enabled, once the magnitude of 3-phase total power in the forward direction (+MW) falls below the Pickup Level for a period of time specified by the Delay, an alarm will occur. The level is programmed in per unit of generator rated MW calculated from the rated MVA and rated power factor. The low forward power element is active only when the generator is online and will be blocked until the generator is brought online, for a period of time defined by the setpoint Block Low Fwd Power From Online. The pickup level should be set lower than expected generator loading during normal operations. If the VT type is selected as "None" or VT fuse loss is detected, the low forward power protection is disabled.

5.9 S8 RTD Temperature



Each of the twelve RTDs may be configured as None or any one of four application types, Stator, Bearing, Ambient, or Other. Each of those types may in turn be any one of four different RTD types: 100 ohm Platinum, 120 ohm Nickel, 100 ohm Nickel, 10 ohm Copper. The table below lists RTD resistance vs. temperature.

Table 5–6: RTD Temperature vs. Resistance

Temperature		100 Ω Pt	120 Ω Ni	100 Ω Ni	10 Ω Cu
° C	° F	(DIN 43760)		-0	0
-50	-58	80.31	86.17	71.81 (0)	2.10 D
-40	-40	84.27	92.76	77.30	7.49
-30	-22	88.22	99.41	82.84	7.88
-20	-4	92.16	106.15	88.45	8.26
-10	14	96.09	113.00	94.17	8.65
0	32	100.00	120.00	100.00	9.04
10	50	103.90	127.17	105.97	9.42
20	68	107.79	134.52	112.10	9.81
30	86	111.67	142.06	118.38	10.19
40	104	115.54	149.79	124.82	10.58
50	122	119.39	157.74	131.45	10.97
60	140	123.24	165.90	138.25	11.35
70	158	127.07	174.25	145.20	11.74
80	176	130.89	182.84	152.37	12.12
90	194	134.70	191.64	159.70	12.51
100	212	138.50	200.64	167.20	12.90
110	230	142.29	209.85	174.87	13.28
120	248	146.06	219.29	182.75	13.67
130	266	149.82	228.96	190.80	14.06
140	284	153.58	238.85	199.04	14.44
150	302	157.32	248.95	207.45	14.83
160	320	161.04	259.30	216.08	15.22
170	338	164.76	269.91	224.92	15.61

Table 5-6:	RTD Tem	nerature vs	Resistance
Tuble 5-0.	NID IEIII	peruture vs.	nesistance

	Temperature		100 Ω Pt	120 Ω Ni	100 Ω Ni	10 Ω Cu
	° C	° F	(DIN 43760)			
	180	356	168.47	280.77	233.97	16.00
1	190	374	172.46	291.96	243.30	16.39
/	200	392	175.84	303.46	252.88	16.78
/]	210	410	179.51	315.31	262.76	17.17
	220	428	183.17	327.54	272.94	17.56
	230	446	186.82	340.14	283.45	17.95
	240	464	190.45	353.14	294.28	18.34
/ \	250	482	194.08	366.53	305.44	18.73
5.9.2 RTDs 1 to 6						•

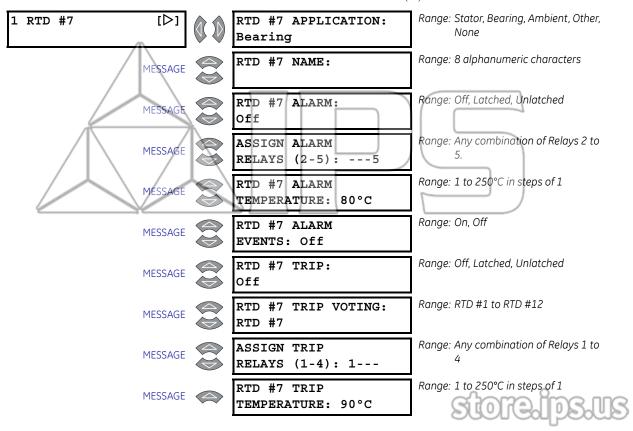
PATH: SETPOINTS $\triangleright \nabla$ S8 RTD TEMPERATURE $\triangleright \nabla$ RTD #1(6)

1 RTD #1	[⊳]	RTD #1 APPLICATION: Stator	Range: Stator, Bearing, Ambient, Other, None
	MESSAGE	RTD #1 NAME:	Range: 8 alphanumeric characters
	MESSAGE	RTD #1 ALARM: Off	Range: Off, Latched, Unlatched
	MESSAGE	ASSIGN ALARM RELAYS (2-5):5	Range: Any combination of Relays 2 to 5.
	MESSAGE	RTD #1 ALARM TEMPERATURE: 130°C	Range: 1 to 250°C in steps of 1
	MESSAGE	RTD #1 ALARM EVENTS: Off	Range: On, Off
	MESSAGE	RTD #1 TRIP: Off	Range: Off, Latched, Unlatched
	MESSAGE	RTD #1 TRIP VOTING: RTD #1	Range: RTD #1 to RTD #12
	MESSAGE	ASSIGN TRIP RELAYS (1-4): 1	Range: Any combination of Relays 1 to 4
	MESSAGE	RTD #1 TRIP TEMPERATURE: 155°C	Range: 1 to 250°C in steps of 1

RTDs 1 through 6 default to Stator RTD type. There are individual alarm and trip configurations for each RTD. This allows one of the RTDs to be turned off if it malfunctions. The alarm level is normally set slightly above the normal running temperature. The trip level is normally set at the insulation rating. Trip voting has been added for extra reliability in the event of RTD malfunction. If enabled, a second RTD must also exceed the trip temperature of the RTD being checked before a trip will be issued. If the RTD is chosen to vote with itself, the voting feature is disabled. Each RTD name may be changed if desired.

5.9.3 RTDs 7 to 10

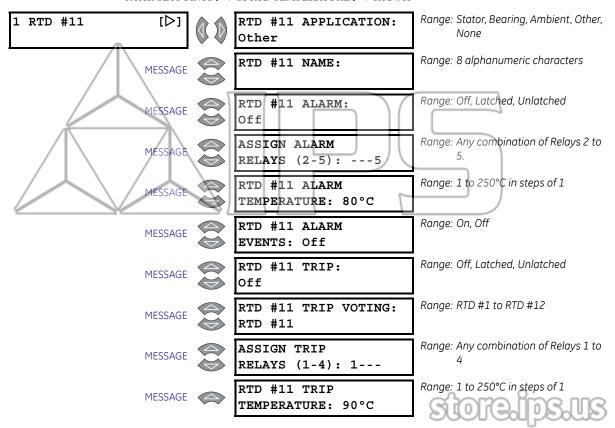
PATH: SETPOINTS ▷∇ S8 RTD TEMPERATURE ▷∇ RTD #7(10)



RTDs 7 through 10 default to Bearing RTD type. There are individual alarm and trip configurations for each RTD. This allows one of the RTDs to be turned off if it malfunctions. The alarm level and the trip level are normally set slightly above the normal running temperature, but below the bearing temperature rating. Trip voting has been added for extra reliability in the event of RTD malfunction. If enabled, a second RTD must also exceed the trip temperature of the RTD being checked before a trip will be issued. If the RTD is chosen to vote with itself, the voting feature is disabled. Each RTD name may be changed if desired.

5.9.4 RTD 11

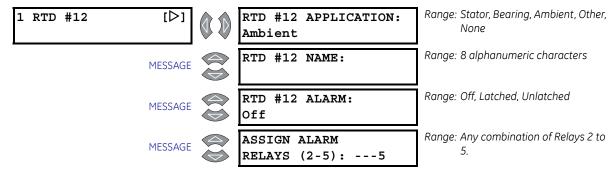
PATH: SETPOINTS ▷▽ S8 RTD TEMPERATURE ▷▽ RTD #11

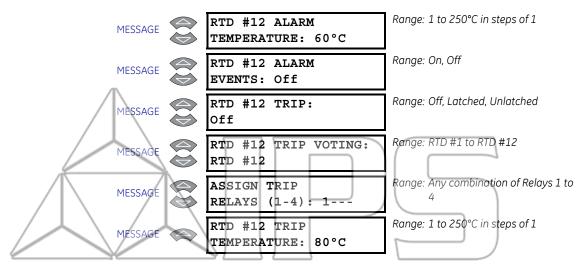


RTD 11 defaults to Other RTD type. The Other selection allows the RTD to be used to monitor any temperature that might be required, either for a process or additional bearings or other. There are individual alarm and trip configurations for this RTD. Trip voting has been added for extra reliability in the event of RTD malfunction. If enabled, a second RTD must also exceed the trip temperature of the RTD being checked before a trip will be issued. If the RTD is chosen to vote with itself, the voting feature is disabled. The RTD name may be changed if desired.

5.9.5 RTD 12

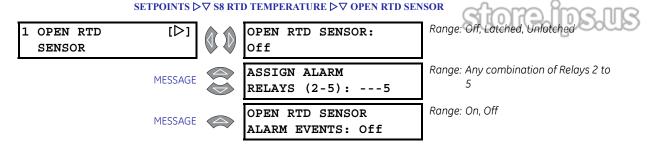
PATH: SETPOINTS $\triangleright \nabla$ S8 RTD TEMPERATURE $\triangleright \nabla$ RTD #12





RTDs 12 defaults to Ambient RTD type. The Ambient selection allows the RTD to be used to monitor ambient temperature. There are individual alarm and trip configurations for this RTD. Trip voting has been added for extra reliability in the event of RTD malfunction. If enabled, a second RTD must also exceed the trip temperature of the RTD being checked before a trip will be issued. If the RTD is chosen to vote with itself, the voting feature is disabled. The RTD name may be changed if desired.

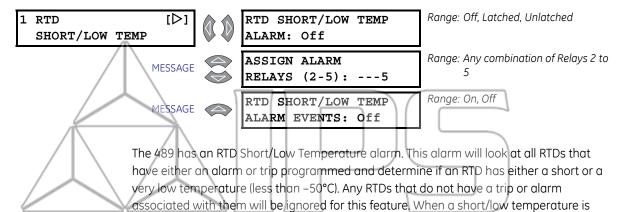
5.9.6 Open RTD Sensor



The 489 has an Open RTD Sensor Alarm. This alarm will look at all RTDs that have either an alarm or trip programmed and determine if an RTD connection has been broken. Any RTDs that do not have a trip or alarm associated with them will be ignored for this feature. When a broken sensor is detected, the assigned output relay will operate and a message will appear on the display identifying the RTD that is broken. It is recommended that if this feature is used, the alarm be programmed as latched so that intermittent RTDs are detected and corrective action may be taken.

5.9.7 RTD Short/Low Temp

PATH: SETPOINTS ▷▽ S8 RTD TEMPERATURE ▷▽ RTD SHORT/LOW TEMP



corrective action may be taken.

detected, the assigned output relay will operate and a message will appear on the display identifying the RTD that caused the alarm. It is recommended that if this feature is used, the alarm be programmed as latched so that intermittent RTDs are detected and

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5.10 S9 Thermal Model

5.10.1 489 Thermal Model

The thermal model of the 489 is primarily intended for induction generators, especially those that start on the system bus in the same manner as induction motors. However, some of the thermal model features may be used to model the heating that occurs in synchronous generators during overload conditions.

One of the principle enemies of generator life is heat. Generator thermal limits are dictated by the design of both the stator and the rotor. Induction generators that start on the system bus have three modes of operation: locked rotor or stall (when the rotor is not turning), acceleration (when the rotor is coming up to speed), and generating (when the rotor turns at super-synchronous speed). Heating occurs in the generator during each of these conditions in very distinct ways. Typically, during the generator starting, locked rotor and acceleration conditions, the generator will be rotor limited. That is to say that the rotor will approach its thermal limit before the stator. Under locked rotor conditions, voltage is induced in the rotor at line frequency, 50 or 60 Hz. This voltage causes a current to flow in the rotor, also at line frequency, and the heat generated (I^2R) is a function of the effective rotor resistance. At 50 or 60 Hz, the reactance of the rotor cage causes the current to flow at the outer edges of the rotor bars. The effective resistance of the rotor is therefore at a maximum during a locked rotor condition as is rotor heating. When the generator is running at above rated speed, the voltage induced in the rotor is at a low frequency (approximately 1 Hz) and therefore, the effective resistance of the rotor is reduced quite dramatically. During overloads, the generator thermal limit is typically dictated by stator parameters. Some special generators might be all stator or all rotor limited. During acceleration, the dynamic nature of the generator slip dictates that rotor impedance is also dynamic, and a third thermal limit characteristic is necessary.

The figure below illustrates typical thermal limit curves for induction motors. The starting characteristic is shown for a high inertia load at 80% voltage. If the machine started quicker, the distinct characteristics of the thermal limit curves would not be required and the running overload curve would be joined with locked rotor safe stall times to produce a single overload curve.

The generator manufacturer should provide a safe stall time or thermal limit curves for any generator that is started as an induction motor. These thermal limits are intended to be used as guidelines and their definition is not always precise. When operation of the generator exceeds the thermal limit, the generator insulation does not immediately melt, rather, the rate of insulation degradation reaches a point where continued operation will significantly reduce generator life.

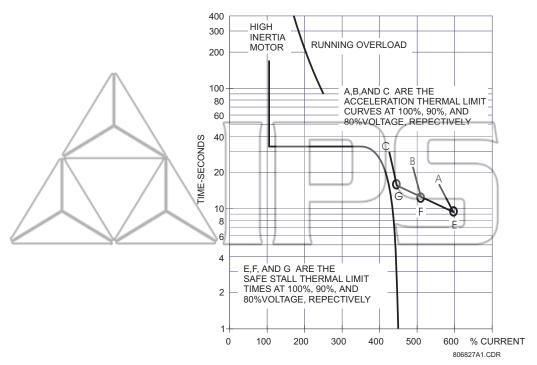


FIGURE 5–14: Typical Time-Current and Thermal Limit Curves (ANSI/IEEE C37.96)

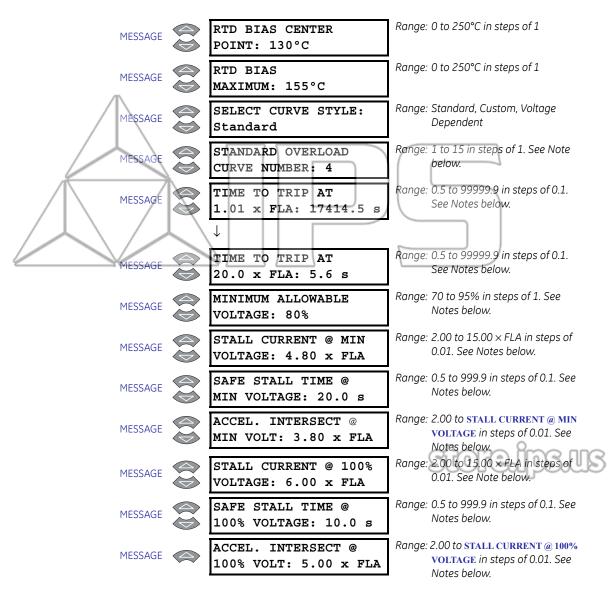
5.10.2 Model Setup

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Setpoints

PATH: SETPOINTS ▷▽ S9 THERMAL MODEL ▷ MODEL SETUP

1 MODEL SETUP	[▷]	1	ENABLE THERMAL MODEL: No	Range: No, Yes
	MESSAGE		OVERLOAD PICKUP LEVEL: 1.01 x FLA	Range: 1.01 to 1.25 × FLA in steps of 0.01
	MESSAGE		UNBALANCE BIAS K FACTOR: 0	Range: 0 to 12 in steps of 1. A value of "0" disables this feature
	MESSAGE		COOL TIME CONSTANT ONLINE: 15 min.	Range: 0 to 500 min. in steps of 1
	MESSAGE		COOL TIME CONSTANT OFFLINE: 30 min.	Range: 0 to 500 min. in steps of 1
	MESSAGE		HOT/COLD SAFE STALL RATIO: 1.00	Range: 0.01 to 1.00 in steps of 0.01
	MESSAGE		ENABLE RTD BIASING: No	Range: No, Yes
	MESSAGE		RTD BIAS MINIMUM: 40°C	Range: 0 to 250°C in steps of 1





The RTD BIAS MINIMUM, RTD BIAS CENTER, and RTD BIAS MAXIMUM setpoints is are seen only if ENABLE RTD BIASING is set to "Yes".



The **STANDARD OVERLOAD CURVE NUMBER** is seen only if **SELECT CURVE STYLE** is set to "Standard". If the **SELECT CURVE STYLE** is set to "Voltage Dependent", all setpoints shown after the **STANDARD OVERLOAD CURVE NUMBER** are displayed. If the **SELECT CURVE STYLE** is set to "Custom", the setpoints shown after **TIME TO TRIP AT 20.0 X FLA** are not displayed.

The current measured at the output CTs is used for the thermal model. The thermal model consists of five key elements: the overload curve and overload pickup level, the unbalance biasing of the generator current while the machine is running, the cooling time constants, and the biasing of the thermal model based on hot/cold generator information and measured stator temperature. Each of these elements are described in detail in the sections that follow.



The generator FLA is calculated as:

Generator Rated MVA
$$\sqrt{3} \times \text{Rated Generator Phase-Phase Voltage}$$
 (EQ 5.29)

The 489 integrates both stator and rotor heating into one model. Machine heating is reflected in a register called Thermal Capacity Used. If the machine has been stopped for a long period of time, it will be at ambient temperature and thermal capacity used should be zero. If the machine is in overload, once the thermal capacity used reaches 100%, a trip will occur.

The overload curve accounts for machine heating during stall, acceleration, and running in both the stator and the rotor. The Overload Pickup setpoint defines where the running overload curve begins as the generator enters an overload condition. This is useful to accommodate a service factor. The curve is effectively cut off at current values below this pickup.

Generator thermal limits consist of three distinct parts based on the three conditions of operation, locked rotor or stall, acceleration, and running overload. Each of these curves may be provided for both a hot and cold machine. A hot machine is defined as one that has been running for a period of time at full load such that the stator and rotor temperatures have settled at their rated temperature. A cold machine is defined as a machine that has been stopped for a period of time such that the stator and rotor temperatures have settled at ambient temperature. For most machines, the distinct characteristics of the thermal limits are formed into one smooth homogeneous curve. Sometimes only a safe stall time is provided. This is acceptable if the machine has been designed conservatively and can easily perform its required duty without infringing on the thermal limit. In this case, the protection can be conservative. If the machine has been designed very close to its thermal limits when operated as required, then the distinct characteristics of the thermal limits become important.

The 489 overload curve can take one of three formats, Standard, Custom Curve, or Voltage Dependent. Regardless of which curve style is selected, the 489 will retain thermal memory in the form of a register called Thermal Capacity Used. This register is updated every 50 ms using the following equation:

$$TC_{used t} = TC_{used t - 50ms} + \frac{50 ms}{time to trip} \times 100\%$$
 (EQ 5.30)

where time to trip = time taken from the overload curve at l_{eq} as a function of FLA.

The overload protection curve should always be set slightly lower than the thermal limits provided by the manufacturer. This will ensure that the machine is tripped before the thermal limit is reached. If the starting times are well within the safe stall times, it is recommended that the 489 Standard Overload Curve be used. The standard overload curves are a series of 15 curves with a common curve shape based on typical generator thermal limit curves (see the following figure and table).

When the generator trips offline due to overload the generator will be locked out (the trip relay will stay latched) until generator thermal capacity reaches 15%.

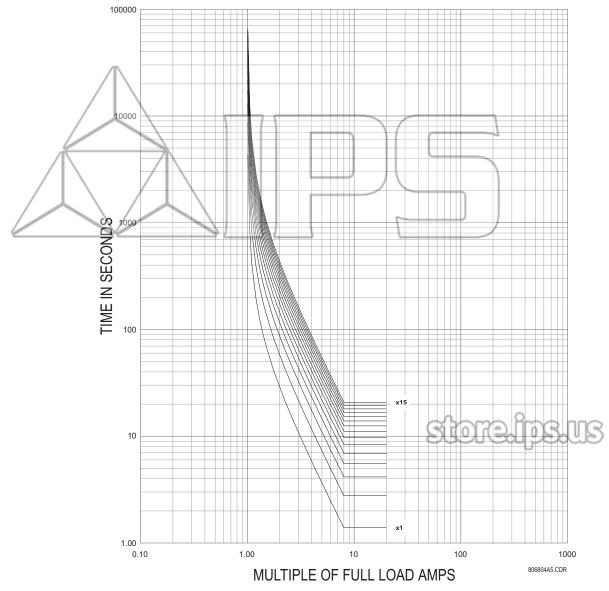


FIGURE 5-15: 489 Standard Overload Curves



Above 8.0 \times Pickup, the trip time for 8.0 is used. This prevents the overload curve from acting as an instantaneous element.

The standard overload curves equation is:

Time to Trip =
$$\frac{\text{Curve Multiplier} \times 2.2116623}{0.02530337 \times (\text{Pickup} - 1)^2 + 0.05054758 \times (\text{Pickup} - 1)}$$
 (EQ 5.31)

Table 5–7: 489 Standard Overload Curve Multipliers

PICKUP	Table 5–7: 489 Standard Overload Curve Multipliers P STANDARD CURVE MULTIPLIERS														
(× FLA)	× 1	× 2	× 3 /	×4	× 5	× 6	× 7	× 8	× 9	× 10	× 11	× 12	× 13	× 14	× 15
1.0	435	870	130	1 74	217	261	304	348	391	435	478	522	565	609	653
	3.6	7.2	61	14	68	22	75	29	83	36	90	43	97	51	04
1.0	853.	170	256	341	426	512	59 7	682	768	85 3	939	102	110	119	128
5	71	7.4	1.1	4.9	8.6	2.3	6. 0	9.7	3.4	7.1	0.8	45	98	52	06
1.1	416.	833.	125	166	208	250	29 1	333	375	416	458	500	541	583	625
	68	36	0.0	6.7	3.4	0.1	6. 8	3.5	0.1	6.8	3.5	0.2	6.9	3.6	0.2
1.2	198.	397.	5 96 .	79 5.	994.	119	139	159	178	198	218	238	2 58	278	298
0	86	72	58	4 4	30	3.2	2.0	0.9	9.7	8.6	7.5	6.3	5. 2	4.1	2.9
1.3	126.	253.	380.	507.	634.	760.	887.	101	114	126	139	152	164	177	190
0	80	61	41	22	02	82	63	4.4	1.2	8.0	4.8	1.6	8.5	5.3	2.1
1.4	91.1	182.	273.	364.	455.	546.	637.	729.	820.	911.	100	109	118	127	136
	4	27	41	55	68	82	96	09	23	37	2.5	3.6	4.8	5.9	7.0
1.5	69.9	139.	209.	279.	349.	419.	489.	559.	629.	699.	769.	839.	909.	979.	104
0	9	98	97	96	95	94	93	92	91	90	89	88	87	86	9.9
1.7	42.4	84.8	127.	169.	212.	254.	296.	339.	381.	424.	466.	508.	551.	593.	636.
5	1	3	24	66	07	49	90	32	73	15	56	98	39	81	22
2.0	29.1	58.3	87.4	116.	145.	174.	204.	233.	262.	291.	320.	349.	379.	408.	437.
	6	2	7	63	79	95	11	26	42	58	74	90	05	21	37
2.2	21.5	43.0	64.5	86.1	107.	129.	150.	172.	193.	215.	236.	258.	279.	301.	322.
5		6	9	2	65	18	72	25	78	31	84	37	90	43	96
2.5	16.6	33.3	49.9	66.6	83.3	99.9	116.	133.	149.	166.	183.	199.	216.	233.	249.
0	6	2	8	4	0	6	62	28	94	60	26	92	58	24	90
2.7	13.3	26.6	39.9	53.3	66.6	79.9	93.2	106.	119.	133.	146.	159.	173.	186.	199.
5	3	5	8	1	4	6	9	62	95	27	60	93	25	58	91
3.0	10.9	21.8	32.8	43.7	54.6	65.5	76.5	87.4	98.3	109.	120.	131.	142.	153.	163.
0	3	6	0	3	6	9	2	6	9	32	25	19	12	05	98
3.2	9.15	18.2	27.4	36.5	45.7	54.8	64.0	73.1	82.3	91.4	100.	109.	118.	128.	137.
5		9	4	8	3	7	2	6	1	6	60	75	89	04	18
3.5 0	7.77	15.5 5	23.3	31.0 9	38.8 7	46.6 4	54.4 1	62.1 9	69.9 6	77.7 3	85.5 1	93.2 8	101. 05	108. 83	116. 60
3.7	6.69	13.3	20.0	26.7	33.4	40.1	46.8	53.5	60.2	66.9	73.6	80.3	87.0	93.7	100.
5		9	8	8	7	7	6	6	5	5	4	4	3	3	42
4.0 0	5.83	11.6 6	17.4 9	23.3	29.1 5	34.9 8	40.8 1	46.6 4	52.4 7	58.3 0	64.1 3	69.9 6	75.7 9	81.6 2	87.4 5
4.2	5.12	10.2	15.3	20.5	25.6	30.7	35.8	41.0	46.1	51.2	56.3	61.5	66.6	71.7	76.8
5		5	7	0	2	5	7	0	2	5	7	0	2	5	7
4.5 0	4.54	9.08	13.6 3	18.1 7	22.7 1	27.2 5	31.8 0	36.3 4	40.8 8	45.4 2	49.9 7	54.5 1	59.0 5	63.5 9	68.1 4
4.7 5	4.06	8.11	12.1 7	16.2 2	20.2 8	24.3 3	28.3 9	32.4 4	36.5 0	40.5 5	44.6 1	48.6 6	52.7 2	56.7 7	60.8
5.0 0	3.64	7.29	10.9	14.5 7	18.2 2	21.8 6	25.5 0	29.1 5	32.7 9	36.4 3	40.0 8	43.7 2	47.3 6	51.0 1	54.6 5
5.5 0	2.99	5.98	8.97	11.9 6	14.9 5	17.9 4	20.9	23.9 1	26.9 0	29.8 9	32.8 8	35.8 7	38.8 6	41.8 5	44.8 4

Table 5–7: 489 Standard Overload Curve Multipliers

PICKUP (× FLA)															
(× FLA)	×1	× 2	× 3	× 4	× 5	× 6	×7	× 8	× 9	× 10	× 11	× 12	× 13	× 14	× 15
6.0 0	2.50	5.00	7.49	9.99	12.4 9	14.9 9	17.4 9	19.9 9	22.4 8	24.9 8	27.4 8	29.9 8	32.4 8	34.9 7	37.4 7
6.5 0	2.12	4.24	6.36	8.48	10.6	12.7 2	14.8 4	16.9 6	19.0 8	21.2	23.3	25.4 4	27.5 5	29.6 7	31.7 9
7.0 0	1.82	3.64	5.46	7.29	9.11	10.9 3	12.7 5	14.5 7	1 6.3	18.2 1	20.0 4	21.8 6	23.6 8	25.5 0	27.3 2
7.5 0	1.58	3.16	4.75	6.33	7.91	9.49	11.0 8	12.6 6	1 4.2 4	1 5.8 2	17.4 1	18.9 9	20.5 7	22.1 5	23.7 4
8.0 0	1.39	2.78	4.16	5.55	6.94	8.33	9.71	11.1 0	12.4 9	13.8 8	15.2 7	16.6 5	18.0 4	19.4 3	20.8
10. 00	1.39	2.78	4.16	5.55	6.94	8.33	9.71	11.1 0	12.4 9	13.8 8	15.2 7	16.6 5	18.0 4	19.4 3	20.8
15. 00	1.39	2.78	4.16	5.55	6.94	8.33	9.71	11.1	12.4 9	13.8 8	15.2 7	16.6 5	18.0 4	19.4 3	20.8
20. 00	1.39	2.78	4.16	5.55	6.94	8.33	9.71	11.1	12.4 9	13.8 8	15.2 7	16.6 5	18.0 4	19.4 3	20.8

Custom Overload Curve

If the induction generator starting current begins to infringe on the thermal damage curves, it may become necessary to use a custom curve to tailor generator protection so successful starting may be possible without compromising protection. Furthermore, the characteristics of the starting thermal (locked rotor and acceleration) and the running thermal damage curves may not fit together very smoothly. In this instance, it may be necessary to use a custom curve to tailor protection to the thermal limits to allow the generator to be started successfully and utilized to its full potential without compromising protection. The distinct parts of the thermal limit curves now become more critical. For these conditions, it is recommended that the 489 custom curve thermal model be used. The custom overload curve allows users to program their own curves by entering trip times for 30 pre-determined current levels.

The curves below show that if the running overload thermal limit curve were smoothed into one curve with the locked rotor thermal limit curve, the induction generator could not be started at 80% voltage. A custom curve is required.

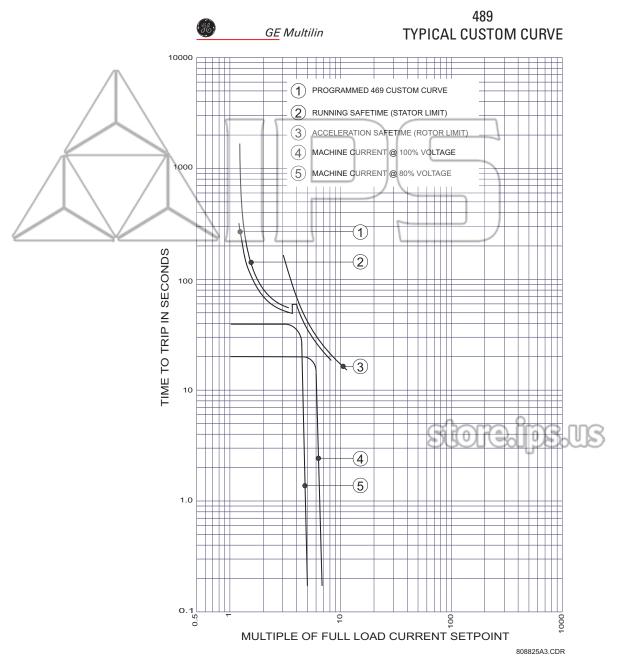


FIGURE 5-16: Custom Curve Example

Voltage Dependent Overload Curve

It is possible and acceptable that the acceleration time exceeds the safe stall time (bearing in mind that a locked rotor condition is quite different than an acceleration condition). In this instance, each distinct portion of the thermal limit curve must be known and protection coordinated against that curve. The protection relay must be able to distinguish between a locked rotor condition, an accelerating condition, and a running condition. The 489 voltage dependent overload curve feature is tailored to protect these types of machines. Voltage is monitored constantly during starting and the acceleration thermal

limit curve adjusted accordingly. If the VT Connection setpoint is set to none or if a VT fuse failure is detected, the acceleration thermal limit curve for the minimum allowable voltage will be used.

The voltage dependent overload curve is comprised of the three characteristic thermal limit curve shapes determined by the stall or locked rotor condition, acceleration, and running overload. The curve is constructed by entering a custom curve shape for the running overload protection curve. Next, a point must be entered for the acceleration protection curve at the point of intersection with the custom curve, based on the minimum allowable starting voltage as defined by the minimum allowable voltage. Locked Rotor Current and safe stall time must also be entered for that voltage. A second point of intersection must be entered for 100% voltage. Once again, the locked rotor current and the safe stall time must be entered, this time for 100% voltage. The protection curve that is created from the safe stall time and intersection point will be dynamic based on the measured voltage between the minimum allowable voltage and the 100% voltage. This method of protection inherently accounts for the change in speed as an impedance relay would. The change in impedance is reflected by machine terminal voltage and line current. For any given speed at any given voltage, there is only one value of line current.



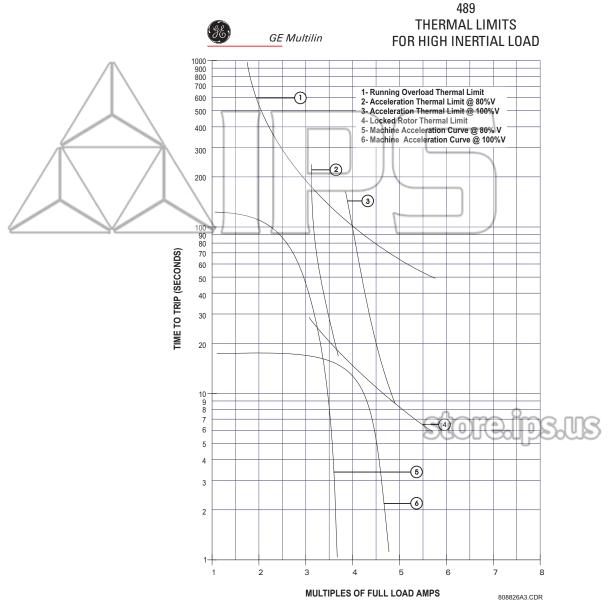


FIGURE 5–17: Thermal Limits for High Inertial Load

To illustrate the Voltage Dependent Overload Curve feature, the thermal limits shown in *Thermal Limits for High Inertial Load* on page 5–79 will be used.

Construct a custom curve for the running overload thermal limit. If the curve does not extend to the acceleration thermal limits, extend it such that the curve intersects the acceleration thermal limit curves. (see the custom curve below).

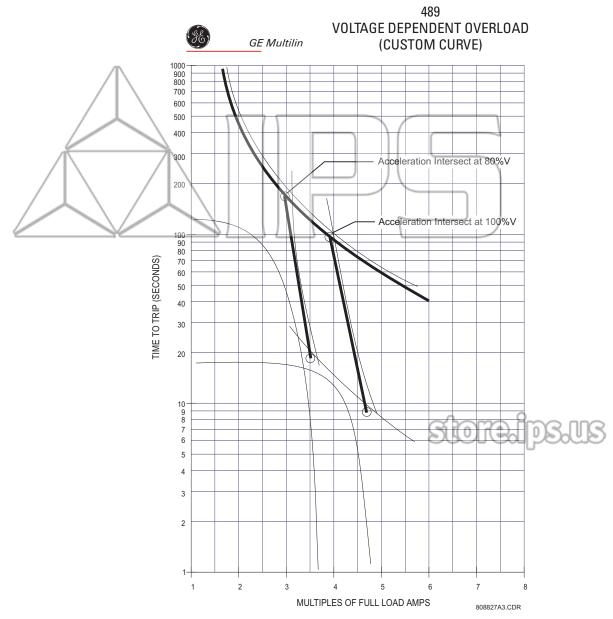


FIGURE 5-18: Voltage Dependent Overload Curve (Custom)

- Enter the per unit current value for the acceleration overload curve intersect with the custom curve for 80% voltage.
- Enter the per unit current and safe stall protection time for 80% voltage (see the acceleration curves below).
- Enter the per unit current value for the acceleration overload curve intersect with the custom curve for 100% voltage.
- Enter the per unit current and safe stall protection time for 100% voltage (see the acceleration curves below).

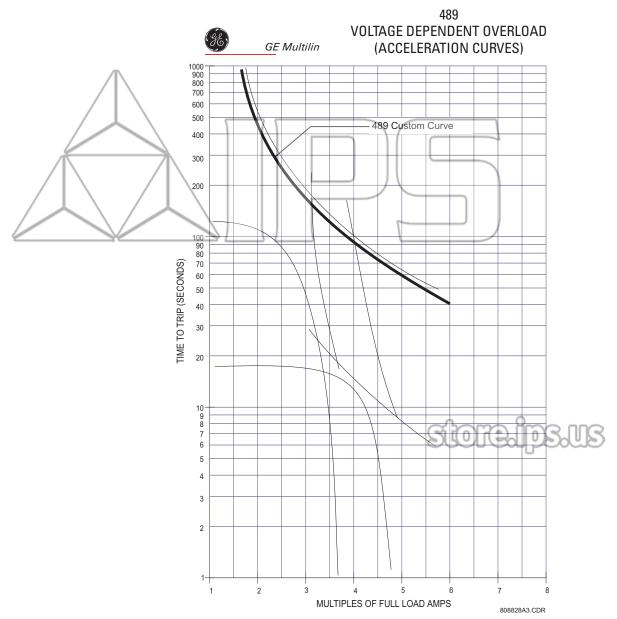


FIGURE 5–19: Voltage Dependent Overload Curve (Acceleration Curves)

The 489 takes the information provided and create protection curves for any voltage between the minimum and 100%. For values above the voltage in question, the 489 extrapolates the safe stall protection curve to 110% voltage. This current level is calculated by taking the locked rotor current at 100% voltage and multiplying by 1.10. For trip times above the 110% voltage level, the trip time of 110% will be used (see the figure below).

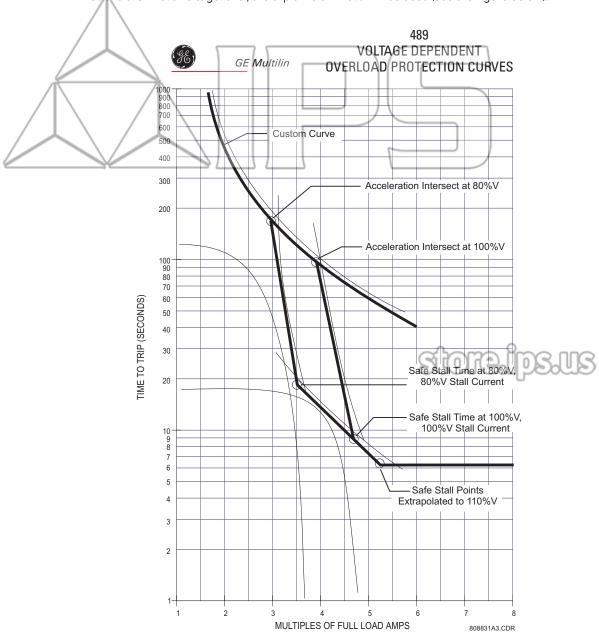


FIGURE 5–20: Voltage Dependent Overload Protection Curves



The safe stall curve is in reality a series of safe stall points for different voltages. For a given voltage, there can be only one value of stall current, and therefore only one safe stall time.

The following curves illustrate the resultant overload protection for 80% and 100% voltage, respectively. For voltages between these levels, the 489 shifts the acceleration curve linearly and constantly based upon the measured voltage during generator start.

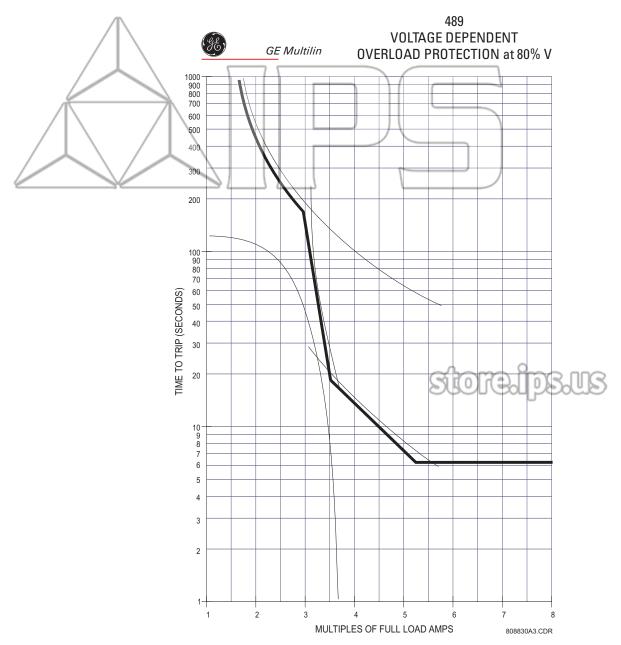


FIGURE 5–21: Voltage Dependent Overload Protection at 80% Voltage

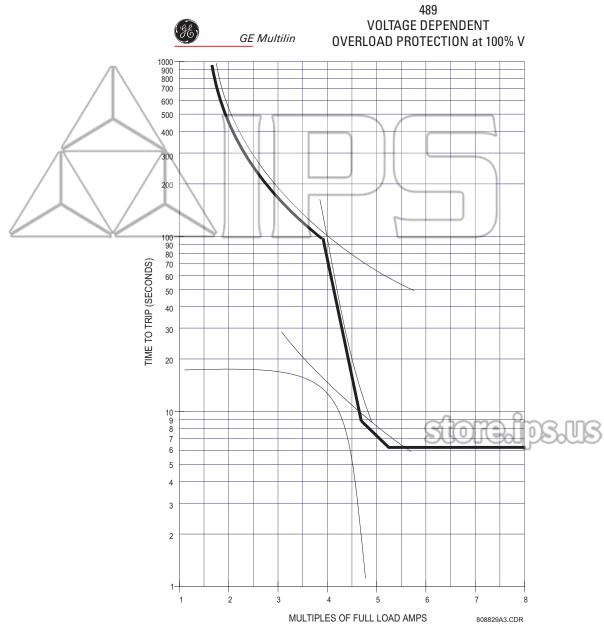


FIGURE 5–22: Voltage Dependent Overload Protection at 100% Voltage

Unbalance Bias

Unbalanced phase currents will cause additional rotor heating that will not be accounted for by electromechanical relays and may not be accounted for in some electronic protective relays. When the generator is running, the rotor will rotate in the direction of the positive sequence current at near synchronous speed. Negative sequence current, which has a phase rotation that is opposite to the positive sequence current, and hence, opposite to the rotor rotation, will generate a rotor voltage that will produce a substantial rotor current. This induced current will have a frequency that is approximately twice the line frequency, 100 Hz for a 50 Hz system or 120 Hz for a 60 Hz system. Skin effect in the rotor bars at this frequency will cause a significant increase in rotor resistance and therefore, a

significant increase in rotor heating. This extra heating is not accounted for in the thermal limit curves supplied by the generator manufacturer as these curves assume positive sequence currents only that come from a perfectly balanced supply and generator design.

The 489 measures the ratio of negative to positive sequence current. The thermal model may be biased to reflect the additional heating that is caused by negative sequence current when the machine is running. This biasing is done by creating an equivalent heating current rather than simply using average current (I_{per_unit}). This equivalent current is calculated using the equation shown below.

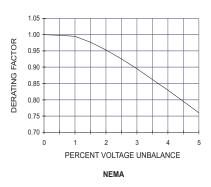
$$I_{eq} = \sqrt{I_1^2 + kI_2^2}$$
 (EQ 5.32)

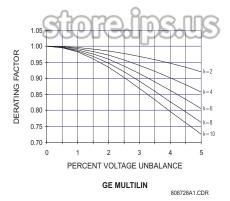
where:

 I_{eq} = equivalent motor heating current in per unit (based on FLA) I_2 = negative-sequence current in per unit (based on FLA) I_1 = positive-sequence current in per unit (based on FLA)

k = constant relating negative-sequence rotor resistance to positive-sequence rotor resistance, not to be confused with the k indicating generator negative-sequence capability for an inverse time curve.

The figure below shows induction machine derating as a function of voltage unbalance as recommended by NEMA (National Electrical Manufacturers Association). Assuming a typical inrush of $6 \times FLA$ and a negative sequence impedance of 0.167, voltage unbalances of 1, 2, 3, 4, and 5% equal current unbalances of 6, 12, 18, 24, and 30%, respectively. Based on this assumption, the GE curve illustrates the amount of machine derating for different values of k entered for the **UNBALANCE BIAS K FACTOR** setpoint. Note that the curve created when k = 8 is almost identical to the NEMA derating curve.





If a k value of 0 is entered, the unbalance biasing is defeated and the overload curve will time out against the measured per unit motor current. k may be calculated conservatively as:

$$k = \frac{175}{I_{LP}^2}$$
 (typical estimate); $k = \frac{230}{I_{LP}^2}$ (conservative estimate) (EQ 5.33)

where I_{LR} is the per-unit locked rotor current.

Machine Cooling

The 489 thermal capacity used value is reduced exponentially when the motor current is below the **OVERLOAD PICKUP** setpoint. This reduction simulates machine cooling. The cooling time constants should be entered for both stopped and running cases (the

generator is assumed to be running if current is measured or the generator is online). A machine with a stopped rotor normally cools significantly slower than one with a turning rotor. Machine cooling is calculated using the following formulae:

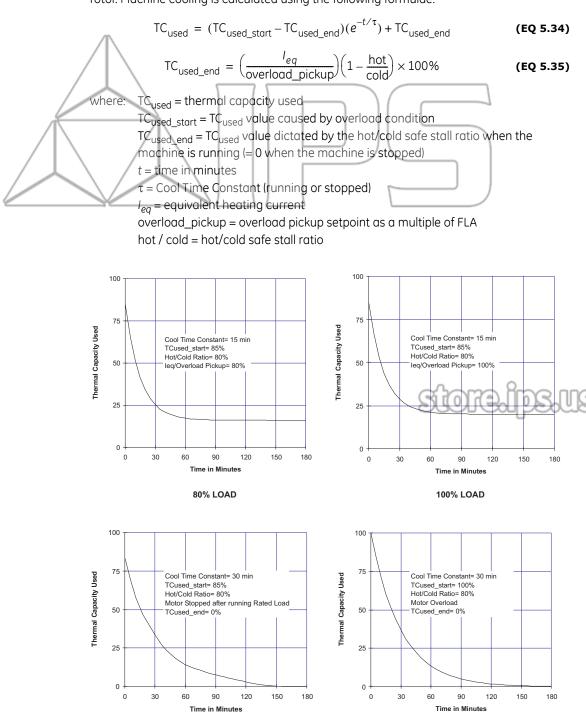


FIGURE 5-23: Thermal Model Cooling

MOTOR STOPPED

MOTOR TRIPPED

808705A2 CDR

Hot/Cold Safe Stall Ratio

When thermal limit information is available for both a hot and cold machine, the 489 thermal model will adapt for the conditions if the HOT/COLD SAFE STALL RATIO is programmed. The value entered for this setpoint dictates the level of thermal capacity used that the relay will settle at for levels of current that are below the OVERLOAD PICKUP LEVEL. When the generator is running at a level below the OVERLOAD PICKUP LEVEL, the thermal capacity used will rise or fall to a value based on the average phase current and the entered HOT/COLD SAFE STALL RATIO. Thermal capacity used will either rise at a fixed rate of 5% per minute or fall as dictated by the running cool time constant.

$$TC_{used_end} = I_{eq} \times \left(1 - \frac{hot}{cold}\right) \times 100\%$$
(EQ 5.36)

Where:
$$TC_{used_end} = \text{Thermal Capacity Used if } I_{per_unit} \text{ remains steady state}$$

$$I_{eq} = \text{equivalent generator heating current}$$

$$hot/cold = \text{HOT/COLD SAFE STALL RATIO setpoint}$$

The hot/cold safe stall ratio may be determined from the thermal limit curves, if provided, or the hot and cold safe stall times. Simply divide the hot safe stall time by the cold safe stall time. If hot and cold times are not provided, there can be no differentiation and the **HOT/COLD SAFE STALL RATIO** should be entered as "1.00".

RTD Bias

The thermal replica created by the features described in the sections above operates as a complete and independent model. However, the thermal overload curves are based solely on measured current, assuming a normal 40°C ambient and normal machine cooling. If there is an unusually high ambient temperature, or if machine cooling is blocked, generator temperature will increase. If the stator has embedded RTDs, the 489 RTD bias feature should be used to correct the thermal model.

The RTD bias feature is a two part curve, constructed using 3 points. If the maximum stator RTD temperature is below the RTD BIAS MINIMUM setpoint (typically 40°C), no biasing occurs. If the maximum stator RTD temperature is above the RTD BIAS MAXIMUM setpoint (typically at the stator insulation rating or slightly higher), then the thermal memory is fully biased and thermal capacity is forced to 100% used. At values in between, the present thermal capacity used created by the overload curve and other elements of the thermal model, is compared to the RTD Bias thermal capacity used from the RTD Bias curve. If the RTD Bias thermal capacity used value is higher, then that value is used from that point onward. The RTD BIAS CENTER POINT should be set at the rated running temperature of the machine. The 489 automatically determines the thermal capacity used value for the center point using the HOT/COLD SAFE STALL RATIO setpoint.

$$TC_{used at RBC} = \left(1 - \frac{hot}{cold}\right) \times 100\%$$
 (EQ 5.37)

At temperatures less that the RTD Bias Center temperature,

$$RTD_Bias_TC_{used} = \frac{Temp_{actual} - Temp_{min}}{Temp_{center} - Temp_{min}} \times TC_{used at RBC}$$
(EQ 5.38)

At temperatures greater than the RTD Bias Center temperature,

$$RTD_Bias_TC_{used} = \frac{Temp_{actual} - Temp_{center}}{Temp_{max} - Temp_{center}} \times (100 - TC_{used at RBC}) + TC_{used at RBC}$$
 (EQ 5.39)

where: $RTD_Bias_TC_{used} = TC$ used due to hottest stator RTD

 $Temp_{actual} = current temperature of the hottest stator RTD$

 $Temp_{min} = RTD$ Bias minimum setpoint $Temp_{center} = RTD$ Bias center setpoint $Temp_{max} = RTD$ Bias maximum setpoint

TC_{used at RBC} = TC used defined by the **HOT/COLD SAFE STALL RATIO** setpoint

In simple terms, the RTD bias feature is real feedback of measured stator temperature. This feedback acts as correction of the thermal model for unforeseen situations. Since RTDs are relatively slow to respond, RTD biasing is good for correction and slow generator heating. The rest of the thermal model is required during high phase current conditions when machine heating is relatively fast.

It should be noted that the RTD bias feature alone cannot create a trip. If the RTD bias feature forces the thermal capacity used to 100%, the machine current must be above the over-load pickup before an overload trip occurs. Presumably, the machine would trip on stator RTD temperature at that time.



No biasing occurs if the hottest stator RTD is open or short.

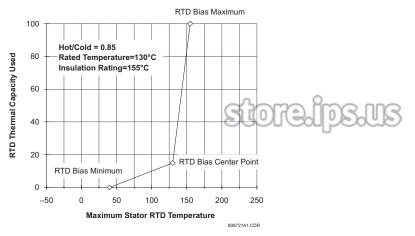
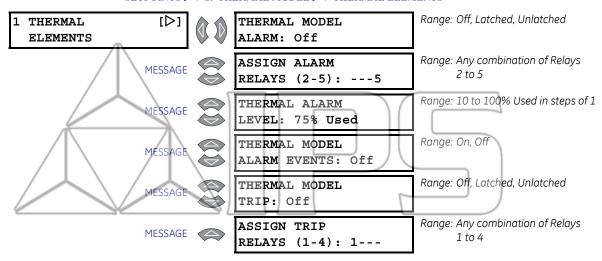


FIGURE 5-24: RTD Bias Curve

5.10.3 Thermal Elements

SETPOINTS $\triangleright \nabla$ S9 THERMAL MODEL $\triangleright \nabla$ THERMAL ELEMENTS



Once the thermal model is setup, an alarm and/or trip element can be enabled. If the generator has been offline for a long period of time, it will be at ambient temperature and thermal capacity used should be zero. If the generator is in overload, once the thermal capacity used reaches 100%, a trip will occur. The thermal model trip will remain active until a lockout time has expired. The lockout time will be based on the reduction of thermal capacity from 100% used to 15% used. This reduction will occur at a rate defined by the offline cooling time constant. The thermal capacity used alarm may be used as a warning indication of an impending overload trip.

5.11 S10 Monitoring

5.11.1 Trip Counter PATH: SETPOINTS ▷▽ S10 MONITORING ▷ TRIP COUNTER Range: Off, Latched, Unlatched TRIP COUNTER TRIP [****] ALARM: Off Range: Any combination of Relays 2 to ASSIGN ALARM MESSAGE RELAYS (2-5): ---5 Range: 1 to 50000 Trips in steps of 1 TRIP COUNTER ALARM **MESSAGE** LEVEL: 25 Trips Range: On, Off TRIP COUNTER ALARM MESSAGE EVENTS: Off

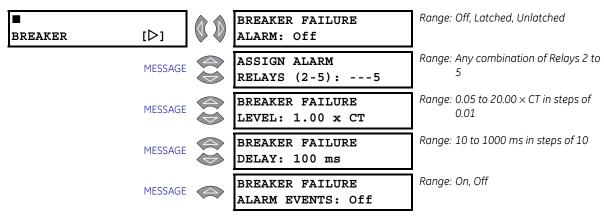
When enabled, a trip counter alarm will occur when the **TRIP COUNTER ALARM LEVEL** is reached. The trip counter must be cleared or the alarm level raised and the reset key must be pressed (if the alarm was latched) to reset the alarm.

For example, it might be useful to set a Trip Counter alarm at 100 trips, prompting the operator or supervisor to investigate the type of trips that have occurred. A breakdown of trips by type may be found in the A4 MAINTENANCE $\triangleright \nabla$ TRIP COUNTERS actual values page. If a trend is detected, it would warrant further investigation.

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5.11.2 Breaker Failure

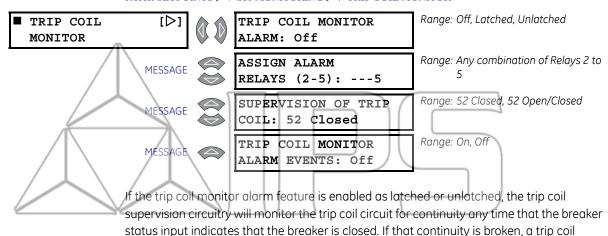
PATH: SETPOINTS $\triangleright \nabla$ S10 MONITORING $\triangleright \nabla$ BREAKER FAILURE



If the breaker failure alarm feature may be enabled as latched or unlatched. If the 1 Trip output relay is operated and the generator current measured at any of the three output CTs is above the level programmed for the period of time specified by the delay, a breaker failure alarm will occur. The time delay should be slightly longer than the breaker clearing time.

5.11.3 Trip Coil Monitor

PATH: SETPOINTS ▷▽ S10 MONITORING ▷▽ TRIP COIL MONITOR



monitor alarm will occur in approximately 300 ms.

If 52 Open/Closed is selected, the trip coil supervision circuitry monitors the trip coil circuit for continuity at all times regardless of breaker state. This requires an alternate path around the 52a contacts in series with the trip coil when the breaker is open. See the figure below for modifications to the wiring and proper resistor selection. If that continuity is broken, a Starter Failure alarm will indicate Trip Coil Supervision.

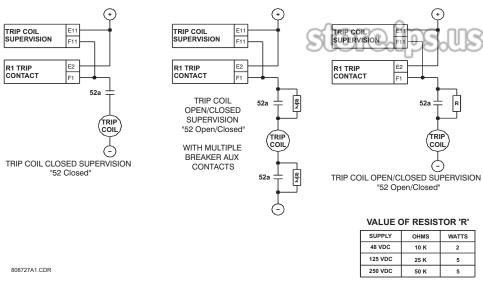
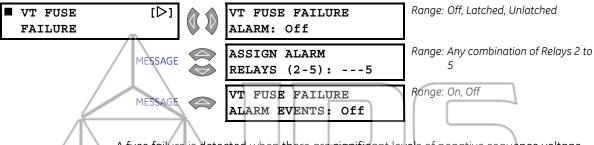


FIGURE 5–25: Trip Coil Supervision

5.11.4 VT Fuse Failure

PATH: SETPOINTS $\triangleright \nabla$ S10 MONITORING $\triangleright \nabla$ VT FUSE FAILURE



A fuse failure is detected when there are significant levels of negative sequence voltage without corresponding levels of negative sequence current measured at the output CTs. Also, if the generator is online and there is not significant positive sequence voltage, it could indicate that all VT fuses have been pulled or the VTs are racked out. If the alarm is enabled and a VT fuse failure detected, elements that could nuisance operation are blocked and an alarm occurs. These blocked elements include voltage restraint for the phase overcurrent, undervoltage, phase reversal, and all power elements.

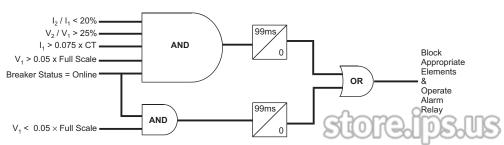
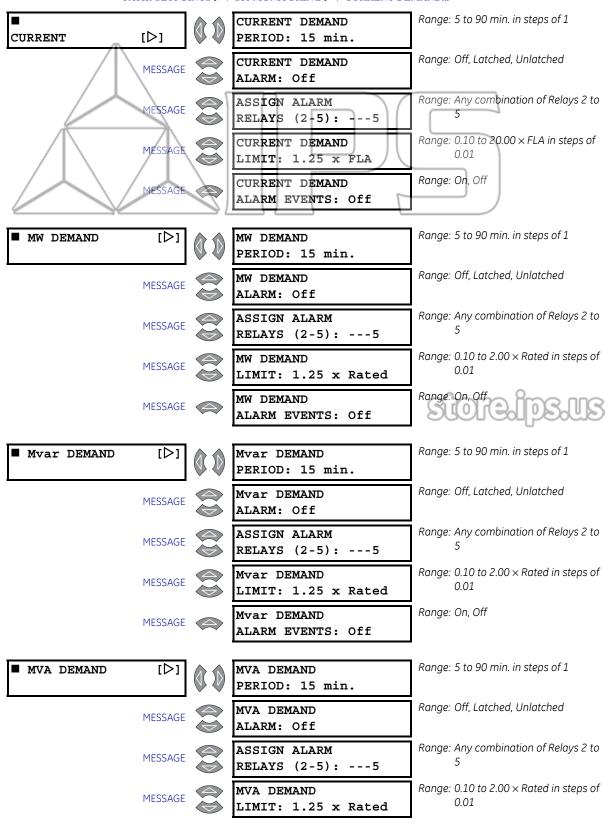


FIGURE 5-26: VT Fuse Failure Logic

5.11.5 **Demand**

PATH: SETPOINTS ▷▽ S10 MONITORING ▷▽ CURRENT DEMAND...





The 489 can measure the demand of the generator for several parameters (current, MW, Mvar, MVA). The demand values of generators may be of interest for energy management programs where processes may be altered or scheduled to reduce overall demand on a feeder. The generator FLA is calculated as:

Generator FLA =
$$\frac{\text{Generator Rated MVA}}{\sqrt{3} \times \text{Generator Rated Phase-Phase Voltage}}$$
 (EQ 5.40)

Power quantities are programmed as per unit calculated from the rated MVA and rated power factor.

Demand is calculated in the following manner. Every minute, an average magnitude is calculated for current, +MW, +Mvar, and MVA based on samples taken every 5 seconds. These values are stored in a FIFO (First In, First Out buffer). The size of the buffer is dictated by the period that is selected for the setpoint. The average value of the buffer contents is calculated and stored as the new demand value every minute. Demand for real and reactive power is only positive quantities (+MW and +Mvar).

Demand =
$$\frac{1}{N} \sum_{n=1}^{N} |\text{Average}_N|$$
 (EQ 5.41)

where: N = programmed Demand Period in minutes, n = time in minutes

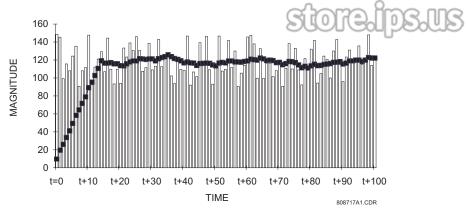
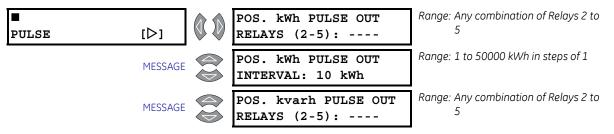
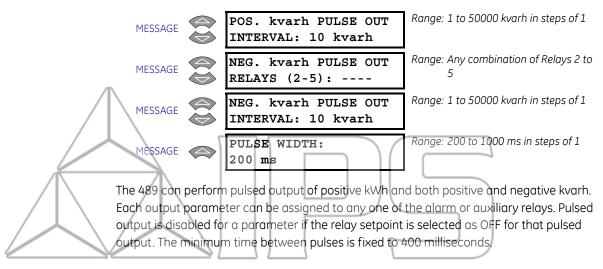


FIGURE 5-27: Rolling Demand (15 Minute Window)

5.11.6 Pulse Output

PATH: SETPOINTS $\triangleright \nabla$ S10 MONITORING $\triangleright \nabla$ PULSE OUTPUT







This feature should be programmed so that no more than one pulse per 600 milliseconds is required or the pulsing will lag behind the interval activation. Do not assign pulsed outputs to the same relays as alarms and trip functions.

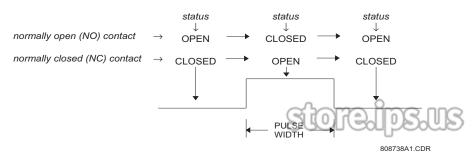
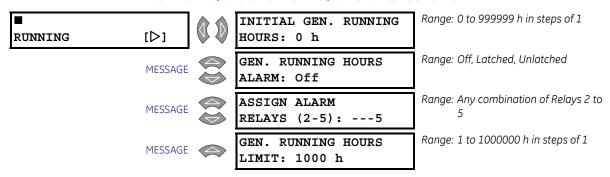


FIGURE 5-28: Pulse Output

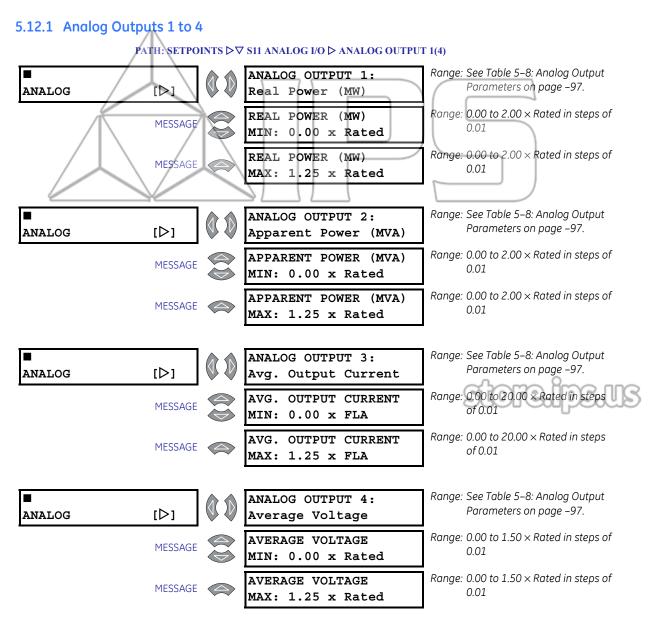
5.11.7 Running Hour Setup

PATH: SETPOINTS ▷▽ S10 MONITORING ▷▽ RUNNING HOUR SETUP



The 489 can measure the generator running hours. This value may be of interest for periodic maintenance of the generator. The initial generator running hour allows the user to program existing accumulated running hours on a particular generator the relay is protecting. This feature switching 489 relays without losing previous generator running hour values.

5.12 S11 Analog Inputs/Outputs



The 489 has four analog output channels (4 to 20 mA or 0 to 1 mA as ordered). Each channel may be individually configured to represent a number of different measured parameters as shown in the table below. The minimum value programmed represents the 4 mA output. The maximum value programmed represents the 20 mA output. All four of the outputs are updated once every 50 ms. Each parameter may only be used once.

The analog output parameter may be chosen as Real Power (MW) for a 4 to 20 mA output. If rated power is 100 MW, the minimum is set for $0.00 \times \text{Rated}$, and the maximum is set for $1.00 \times \text{Rated}$, the analog output channel will output 4 mA when the real power

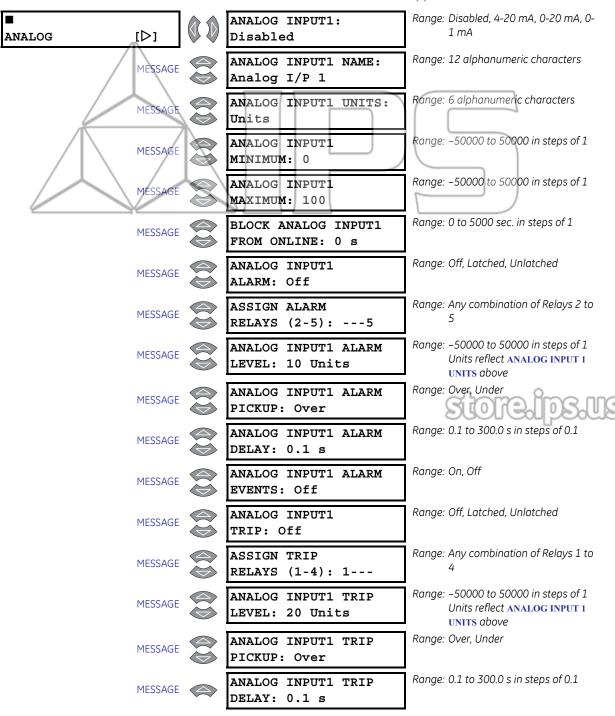
measurement is 0 MW. When the real power measurement is 50 MW, the analog output channel will output 12 mA. When the real power measurement is 100 MW, the analog output channel will output 20 mA.

Table 5–8: Analog Output Parameters

	Parameter Name	Range / Units	Step	Default		
				Min.	Max	
	IA Output Current	0.00 to 20.00 × FLA	0.01	0.00	1.25	
	IB Output Current	0.00 to 20.00 × FLA	0.01	0.00	1.25	
	IC Output Current	0.00 to 20.00 × FLA	0.01	0.00	1.25	
/	Avg. Output Current	0.00 to 20.00 × FLA	0.01	0.00	1.25	
7	Neg. Seq. Current	0 to 2000% FLA	1	0	100	
	Averaged Gen. Load	0.00 to 20.00 × FLA	0.01	0.00	1.25	
	Hottest Stator RTD	-50 to +250°C or -58 to +482°F	1	0	200	
	Hottest Bearing RTD	-50 to +250°C or -58 to +482°F	1	0	200	
	Ambient RTD	-50 to +250°C or -58 to +482°F	1	0	70	
	RTDs 1 to 12	-50 to +250°C or -58 to +482°F	1	0	200	
	AB Voltage	0.00 to 1.50 × Rated	0.01	0.00	1.25	
	BC Voltage	0.00 to 1.50 × Rated	0.01	0.00	1.25	
	CA Voltage	0.00 to 1.50 × Rated	0.01	0.00	1.25	
	Volts/Hertz	0.00 to 2.00 × Rated	0.01	0.00	1.50	
	Frequency	0.00 to 90.00 Hz	0.01	59.00	61.00	
	Neutral Volt. (3rd)	0 to 25000 V	0.1	0.0	45.0	
	Average Voltage	0.00 to 1.50 × Rated	0.01	0.00	1.25	
	Power Factor	0.01 to 1.00 lead/lag	0.01	0.8 lag	0.8 lead	
	Reactive Power (Mvar)	-2.00 to 2.00 × Rated	0.01	0.00	1.25	
	Real Power	-2.00 to 2.00 × Rated	0.01	0.00	1.25	
	Apparent Power	0.00 to 2.00 × Rated	0.01	0.00	1.25	
	Analog Inputs 1 to 4	-50000 to +50000	1	0	50000	
	Tachometer	0 to 7200 RPM	1	3500	3700	
	Thermal Capacity Used	0 to 100%	1	0	100	
	Current Demand	0.00 to 20.00 × FLA	0.01	0.00	1.25	
	Mvar Demand	0.00 to 2.00 × Rated	0.01	0.00	1.25	
	MW Demand	0.00 to 2.00 × Rated	0.01	0.00	1.25	
	MVA Demand	0.00 to 2.00 × Rated	0.01	0.00	1.25	

5.12.2 Analog Inputs 1 to 4

PATH: SETPOINTS ▷▽ S11 ANALOG I/O ▷▽ ANALOG INPUT 1(4)



There are 4 analog inputs (4 to 20 mA, 0 to 20 mA, or 0 to 1 mA) that may be used to monitor transducers such as vibration monitors, tachometers, pressure transducers, etc. These inputs may be used for alarm and/or tripping purposes. The inputs are sampled every 50 ms. The level of the analog input is also available over the communications port. With the EnerVista 489 Setup program, the level of the transducer may be trended and graphed.

Before the input may be used, it must be configured. A name may be assigned for the input, units may be assigned, and a minimum and maxi-mum value must be assigned. Also, the trip and alarm features may be blocked until the generator is online for a specified time delay. If the block time is 0 seconds, there is no block and the trip and alarm features will be active when the generator is offline or online. If a time is programmed other than 0 seconds, the feature will be disabled when the generator is offline and also from the time the machine is placed online until the time entered expires. Once the input is setup, both the trip and alarm features may be configured. In addition to programming a level and time delay, the PICKUP setpoint may be used to dictate whether the feature picks up when the measured value is over or under the level.

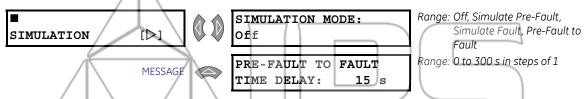
If a vibration transducer is to be used, program the name as "Vib Monitor", the units as "mm/s", the minimum as "0", the maximum as "25", and the Block From Online as "0 s". Set the alarm for a reasonable level slightly higher than the normal vibration level. Program a delay of "3 s" and the pickup as "Over".



5.13 S12 Testing

5.13.1 Simulation Mode

PATH: SETPOINTS ▷▽ S12 489 TESTING ▷ SIMULATION MODE



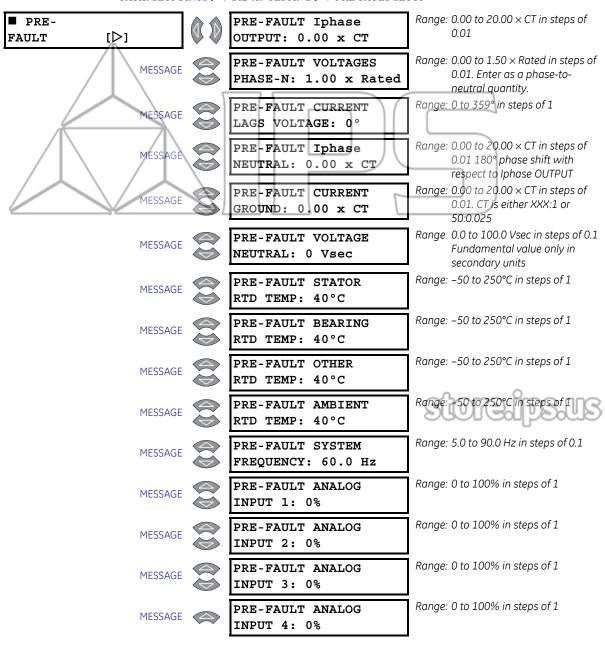
The 489 may be placed in several simulation modes. This simulation may be useful for several purposes. First, it may be used to under-stand the operation of the 489 for learning or training purposes. Second, simulation may be used during startup to verify that control circuitry operates as it should in the event of a trip or alarm. In addition, simulation may be used to verify that setpoints had been set properly in the event of fault conditions.

The **SIMULATION MODE** setpoint may be entered only if the generator is offline, no current is measured, and there are no trips or alarms active. The values entered as Pre-Fault Values will be substituted for the measured values in the 489 when the **SIMULATION MODE** is "Simulate Pre-Fault". The values entered as Fault Values will be substituted for the measured values in the 489 when the **SIMULATION MODE** is "Simulate Fault". If the **SIMULATION MODE** is set to "Pre-Fault to Fault", the Pre-Fault values will be substituted for the period of time specified by the delay, followed by the Fault values. If a trip occurs, the **SIMULATION MODE** reverts to "Off". Selecting "Off" for the **SIMULATION MODE** places the 489 back in service. If the 489 measures current or control power is cycled, the **SIMULATION MODE** automatically reverts to "Off".

If the 489 is to be used for training, it might be desirable to allow all parameter averages, statistical information, and event recording to update when operating in simulation mode. If however, the 489 has been installed and will remain installed on a specific generator, it might be desirable assign a digital input to Test Input and to short that input to prevent all of this data from being corrupted or updated. In any event, when in simulation mode, the 489 In Service LED (indicator) will flash, indicating that the 489 is not in protection mode.

5.13.2 Pre-Fault Setup

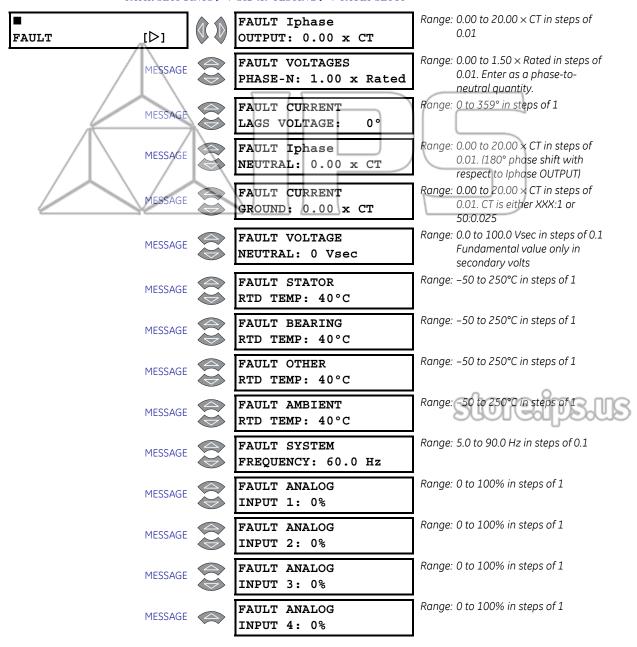
PATH: SETPOINTS ▷∇ S12 489 TESTING ▷∇ PRE-FAULT SETUP



The values entered under Pre-Fault Values will be substituted for the measured values in the 489 when the **SIMULATION MODE** is "Simulate Pre-Fault".

5.13.3 Fault Setup

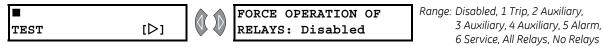
PATH: SETPOINTS ▷▽ S12 489 TESTING ▷▽ FAULT SETUP



The values entered here are substituted for the measured values in the 489 when the **SIMULATION MODE** is "Simulate Fault".

5.13.4 Test Output Relays

PATH: SETPOINTS $\triangleright \nabla$ S12 489 TESTING $\triangleright \nabla$ TEST OUTPUT RELAYS

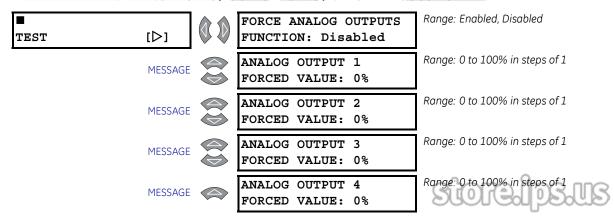


The test output relays setpoint may be used during startup or testing to verify that the output relays are functioning correctly. The output relays can be forced to operate only if the generator is offline, no current is measured, and there are no trips or alarms active. If any relay is forced to operate, the relay will toggle from its normal state. The appropriate relay indicator will illuminate at that time. Selecting "Disabled" places the output relays back in service. If the 489 measures current or control power is cycled, the force operation of relays setpoint will automatically become disabled and the output relays will revert back to their normal states.

If any relay is forced, the 489 In Service indicator will flash, indicating that the 489 is not in protection mode.

5.13.5 Test Analog Output

PATH: SETPOINTS ▷ ♥ S12 489 TESTING ▷ ♥ TEST ANALOG OUTPUT

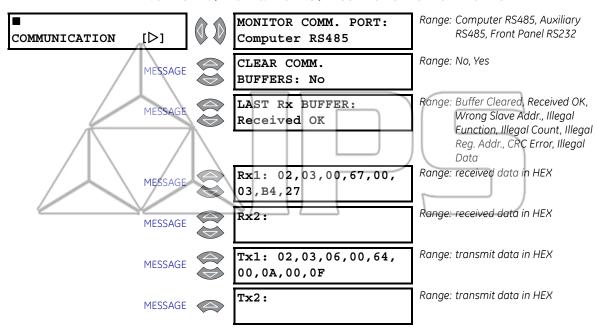


These setpoints may be used during startup or testing to verify that the analog outputs are functioning correctly. The analog outputs can be forced only if the generator is offline, no current is measured, and there are no trips or alarms active. When the **FORCE ANALOG OUTPUTS FUNCTION** is "Enabled", the output reflects the forced value as a percentage of the range 4 to 20 mA or 0 to 1 mA. Selecting "Disabled" places all four analog output channels back in service, reflecting their programmed parameters. If the 489 measures current or control power is cycled, the force analog output function is automatically disabled and all analog outputs will revert back to their normal state.

Any time the analog outputs are forced, the In Service indicator will flash, indicating that the 489 is not in protection mode.

5.13.6 Comm Port Monitor

PATH: SETPOINTS ▷ ♥ S12 489 TESTING ▷ ♥ COMMUNICATION PORT MONITOR



During communications troubleshooting, it can be useful to see the data being transmitted to the 489 from some master device, as well as the data transmitted back to that master device. The messages shown here make it possible to view that data. Any of the three communications ports may be monitored. After the communications buffers are cleared, any data received from the monitored communications port is stored in Rx1 and Rx2. If the 489 transmits a message, it appears in the Tx1 and Tx2 buffers. In addition to these buffers, there is a message indicating the status of the last received message.

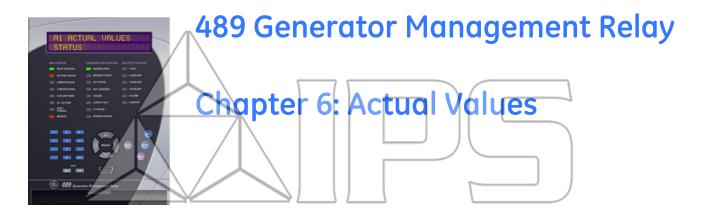
5.13.7 Factory Service

PATH: SETPOINTS ▷∇ S12 489 TESTING ▷∇ FACTORY SERVICE



This section is for use by GE Multilin personnel for testing and calibration purposes.

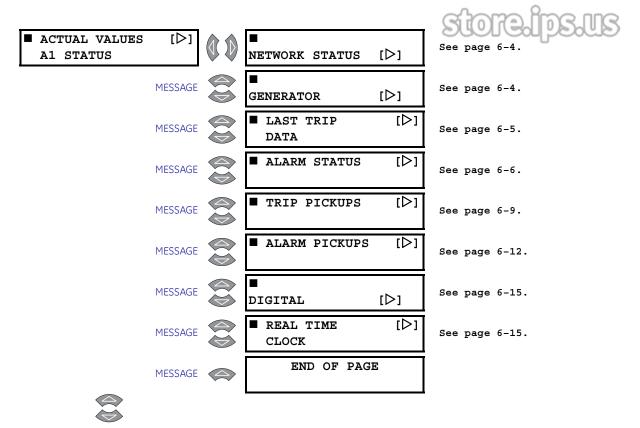


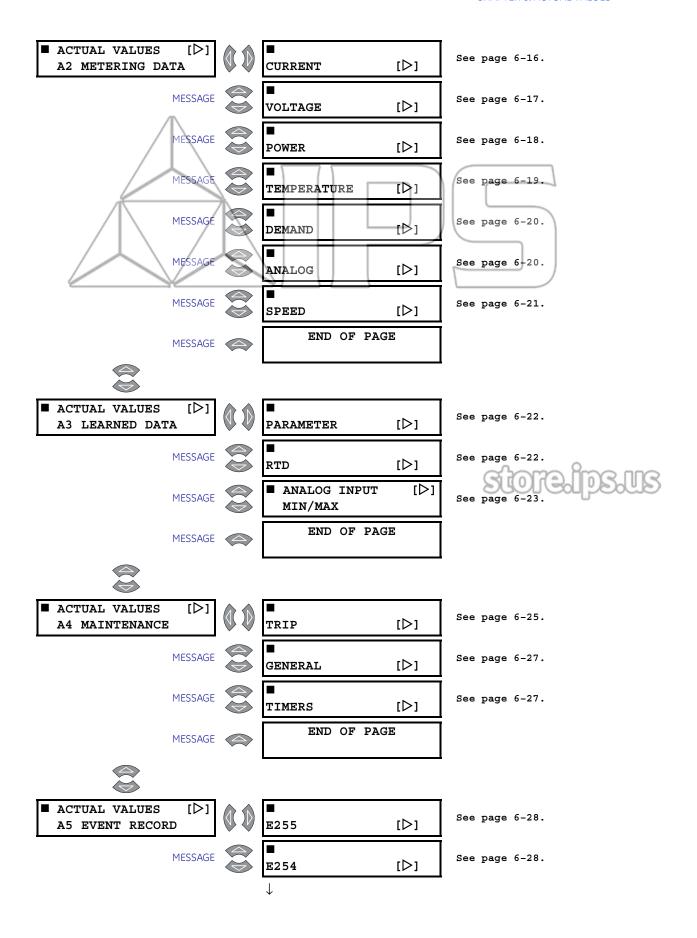


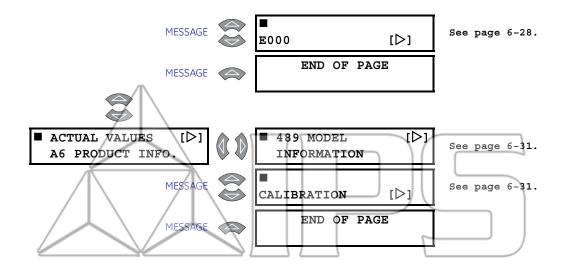
6.1 Overview

6.1.1 Actual Values Main Menu

The actual values message map is shown below.







6.1.2 Description

Measured values, maintenance and fault analysis information are accessed in the actual values. Actual values may be accessed via one of the following methods:

- 1. Front panel, using the keys and display.
- 2. Front program port and a portable computer running the EnerVista 489 Setup software supplied with the relay.
- 3. Rear terminal RS485 port and a PLC/SCADA system running user-written software.

Any of these methods can be used to view the same information. However, a computer makes viewing much more convenient since many variables may be viewed simultaneously.

Actual value messages are organized into logical groups, or pages, for easy reference, as shown below. All actual value messages are illustrated and described in blocks throughout this chapter. All values shown in these message illustrations assume that no inputs (besides control power) are connected to the 489.

In addition to the actual values, there are also diagnostic and flash messages that appear only when certain conditions occur. They are described later in this chapter.

6.2 A1 Status

6.2.1 Network Status

PATH: ACTUAL VALUES hd A1 STATUS hd hd NETWORK STATUS

This actual value appears when the relay is ordered with the Ethernet (T) option.

The ETHERNET STATUS actual value message indicates the status of the Ethernet link, connection, and diagnostic via three indicators. The [] symbol indicates on, and the [] symbol indicates off. There is also a blinking indication.

The box under LNK column indicates the Ethernet link status. If it is on, the Ethernet port is connected to the network; if it is off, the port is disconnected. This indicator is normally on.

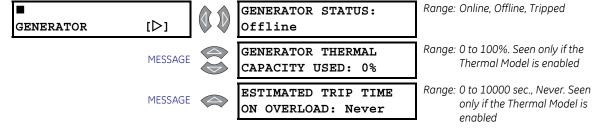
The box under the **CON** column indicates the connection status. If on, the Ethernet port is configured and ready to transmit and receive data. If blinking, the Ethernet port is either active (transmitting or receiving data) or indicating an error if the diagnostic status is also on or blinking.

The box under the **DIA** column indicates the diagnostic status. If it is on, then either a fatal Ethernet port error has occurred or there is a duplicate IP address on the network. If blinking, then there is a non-fatal network error. Off indicates no errors.

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6.2.2 Generator Status

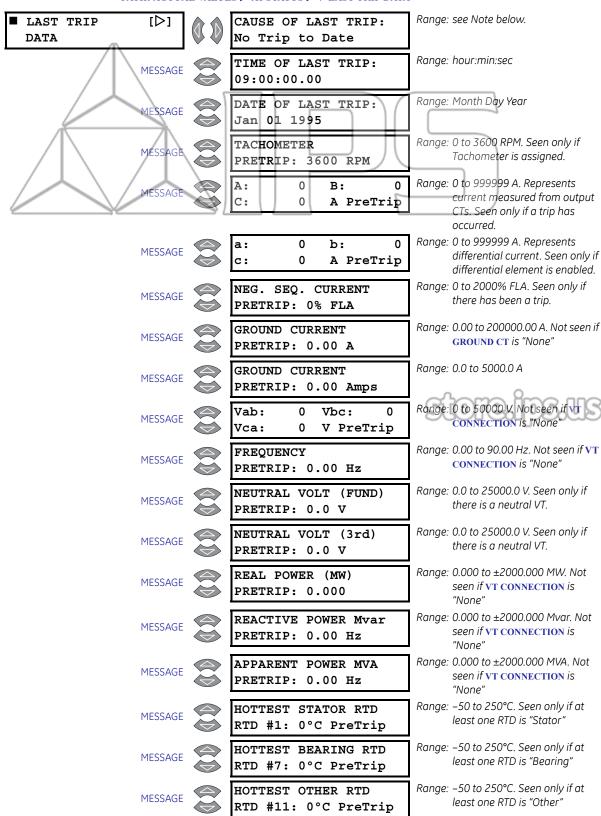
PATH: ACTUAL VALUES ▷ A1 STATUS ▷ GENERATOR STATUS

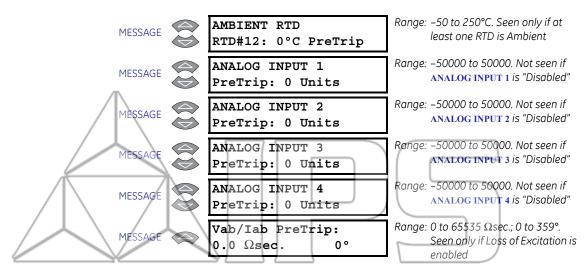


These messages describe the status of the generator at any given point in time. If the generator has been tripped, is still offline, and the 489 has not yet been reset, the **GENERATOR STATUS** will be "Tripped". The **GENERATOR THERMAL CAPACITY USED** value reflects an integrated value of both the stator and rotor thermal capacity used. The values for **ESTIMATED TRIP TIME ON OVERLOAD** will appear whenever the 489 thermal model picks up on the overload curve.

6.2.3 Last Trip Data

PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ LAST TRIP DATA





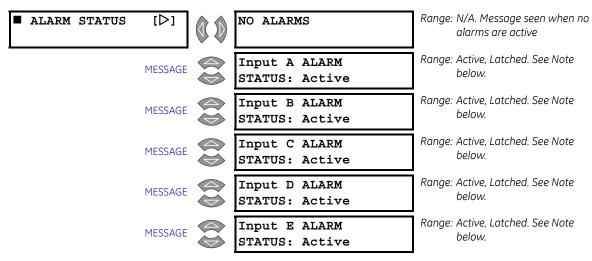


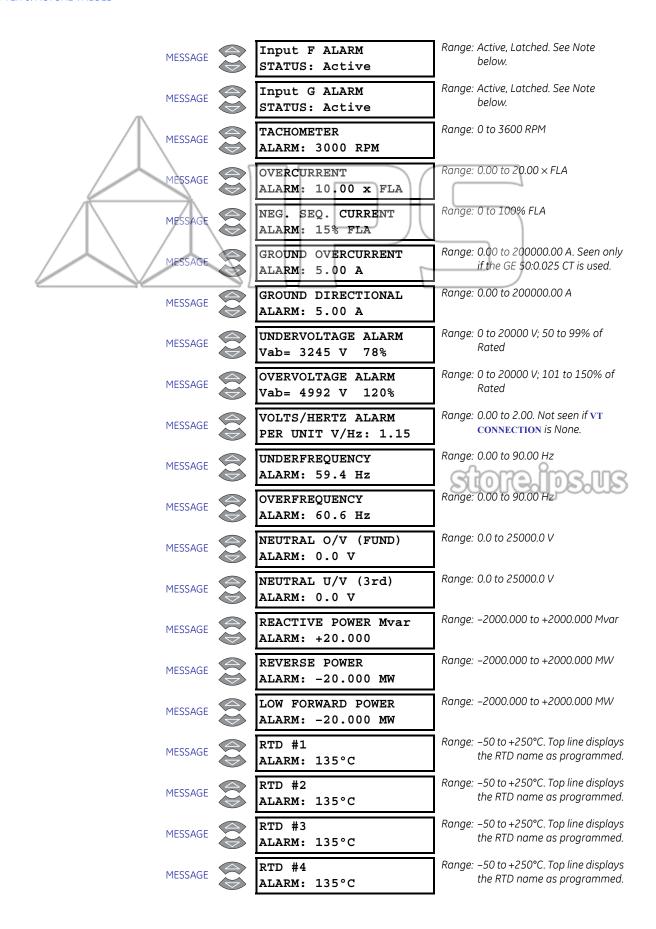
The range for the **CAUSE OF LAST TRIP** setpoint is: No Trip to Date, General Inputs A to G, Sequential Trip, Field-Bkr Discrep., Tachometer, Thermal Model, Offline Overcurrent, Phase Overcurrent, Neg. Seq. Overcurrent, Ground Overcurrent, Phase Differential, RTDs 1 to 12, Overvoltage, Undervoltage, Volts/Hertz, Phase Reversal, Underfrequency, Overfrequency, Neutral O/V, Neutral U/V (3rd), Reactive Power, Reverse Power, Low Forward Power, Inadvertent Energ., and Analog Inputs 1 to 4.

Immediately prior to issuing a trip, the 489 takes a snapshot of generator parameters and stores them as pre-trip values; this allows for troubleshooting after the trip occurs. The cause of last trip message is updated with the current trip and the screen defaults to that message. All trip features are automatically logged as date and time stamped events as they occur. This information can be cleared using the S1 489 SETUP DV CLEAR DATA DV CLEAR LAST TRIP DATA setpoint. If the cause of last trip is "No Trip To Date", the subsequent pretrip messages will not appear. Last Trip Data will not update if a digital input programmed as Test Input is shorted.

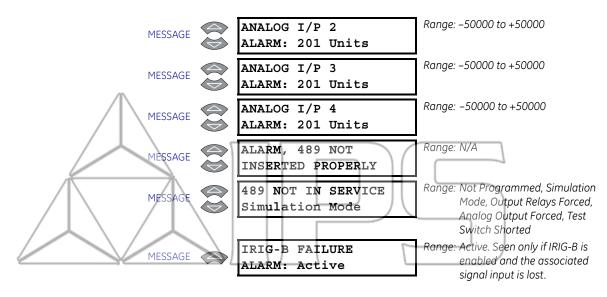
6.2.4 Alarm Status

PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ ALARM STATUS





MESSAGE	RTD #5 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #6 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #7 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #8 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #9 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #10 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #11 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	RTD #12 ALARM: 135°C	Range: –50 to +250°C. Top line displays the RTD name as programmed.
MESSAGE	OPEN SENSOR ALARM: RTD # 1 2 3 4 5 6	Range: RTDs 1 to 12
MESSAGE	SHORT/LOW TEMP ALARM RTD # 7 8 9 10 11	Range: RTDs 1 to 12
MESSAGE	THERMAL MODEL ALARM: 100% TC USED	Range: 1 to 100%
MESSAGE	TRIP COUNTER ALARM: 25 Trips	Range: 1 to 10000
MESSAGE	BREAKER FAILURE ALARM: Active	Range: Active, Latched
MESSAGE	TRIP COIL MONITOR ALARM: Active	Range: Active, Latched
MESSAGE	VT FUSE FAILURE ALARM: Active	Range: Active, Latched
MESSAGE	CURRENT DEMAND ALARM: 1053 A	Range: 1 to 999999 A
MESSAGE	MW DEMAND ALARM: 50.500	Range: -2000.000 to +2000.000 MW
MESSAGE	Mvar DEMAND ALARM: -20.000	Range: –2000.000 to +2000.000 Mvar
MESSAGE	MVA DEMAND ALARM: 20.000	Range: 0 to 2000.000 MVA
MESSAGE	GEN. RUNNING HOURS ALARM: 1000 h	Range: 0 to 1000000 hrs. Seen only if Running Hr. Alarm is enabled.
MESSAGE	ANALOG I/P 1 ALARM: 201 Units	Range: –50000 to +50000



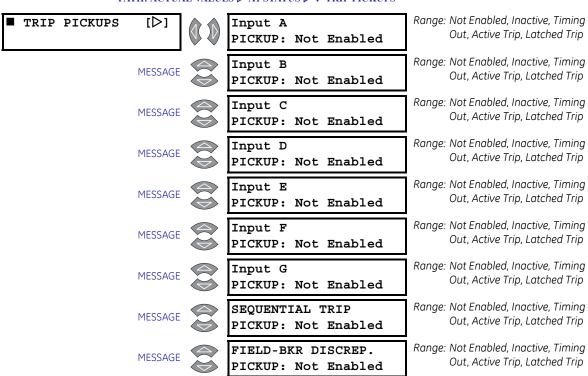
Any active or latched alarms may be viewed here.

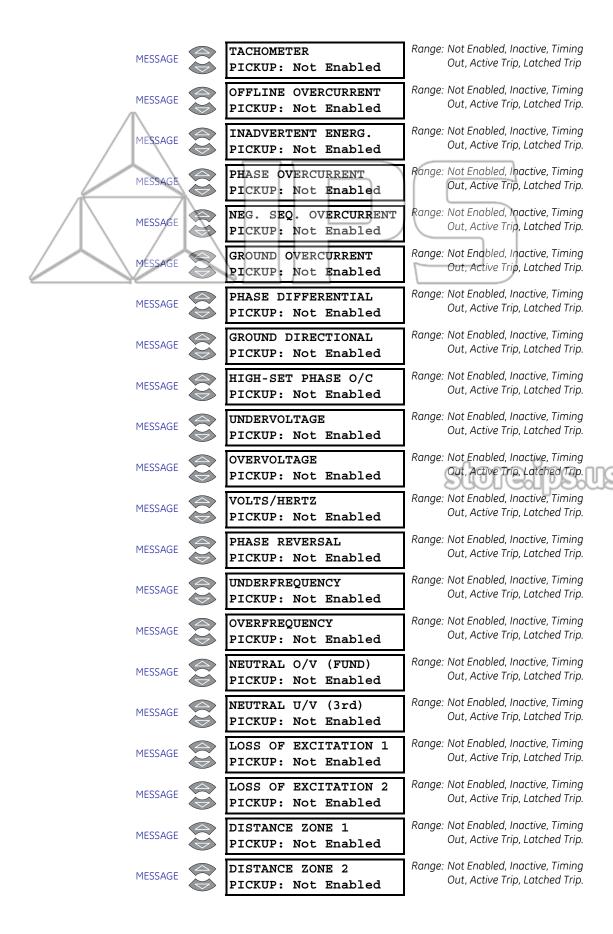
The various alarm and alarm status actual values reflect the Input Name as programmed in the first line of the message. The status is "Active" if the condition that caused the alarm is still present.

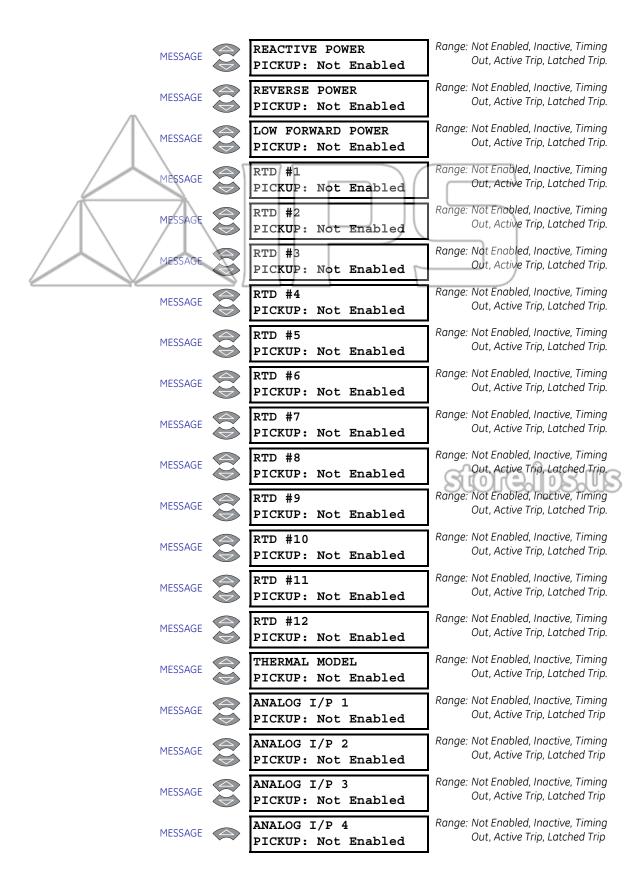
If the 489 chassis is only partially engaged with the case, the ALARM, 489 NOT INSERTED **PROPERLY** service alarm appears after 1 sec. Secure the chassis handle to ensure that all contacts mate properly.

6.2.5 Trip Pickups

PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ TRIP PICKUPS





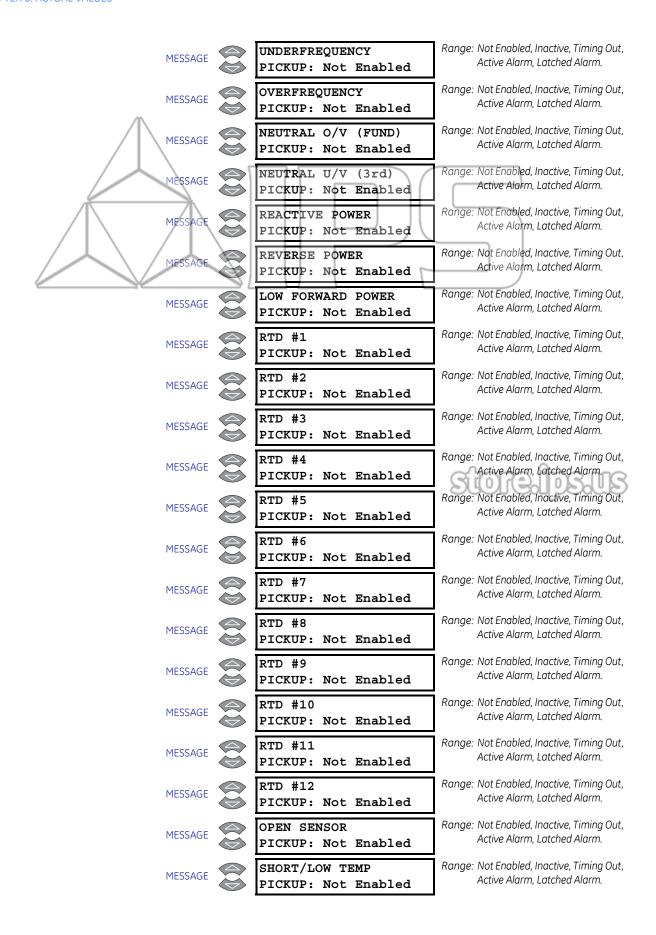


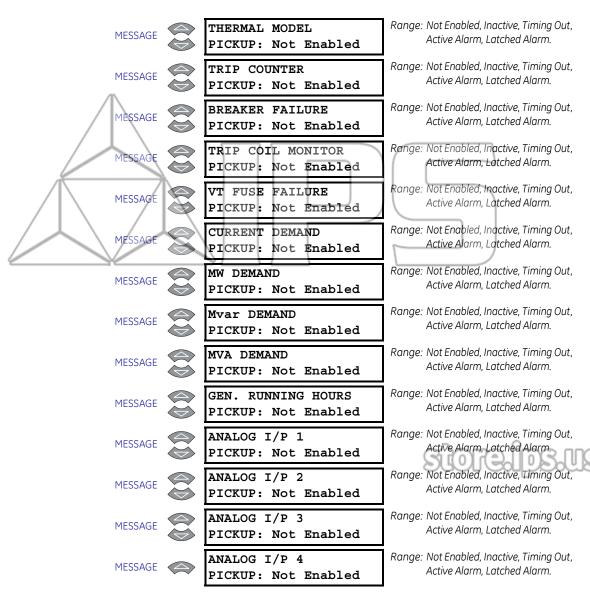


The various trip pickup actual values reflect the Input Name as programmed in the first line of the message. The various digital and analog input functions are shown only if the function has been assigned as an input.

The trip pickup messages may be very useful during testing. They will indicate if a trip feature has been enabled, if it is inactive (not picked up), timing out (picked up and timing), active trip (still picked up, timed out, and causing a trip), or latched tip (no longer picked up, but had timed out and caused a trip that is latched). These values may also be particularly useful as data transmitted to a master device for monitoring.

6.2.6 Alarm Pickups PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ ALARM PICKUPS Range: Not Enabled, Inactive, Timing Out, ALARM PICKUPS [⊳] Input A Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input B MESSAGE Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input C **MESSAGE** Active Alarm, Latched Alarm, PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input D **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input E **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input F **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, Input G **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, TACHOMETER **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, OVERCURRENT **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, NEG. SEQ. OVERCURRENT **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timina Out. GROUND OVERCURRENT **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, GROUND DIRECTIONAL **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, UNDERVOLTAGE **MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, **OVERVOLTAGE MESSAGE** Active Alarm, Latched Alarm. PICKUP: Not Enabled Range: Not Enabled, Inactive, Timing Out, VOLTS/HERTZ Active Alarm, Latched Alarm. PICKUP: Not Enabled





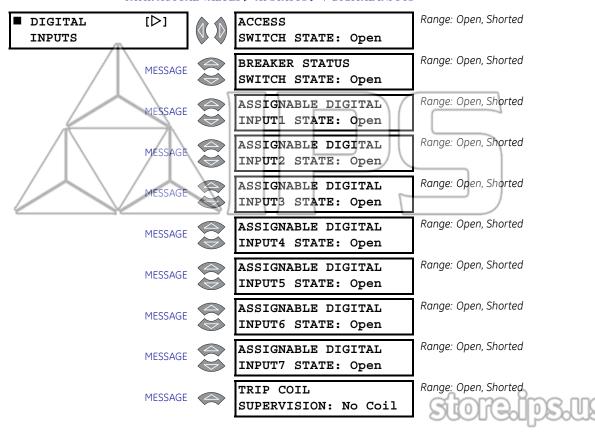


The various alarm pickup actual values reflect the Input Name as programmed in the first line of the message. The various digital and analog input functions are shown only if the function has been assigned as an input.

The alarm pickup messages may be very useful during testing. They will indicate if a alarm feature has been enabled, if it is inactive (not picked up), timing out (picked up and timing), active alarm (still picked up, timed out, and causing an alarm), or latched alarm (no longer picked up, but had timed out and caused a alarm that is latched). These values may also be particularly useful as data transmitted to a master device for monitoring.

6.2.7 Digital Inputs

PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ DIGITAL INPUTS



The messages shown here may be used to monitor digital input status. This may be useful during relay testing or during installation.

6.2.8 Real Time Clock

PATH: ACTUAL VALUES ▷ A1 STATUS ▷ ♡ REAL TIME CLOCK



The time and date from the 489 real time clock may be viewed here.

6.3 **A2 Metering Data**

6.3.1 **Current Metering** PATH: ACTUAL VALUES ▷▽ A2 METERING DATA ▷ CURRENT METERING Range: 0 to 999999 A 0 в: 0 CURRENT [] 0 Amps Range: 0 to 999999 A 0 b: 0 a: MESSAGE 0 Neut.Amps c: Range: 0 to 999999 A 0 b: **MESSAGE** c: 0 Diff.Amps Range: 0 to 999999 A AVERAGE PHASE MESSAGE CURRENT: 0 Amps Range: 0 to 2000% FLA GENERATOR LOAD: MESSAGE 0% FLA Range: 0 to 2000% FLA NEGATIVE SEQUENCE MESSAGE CURRENT: 0% FLA Range: 0 to 999999 A, 0 to 359° CURRENT: PHASE A MESSAGE 0 A Lag Range: 0 to 999999 A, 0 to 359° PHASE B CURRENT: **MESSAGE** Lag Range: 0 to 999999 A, 0 to 359° PHASE C CURRENT: MESSAGE 0° Lag Range: 0 to 999999 A, 0 to 359° NEUT. END A CURRENT: MESSAGE 0° Lag Range: 0 to 999999 A, 0 to 359° NEUT. END B CURRENT: MESSAGE 0° Lag Range: 0 to 999999 A, 0 to 359° NEUT. END C CURRENT: MESSAGE 0° Lag Range: 0 to 999999 A, 0 to 359° DIFF. A CURRENT: **MESSAGE** 0° Lag 0 A Range: 0 to 999999 A, 0 to 359° DIFF. B CURRENT: MESSAGE 0 A 0° Lag Range: 0 to 999999 A, 0 to 359° DIFF. C CURRENT: **MESSAGE** 0° Lag 0 A Range: 0.0 to 200000.0 A, 0 to 359°. GROUND CURRENT: **MESSAGE** Seen only if 1 A or 5 A Ground 0.0 A 0° Lag CT is used Range: 0.00 to 100.00 A, 0 to 359°. GROUND CURRENT: MESSAGE Seen only if 50:0.025 CT is used

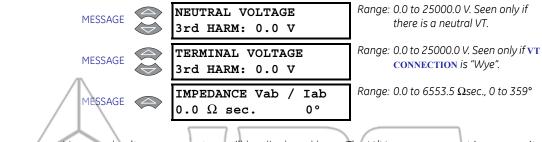
0.00 A

0° Lag

All measured current values are displayed here. **A, B, C AMPS** represent the output side CT measurements: **A, B, C NEUT. AMPS** the neutral end CT measurements, and **A, B, C DIFF. AMPS** the differential operating current calculated as the vector difference between the output side and the neutral end CT measurements on a per phase basis. The 489 negative-sequence current is defined as the ratio of negative-sequence current to generator rated FLA, I_2 / FLA × 100%. The generator full load amps is calculated as: generator rated MVA / ($\sqrt{3}$ × generator phase-to-phase voltage). Polar coordinates for measured currents are also shown using Va (wye connection) or Vab (open delta connection) as a zero angle reference vector. In the absence of a voltage signal (Va or Vab), the IA output current is used as the zero angle reference vector.

6.3.2 Voltage Metering

PATH: ACTUAL VALUES $\triangleright \nabla$ A2 METERING DATA $\triangleright \nabla$ VOLTAGE METERING Range: 0 to 50000 V. Not seen if VT 0 Vab: Vbc: **CONNECTION** is "None". VOLTAGE [D] Vca: Volts Range: 0 to 50000 V. Not seen if VT AVERAGE LINE **MESSAGE CONNECTION** is "None". VOLTAGE: 0 Volts Range: 0 to 50000 V. Not seen if VT 0 0 Vbn: **MESSAGE CONNECTION** is "Wye". 0 Vcn: Volts Range: 0 to 50000 V. Not seen if VT AVERAGE PHASE **MESSAGE CONNECTION** is "Wye". VOLTAGE: 0 Volts Range: 0 to 50000 V, 0 to 359°. Not LINE A-B VOLTAGE: MESSAGE seen if VT CONNECTION is 0° Lag 0 V "None". Range: as above LINE B-C VOLTAGE: Range: as above LINE C-A VOLTAGE: **MESSAGE** 0 V 0° Lag Range: 0 to 50000 V, 0 to 359°. Not **MESSAGE** seen if **VT CONNECTION** is "Wye". Range: as above PHASE B-N VOLTAGE: **MESSAGE** 0° Lag Range: as above PHASE C-N VOLTAGE: **MESSAGE** Range: 0.00 to 2.00. Not seen if VT PER UNIT MEASUREMENT **MESSAGE CONNECTION** is "None". OF V/Hz: 0.00 Range: 0.00 to 90.00 Hz. Not seen if VT FREQUENCY: **MESSAGE CONNECTION** is "None". 0.00 Hz Range: 0.0 to 25000.0 V. Seen only if NEUTRAL VOLTAGE **MESSAGE** there is a neutral VT. FUND: 0.0 V

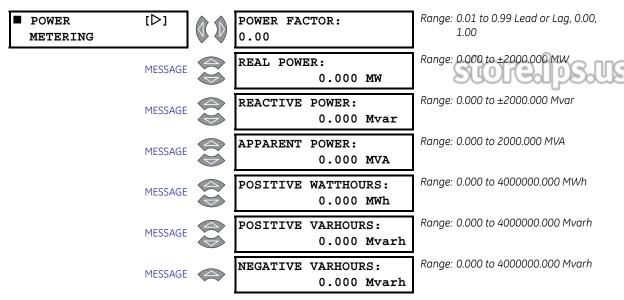


Measured voltage parameters will be displayed here. The V/Hz measurement is a per unit value based on Vab voltage/measured frequency divided by generator phase-to-phase nominal voltage/nominal system frequency. Polar coordinates for measured phase and/or line voltages are also shown using Va (wye connection) or Vab (open delta connection) as a zero angle reference vector. In the absence of a voltage signal (Va or Vab), IA output current is used as the zero angle reference vector.

If VT CONNECTION TYPE is programmed as "None" and NEUTRAL VOLTAGE TRANSFORMER is "No" in S2 SYSTEM, the **THIS FEATURE NOT PROGRAMMED** flash message will appear when an attempt is made to enter this group of messages.

6.3.3 Power Metering

PATH: ACTUAL VALUES $\triangleright \nabla$ A2 METERING DATA $\triangleright \nabla$ POWER METERING



The values for power metering appear here. Three-phase total power quantities are displayed here. Watthours and varhours are also shown here. Watthours and varhours will not update if a digital input programmed as Test Input is shorted.

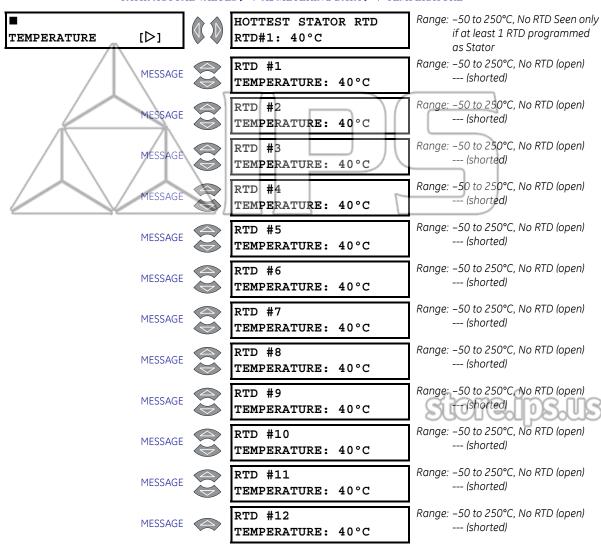


An induction generator, by convention generates Watts and consumes vars (+W and -vars). A synchronous generator can also generate vars (+vars).

If the VT CONNECTION TYPE is programmed as "None", the **THIS FEATURE NOT PROGRAMMED** flash message will appear when an attempt is made to enter this group of messages.

6.3.4 Temperature

PATH: ACTUAL VALUES ▷ ♥ A2 METERING DATA ▷ ♥ TEMPERATURE



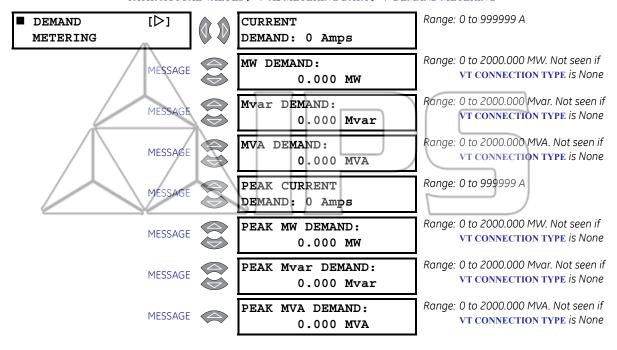


These messages are seen only if the corresponding RTDs are programmed. The actual messages reflect the RTD Names as programmed.

The current level of the 12 RTDs will be displayed here. If the RTD is not connected, the value will be "No RTD". If the RTD is shorted, then "---" will be displayed. If no RTDs are programmed in the **57 RTD TEMPERATURE** setpoints menu, the **THIS FEATURE NOT PROGRAMMED** flash message will appear when an attempt is made to enter this group of messages.

6.3.5 Demand Metering

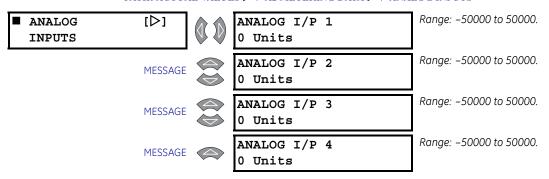
PATH: ACTUAL VALUES $\triangleright \nabla$ A2 METERING DATA $\triangleright \nabla$ DEMAND METERING



The values for current and power demand are shown here. This peak demand information can be cleared using the S1 489 SETUP $\triangleright \nabla$ CLEAR DATA $\triangleright \nabla$ CLEAR PEAK DEMAND setpoint. Demand is shown only for positive real and positive reactive power (+Watts, +vars). Peak demand will not update if a digital input programmed as Test Input is shorted.

6.3.6 Analog Inputs

PATH: ACTUAL VALUES $\triangleright \nabla$ A2 METERING DATA $\triangleright \nabla$ ANALOG INPUTS



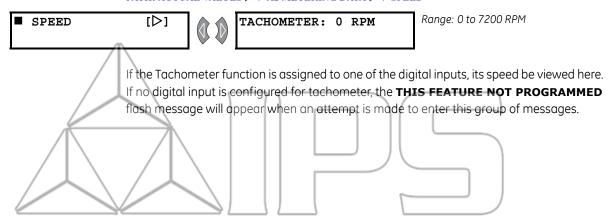


These messages are seen only if the corresponding Analog Inputs are programmed. The actual messages reflect the Analog Input Names as programmed.

The values for analog inputs are shown here. The name of the input and the units will reflect those programmed for each input. If no analog inputs are programmed in the S11 ANALOG I/O setpoints page, the **THIS FEATURE NOT PROGRAMMED** flash message will appear when an attempt is made to enter this group of messages.

6.3.7 Speed

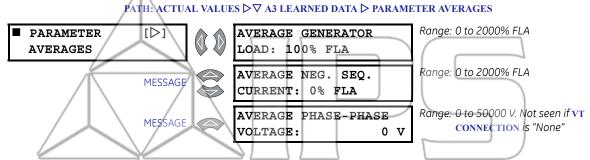
PATH: ACTUAL VALUES $\triangleright \nabla$ A2 METERING DATA $\triangleright \nabla$ SPEED





6.4 A3 Learned Data

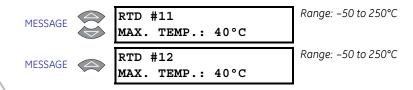
6.4.1 Parameter Averages



The 489 calculates the average magnitude of several parameters over a period of time. This time is specified by \$1 489 SETUP >> PREFERENCES >> PARAMETER AVERAGES CALC. PERIOD setpoint (default 15 minutes). The calculation is a sliding window and is ignored when the generator is offline (that is, the value that was calculated just prior to going offline will be held until the generator is brought back online and a new calculation is made). Parameter averages will not update if a digital input programmed as Test Input is shorted.

6.4.2 RTD Maximums





These messages are seen only if the corresponding RTDs are programmed. The actual messages reflect the RTD Names as programmed.

The 489 will learn the maximum temperature for each RTD. This information can be cleared using the \$1 489 SETUP >> CLEAR DATA >> CLEAR RTD MAXIMUMS setpoint. The RTD maximums will not update if a digital input programmed as Test Input is shorted. If no RTDs are programmed in the \$7 RTD TEMPERATURE setpoints page, the THIS FEATURE NOT PROGRAMMED flash message will appear when an attempt is made to enter this group of messages.

6.4.3 Analog Input Min/Max

PATH: ACTUAL VALUES ▷∇ A3 LEARNED DATA ▷∇ ANALOG INPUT MIN/MAX

■ ANALOG INPUT MIN/MAX	[▷]	ANALOG I/P 1 MIN: O Units	Range: –50000 to 50000
M	1ESSAGE	ANALOG I/P 1 MAX: 0 Units	Range: –50000 to 50000
M	1ESSAGE	ANALOG I/P 2 MIN: O Units	Range: -50000 to 50000
M	1ESSAGE	ANALOG I/P 2 MAX: 0 Units	Range: –50000 to 50000
М	1ESSAGE	ANALOG I/P 3 MIN: O Units	Range: –50000 to 50000
M	1ESSAGE	ANALOG I/P 3 MAX: 0 Units	Range: –50000 to 50000
M	1ESSAGE	ANALOG I/P 4 MIN: O Units	Range: –50000 to 50000
M	1ESSAGE	ANALOG I/P 4 MAX: 0 Units	Range: –50000 to 50000



These messages are seen only if the corresponding Analog Inputs are programmed. The actual messages reflect the Analog Input Names as programmed.

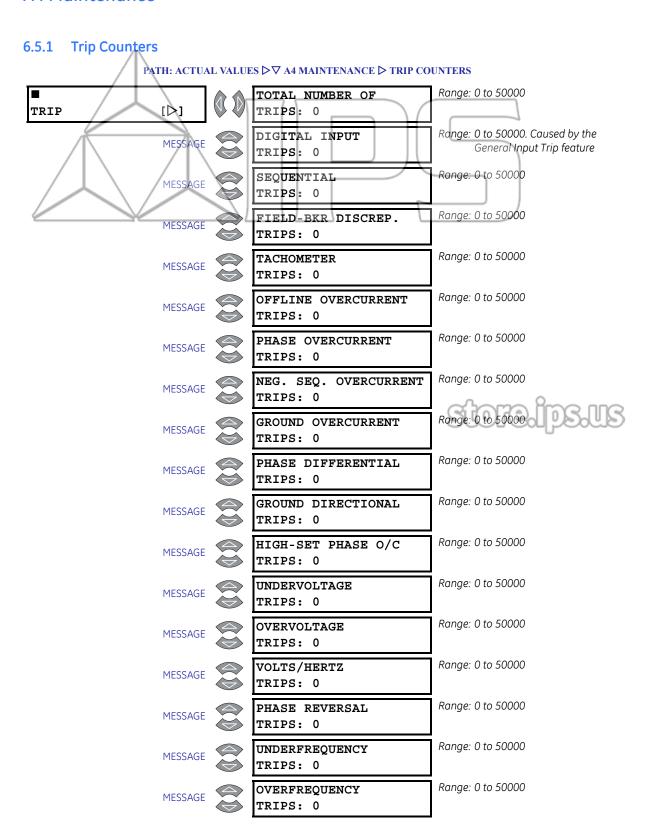
The 489 learns the minimum and maximum values of the analog inputs since they were last cleared. This information can be cleared using the S1 489 SETUP $\triangleright \nabla$ CLEAR DATA $\triangleright \nabla$ CLEAR ANALOG I/P MIN/MAX setpoint. When the data is cleared, the present value of each analog input will be loaded as a starting point for both minimum and maximum. The name of the input and the units will reflect those programmed for each input. Analog Input minimums and maximums will not update if a digital input programmed as Test Input is shorted.

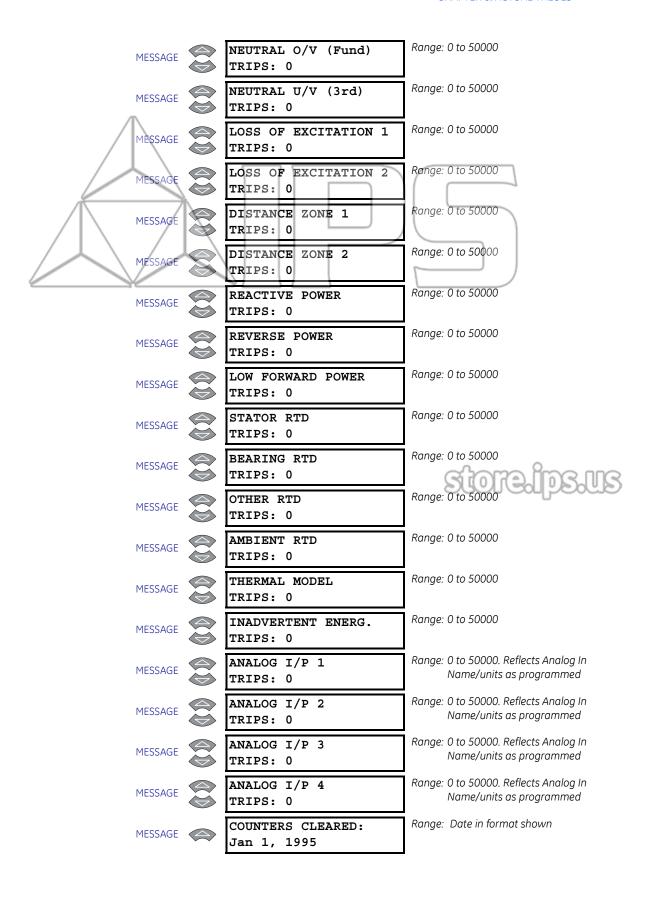
If no Analog Inputs are programmed in the S11 ANALOG I/O setpoints menu, the **THIS FEATURE NOT PROGRAMMED** flash message will appear when an attempt is made to enter this group of messages.



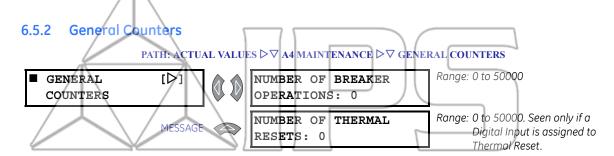
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6.5 A4 Maintenance





The number of trips by type is displayed here. When the total reaches 50000, all counters reset. This information can be cleared with the S1 489 SETUP $\triangleright \nabla$ CLEAR DATA $\triangleright \nabla$ CLEAR TRIP COUNTERS setpoint. Trip counters will not update if a digital input programmed as Test Input is shorted. In the event of multiple trips, the only the first trip will increment the trip counters.



One of the 489 general counters will count the number of breaker operations over time. This may be useful information for breaker maintenance. The number of breaker operations is incremented whenever the breaker status changes from closed to open and all phase currents are zero. Another counter counts the number of thermal resets if one of the assignable digital inputs is assigned to thermal reset. This may be useful information when troubleshooting. When either of these counters exceeds 50000, that counter will reset to 0.

The Number of Breaker Operations counter can also be cleared using the S1 489 SETUP $\triangleright \nabla$ CLEAR DATA $\triangleright \nabla$ CLEAR BREAKER INFORMATION SETPOINT. The NUMBER OF THERMAL RESETS counter can be cleared using the S1 489 SETUP $\triangleright \nabla$ GLEAR DATA $\triangleright \nabla$ CLEAR GENERATOR INFORMATION SETPOINT.

The number of breaker operations will not update if a digital input programmed as Test Input is shorted.

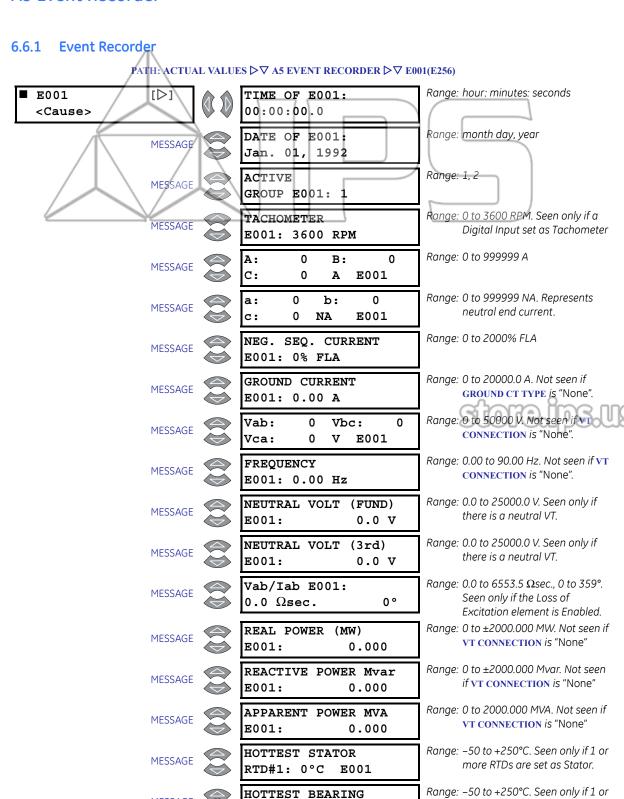
6.5.3 Timers

PATH: ACTUAL VALUES ▷ ♥ A4 MAINTENANCE ▷ ♥ TIMERS



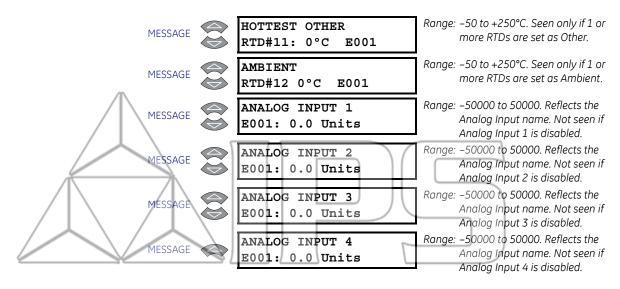
The 489 accumulates the total online time for the generator. This may be useful for scheduling routine maintenance. When this timer exceeds 1000000, it resets to 0. This timer can be cleared using the S1 489 SETUP $\triangleright \nabla$ CLEAR DATA $\triangleright \nabla$ CLEAR GENERATOR INFORMATION setpoint. The generator hours online will not update if a digital input programmed as Test Input is shorted.

6.6 A5 Event Recorder



RTD#7: 0°C

more RTDs are set as Bearing.



The 489 Event Recorder stores generator and system information each time an event occurs. The description of the event is stored and a time and date stamp is also added to the record.



The event recorder data may be inaccurate if 489 relay power-on time is less than 2 seconds.

The date and time stamping feature allows reconstruction of the sequence of events for troubleshooting. Events include all trips, any alarm optionally (except Service Alarm, and 489 Not Inserted Alarm, which always records as events), loss of control power, application of control power, thermal resets, simulation, serial communication starts/stops, and general input control functions optionally.

E001 is the most recent event and E256 is the oldest event. Each new event bumps the other event records down until the 256th event is reached. The 256th event record is lost when the next event occurs. This information can be cleared using S1 489 SETUP ▷ ▼ CLEAR DATA ▷ ▼ CLEAR EVENT RECORD setpoint. The event record will not update if a digital input programmed as Test Input is shorted.

TRIPS Ambient RTD12 Trip * Analog I/P 1 to 4 Trip * Bearing RTD 7 Trip * Bearing RTD 8 Trip * Bearing RTD 9 Trip * Bearing RTD 10 Trip * Differential Trip Distance Zone 1 Trip Distance Zone 2 Trip Field-Bkr Discr. Trip **Gnd Directional Trip** Ground O/C Trip Inadvertent Energization Hiset Phase O/C Trip Input A to G Trip * Loss of Excitation 1 Trip Loss of Excitation 2 Low Fwd Power Trip Neg Seq O/C Trip Neutral O/V Trip Neut. U/V (3rd) Trip Offline O/C Trip Overfrequency Trip Overvoltage Trip

Table 6-1: Cause of Events (Sheet 1 of 2)

^{*} reflects the name as programmed

Table 6–1: Cause of Events (Sheet 2 of 2)

TRIPS							
Phase O/C Trip	Phase Reversal Trip	Reactive Power Trip	Reverse Power Trip				
RTD11 Trip *	Sequential Trip	Stator RTD 1 Trip *	Stator RTD 2 Trip *				
Stator RTD 3 Trip *	Stator RTD 4 Trip *	Stator RTD 5 Trip *	Stator RTD 6 Trip *				
Tachometer Trip	Thermal Model Trip	Underfrequency Trip	Undervoltage Trip				
Volts/Hertz Trip							
ALARMS (OPTIONAL EVENTS)							
489 Not Inserted	Ambient RTD12 Alarm *	Analog I/P 1 to 4 Alarm	Bearing RTD 7 Alarm *				
Bearing RTD 8 Alarm *	Bearing RTD 9 Alarm *	Bearing RTD 10 Alarm *	Breaker Failure				
Current Demand Alarm	Gnd Directional Alarm	Ground O/C Alarm	Input A to G Alarm *				
Low Fwd Power Alarm	MVA Demand Alarm	Mvar Demand Alarm	MW Demand Alarm				
NegSeq Current Alarm	Neut. U/V 3rd Alarm	Neutral O/V Alarm	Open RTD Alarm				
Overcurrent Alarm	Overfrequency Alarm	Overvoltage Alarm	Reactive Power Alarm				
Reverse Power Alarm	RTD11 Alarm *	Service Alarm	Short/Low RTD Alarm				
Stator RTD 1 Alarm	Stator RTD 2 Alarm	Stator RTD 3 Alarm	Stator RTD 4 Alarm				
Stator RTD 5 Alarm	Stator RTD 6 Alarm	Tachometer Alarm	Thermal Model Alarm				
Trip Coil Monitor	Trip Counter Alarm	Underfrequency Alarm	Undervoltage Alarm				
Volts Per Hertz Alarm	VT Fuse Fail Alarm						
OTHER							
Control Power Applied	Control Power Lost	Dig I/P Waveform Trig	Input A to G Control *				
Serial Comm. Start	Serial Comm. Stop	Serial Waveform Trip	Setpoint 1 Active				
Setpoint 2 Active	Simulation Started	Simulation Stopped	Thermal Reset Close				

^{*} reflects the name as programmed

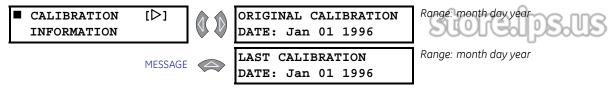
6.7 A6 Product Information

6.7.1 489 Model Info PATH: ACTUAL VALUES ▷∇ A6 PRODUCT INFO ▷ 489 MODEL INFO ■ 489 MODEL ORDER CODE: Range: N/A INFORMATION 489-P5-HI-A20 Range: N/A 489 SERIAL NO: MESSAGE A3260001 Range: N/A 489 REVISION: MESSAGE 32E100A4.000 Range: N/A 489 BOOT REVISION: MESSAGE 30K401A0.000

All of the 489 model information may be viewed here when the unit is powered up. In the event of a product software upgrade or service question, the information shown here should be jotted down prior to any inquiry.

6.7.2 Calibration Info

PATH: ACTUAL VALUES $\triangleright \nabla$ A6 PRODUCT INFO $\triangleright \nabla$ CALIBRATION INFO



The date of the original calibration and last calibration may be viewed here.

6.8 Diagnostics

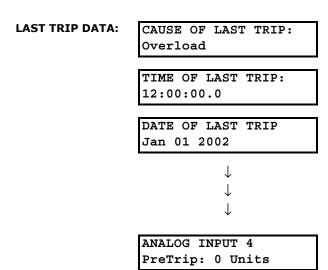
6.8.1 Diagnostic Messages

In the event of a trip or alarm, some of the actual value messages are very helpful in diagnosing the cause of the condition. The 489 will automatically default to the most important message. The hierarchy is trip and pretrip messages, then alarm messages. In order to simplify things for the operator, the Message LED (indicator) will flash prompting the operator to press the MESSAGE ▶ key. When the MESSAGE ▶ key is pressed, the 489 will automatically display the next relevant message and continue to cycle through the messages with each keypress. When all of these conditions have cleared, the 489 will revert back to the normal default messages.

Any time the 489 is not displaying the default messages because other actual value or setpoint messages are being viewed and there are no trips or alarms, the Message LED (indicator) will be on solid. From any point in the message structure, pressing the MESSAGE ▶ key will cause the 489 to revert back to the normal default messages. When normal default messages are being displayed, pressing the MESSAGE ▶ key will cause the 489 to display the next default message immediately.

EXAMPLE:

If a thermal model trip occurred, an RTD alarm may also occur as a result of the overload. The 489 would automatically default to the CAUSE OF LAST TRIP message at the top of the AI STATUS ▷ V LAST TRIP DATA queue and the Message LED would flash. Pressing the MESSAGE ▶ key cycles through the time and date stamp information as well as all of the pre-trip data. When the bottom of this queue is reached, an additional press of the MESSAGE ▶ key would normally return to the top of the queue. However, because there is an alarm active, the display will skip to the alarm message at the top of the AI STATUS ▷ V ALARM STATUS queue. Finally, another press of the MESSAGE ▶ key will cause the 489 to return to the original CAUSE OF LAST TRIP message, and the cycle could be repeated.



ACTIVE ALARMS:

STATOR RTD #1 ALARM: 135°C

START BLOCK LOCKOUTS:

OVERLOAD LOCKOUT BLOCK: 25 min

When the RESET has been pressed and the hot RTD condition is no longer present, the display will revert back to the normal default messages.

6.8.2 / Flash Messages

Flash messages are warning, error, or general information messages that are temporarily displayed in response to certain key presses. These messages are intended to assist with navigation of the 489 messages by explaining what has happened or by prompting the user to perform certain actions.

Table 6–2: Flash Messages

[.] KEY IS USED TO ADVANCE THE CURSOR	ACCESS DENIED, ENTER PASSCODE	ACCESS DENIED, SHORT ACCESS SWITCH	ALL POSSIBLE RESETS HAVE BEEN PERFORMED	ARE YOU SURE? PRESS [ENTER] TO VERIFY
DATA CLEARED SUCCESSFULLY	DATE ENTRY OUT OF RANGE	DATE ENTRY WAS NOT COMPLETE	DEFAULT MESSAGE HAS BEEN ADDED	DEFAULT MESSAGE HAS BEEN REMOVED
DEFAULT MESSAGE LIST IS FULL	DEFAULT MESSAGES 6 TO 20 ARE ASSIGNED	END OF LIST	END OF PAGE	ENTER A NEW PASSCODE FOR ACCESS
INVALID PASSCODE ENTERED!	INVALID SERVICE CODE ENTERED	KEY PRESSED IS INVALID HERE	NEW PASSCODE HAS BEEN ACCEPTED	NEW SETPOINT HAS BEEN STORED
NO ALARMS ACTIVE	NO TRIPS OR ALARMS TO RESET	OUT OF RANGE.! ENTER: #### TO ##### BY #	PASSCODE SECURITY NOT ENABLED, ENTER 0	PRESS [ENTER] TO ADD DEFAULT MESSAGE
PRESS [ENTER] TO REMOVE MESSAGE	RESET PERFORMED SUCCESSFULLY	ROUNDED SETPOINT HAS BEEN STORED	SETPOINT ACCESS IS NOW PERMITTED	SETPOINT ACCESS IS NOW RESTRICTED
TACHOMETER MUST USE INPUT 4, 5, 6, OR 7	THAT DIGITAL INPUT IS ALREADY IN USE	THAT INPUT ALREADY USED FOR TACHOMETER	THIS FEATURE NOT PROGRAMMED	THIS PARAMETER IS ALREADY ASSIGNED
TIME ENTRY OUT OF RANGE	TIME ENTRY WAS	TOP OF LIST	TOP OF PAGE	

- **NEW SETPOINT HAS BEEN STORED:** This message appear each time a setpoint has been altered and stored as shown on the display.
- ROUNDED SETPOINT HAS BEEN STORED: Since the 489 has a numeric keypad, an
 entered setpoint value may fall between valid setpoint values. The 489 detects this
 condition and store a value rounded to the nearest valid setpoint value. To find the
 valid range and step for a given setpoint, press the HELP key while the setpoint is
 being displayed.
- OUT OF RANGE! ENTER: #### TO ##### BY #: If a setpoint value outside the acceptable range of values is entered, the 489 displays this message and substitutes proper values for that setpoint. An appropriate value may then be entered.

- ACCESS DENIED, SHORT ACCESS SWITCH: The Access Switch must be shorted to store
 any setpoint values. If this message appears and it is necessary to change a setpoint,
 short the Access terminals C1 and C2.
- ACCESS DENIED, ENTER PASSCODE: The 489 has a passcode security feature. If this
 feature is enabled, not only must the Access Switch terminals be shorted, but a valid
 passcode must also be entered. If the correct passcode has been lost or forgotten,
 contact the factory with the encrypted access code. All passcode features may be
 found in the S1 489 SETUP ➤ PASSCODE setpoints menu.
- INVALID PASSCODE ENTERED: This flash message appears if an invalid passcode is entered for the passcode security feature.
- NEW PASSCODE HAS BEEN ACCEPTED: This message will appear as an acknowledge
 that the new passcode has been accepted when changing the passcode for the
 passcode security feature.
- PASSCODE SECURITY NOT ENABLED, ENTER 0: The passcode security feature is
 disabled whenever the passcode is zero (factory default). Any attempts to enter a
 passcode when the feature is disabled results in this flash message, prompting the
 user to enter "0" as the passcode. When this has been done, the feature may be
 enabled by entering a non-zero passcode.
- ENTER A NEW PASSCODE FOR ACCESS: The passcode security feature is disabled if
 the passcode is zero. If the CHANGE PASSCODE SETPOINT is entered as yes, this flash
 message appears prompting the user to enter a non-zero passcode and enable the
 passcode security feature.
- **SETPOINT ACCESS IS NOW PERMITTED:** Any time the passcode security feature is enabled and a valid passcode is entered, this flash message appears to notify that setpoints may now be altered and stored.
- SETPOINT ACCESS IS NOW RESTRICTED: If the passcode security feature is enabled and a valid passcode entered, this message appears when the S1 489 SETUP ▷

 PASSCODE ▷ ▼ SETPOINT ACCESS setpoint is altered to "Restricted". This message also appears any time that setpoint access is permitted and the access jumper is removed.
- DATE ENTRY WAS NOT COMPLETE: Since the DATE setpoint has a special format
 (entered as MM/DD/YYYY), this message appears and the new value will not be stored
 if the ENTER key is pressed before all of the information has been entered. Another
 attempt will have to be made with the complete information.
- **DATE ENTRY WAS OUT OF RANGE:** Appears if an invalid entry is made for the **DATE** (for example, 15 entered for the month).
- **TIME ENTRY WAS NOT COMPLETE:** Since the **TIME** setpoint has a special format (entered as HH/MM/SS.s), this message appears and the new value will not be stored if the ENTER key is pressed before *all* of the information has been entered. Another attempt will have to be made with the complete information.
- **TIME ENTRY WAS OUT OF RANGE:** Appears if an invalid entry is made for the **TIME** (for example, 35 entered for the hour).
- **NO TRIPS OR ALARMS TO RESET:** Appears if the RESET key is pressed when there are no trips or alarms present.
- **RESET PERFORMED SUCCESSFULLY:** If all trip and alarm features that are active can be cleared (that is, the conditions that caused these trips and/or alarms are no longer

- present), then this message appears when a reset is performed, indicating that all trips and alarms have been cleared.
- ALL POSSIBLE RESETS HAVE BEEN PERFORMED: If only some of the trip and alarm
 features that are active can be cleared (that is, the conditions that caused some of
 these trips and/or alarms are still present), then this message appears when a reset is
 performed, indicating that only trips and alarms that could be reset have been reset.
 - ARE YOU SURE? PRESS [ENTER] TO VERIFY: If the RESET key is pressed and resetting of any trip or alarm feature is possible, this message appears to verify the operation. If RESET is pressed again while this message is displayed, the reset will be performed.
- PRESS [ENTER] TO ADD DEFAULT MESSAGE: Appears if the decimal [.] key, immediately followed by the ENTER key, is entered anywhere in the actual value message structure. This message prompts the user to press ENTER to add a new default message. To add a new default message, ENTER must be pressed while this message is being displayed.
- **DEFAULT MESSAGE HAS BEEN ADDED:** Appears anytime a new default message is added to the default message list.
- **DEFAULT MESSAGE LIST IS FULL:** Appears if an attempt is made to add a new default message to the default message list when 20 messages are already assigned. To add a new message, one of the existing messages must be removed.
- PRESS [ENTER] TO REMOVE MESSAGE: Appears if the decimal [.] key, immediately
 followed by the ENTER key, is entered in the S1 489 SETUP ▷▽ DEFAULT MESSAGES
 setpoint page. This message prompts the user to press ENTER to remove a default
 message. To remove the default message, ENTER must be pressed while this message
 is being displayed.
- DEFAULT MESSAGE HAS BEEN REMOVED: Appears anytime a default message is removed from the default message list.
- **DEFAULT MESSAGES** 6 of 20 ARE ASSIGNED: Appears anytime the S1 489 SETUP ▷▼ **DEFAULT MESSAGES** setpoint page is entered, notifying the user of the number of default messages assigned.
- INVALID SERVICE CODE ENTERED: Appears if an invalid code is entered in the \$12 489

 TESTING ▷ ▼ FACTORY SERVICE setpoints page.
- **KEY PRESSED HERE IS INVALID:** Under certain situations, certain keys have no function (for example, any number key while viewing actual values). This message appears if a keypress has no current function.
- DATA CLEARED SUCCESSFULLY: Confirms that data is reset in the S1 489 SETUP ▷▼ CLEAR DATA setpoints page.
- [.] **KEY IS USED TO ADVANCE THE CURSOR:** Appears immediately to prompt the use of the [.] key for cursor control anytime a setpoint requiring text editing is viewed. If the setpoint is not altered for 1 minute, this message flashes again.
- TOP OF PAGE: This message will indicate when the top of a page has been reached.
- **BOTTOM OF PAGE:** This message will indicate when the bottom of a page has been reached.
- TOP OF LIST: This message will indicate when the top of subgroup has been reached.

- **END OF LIST:** This message will indicate when the bottom of a subgroup has been reached.
- **NO ALARMS ACTIVE:** If an attempt is made to enter the Alarm Status message subgroup, but there are no active alarms, this message will appear.
- THIS FEATURE NOT PROGRAMMED: If an attempt is made to enter an actual value message subgroup, when the setpoints are not configured for that feature, this message will appear.
- THIS PARAMETER IS ALREADY ASSIGNED: A given analog output parameters can only
 be assigned to one output. If an attempt is made to assign a parameter to a second
 output, this message will appear.
- **THAT INPUT ALREADY USED FOR TACHOMETER:** If a digital input is assigned to the tachometer function, it cannot be used for any other digital input function. If an attempt is made to assign a digital input to a function when it is already assigned to tachometer, this message will appear.
- TACHOMETER MUST USE INPUT 4, 5, 6, or 7: Only digital inputs 4, 5, 6, or 7 may be used for the tachometer function. If an attempt is made to assign inputs 1,2,3, or 4 to the tachometer function, this message will appear.
- THAT DIGITAL INPUT IS ALREADY IN USE: If an attempt is made to assign a digital
 input to tachometer when it is already assigned to another function, this message will
 appear.
- To edit use VALUE UP or VALUE DOWN key: If a numeric key is pressed on a setpoint
 parameter that is not numeric, this message will prompt the user to use the value
 keys.
- **GROUP 1 SETPOINT HAS BEEN STORED:** This message appear each time a setpoint has been altered and stored to setpoint Group 1 as shown on the display.
- **GROUP 2 SETPOINT HAS BEEN STORED:** This message appear each time a setpoint has been altered and stored to setpoint Group 2 as shown on the display.





7.1 Test Setup

7.1.1 Description

The purpose of this testing description is to demonstrate the procedures necessary to perform a complete functional test of all the 489 hardware while also testing firmware/hardware interaction in the process. Since the 489 is packaged in a drawout case, a demo case (metal carry case in which the 489 may be mounted) may be useful for creating a portable test set with a wiring harness for all of the inputs and outputs. Testing of the relay during commissioning using a primary injection test set will ensure that CTs and wiring are correct and complete.

The 489 tests are listed below. For the following tests refer to Secondary Current Injection Testing on page 7–3:

- 1. Output Current Accuracy Test
- 2. Phase Voltage Input Accuracy Test
- 3. Ground, Neutral, and Differential Current Accuracy Test
- 4. Neutral Voltage (Fundamental) Accuracy Test
- 5. Negative Sequence Current Accuracy Test
- 6. RTD Accuracy Test
- 7. Digital Input and Trip Coil Supervision Accuracy Test
- 8. Analog Input and Outputs Test
- 9. Output Relay Test
- 10. Overload Curve Test
- 11. Power Measurement Test
- 12. Reactive Power Test

- 13. Voltage Phase Reversal Test
- 14. For the following tests refer to Secondary Injection Setup #2 on page 7–15:
- 15. GE Multilin (HGF) Ground Current Accuracy Test
- 16. Neutral Voltage (3rd Harmonic) Accuracy Test
- 17. Phase Differential Trip Test
- 18. For the following test refer to Secondary Injection Test Setup #3 on page 7-19:
- 19. Voltage Restrained Overcurrent Test





FIGURE 7–1: Secondary Current Injection Testing

7.2 Hardware Functional Tests

7.2.1 Output Current Accuracy

The specification for output and neutral end current input is $\pm 0.5\%$ of $2 \times CT$ when the injected current is less than $2 \times CT$. Perform the steps below to verify accuracy.

▶ Alter the following setpoint:

S2 SYSTEM SETUP ▷ CURRENT SENSING ▷ ♡ PHASE CT PRIMARY: "1000 A"

Measured values should be ± 10 A.

Inject the values shown in the table below and verify accuracy of the measured values.

View the measured values in the A2 METERING DATA ▷ ♥ CURRENT METERING menu.

Injected	Current	Expected	Measured Current									
1 A Unit	5 A Unit	Current	Phase A	Phase B	Phase C							
0.1 A	0.5 A	100 A										
0.2 A	1.0 A	200 A										
0.5 A	2.5 A	500 A										
1 A	5 A	1000 A										
1.5 A	7.5 A	1500 A		0	0							
2 A	10 A	2000 A		510016	2, 03,							

7.2.2 Phase Voltage Input Accuracy

The specification for phase voltage input accuracy is $\pm 0.5\%$ of full scale (200 V). Perform the steps below to verify accuracy.

Alter the following setpoints in the S2 SYSTEM SETUP ▷ ♥ VOLTAGE SENSING menu:

VT CONNECTION TYPE: "Wye"
VOLTAGE TRANSFORMER RATIO: "10.00:1"

Measured values should be ± 1.0 V.

- Apply the voltage values shown in the table and verify accuracy of the measured values.
- **View the measured values in the A2 METERING DATA** ▷ ▽ **VOLTAGE METERING menu**.

Applied Line-	Expected Voltage	Measured Voltage								
Neutral Voltage	Reading	A-N	B-N	C-N						
30 V	300 V									
50 V	500 V									
100 V	1000 V									
150 V	1500 V									

Ī	Applied Line-	Expected Voltage	Measured Voltage								
	Neutral Voltage Reading	A-N	B-N	C-N							
-	200 V	2000 V									

7.2.3 Ground (1 A) Neutral, and Differential Current Accuracy

The specification for neutral, differential and 1 A ground current input accuracy is $\pm 0.5\%$ of $2 \times CT$. Perform the steps below to verify accuracy.

▶ In the S2 SYSTEM SETUP ▷ CURRENT SENSING menu, set:

GROUND CT: "1A Secondary" GROUND CT RATIO: "1000:1" PHASE CT PRIMARY: "1000 A"

 \triangleright In the S5 CURRENT ELEMENTS $\triangleright \nabla$ PHASE DIFFERENTIAL menu, set:

PHASE DIFFERENTIAL TRIP: "Unlatched" DIFFERENTIAL TRIP MIN. PICKUP: "0.1 x CT"

The last two setpoints are needed to view the neutral and the differential current. The trip element will operate when differential current exceeds 100 A.

Measured values should be ± 10 A.

- \triangleright Inject (I_A only) the values shown in the table below into one phase only and verify accuracy of the measured values.
- View the measured values in the A2 METERING DATA ➤ CURRENT METERING menu or press the NEXT key to view the current values when differential trip element is active.

Table 7–1: Neutral and Ground Current Test Results

Injected Current	Expected Current	Measured Ground Current		Measured Neutral Current								
1 A Unit	Current	Ground Current	Phase A	Phase B	Phase C							
0.1 A	100 A											
0.2 A	200 A											
0.5 A	500 A											
1 A	1000 A											

Table 7-2: Differential Current Test Results

Injected Current	Expected Cur	rrent Reading	Measured Differential Current								
Current	Differential Phase A	Differential Phase B,C	Phase A	Phase B	Phase C						
0.1 A	200 A	100 A									
0.2 A	400 A	200 A									
0.5 A	1000 A	500 A									
1 A	2000 A	1000 A									

7.2.4 Neutral Voltage (Fundamental) Accuracy

The specification for neutral voltage (fundamental) accuracy is $\pm 0.5\%$ of full scale (100 V). Perform the steps below to verify accuracy.

▶ In the S2 SYSTEM SETUP ▷ VOLTAGE SENSING menu, set:

NEUTRAL VOLTAGE TRANSFORMER: "Yes"
NEUTRAL V.T. RATIO: "10.00:1"

▶ In the S2 SYSTEM SETUP ▷ ♥ GEN. PARAMETERS menu, set:

GENERATOR NOMINAL FREQUENCY: "60 Hz"

Measured values should be ± 5.0 V.

Apply the voltage values shown in the table and verify accuracy of the measured values.

> View the measured values in the A2 METERING DATA ▷ ♥ VOLTAGE METERING menu.

Applied Neutral Voltage at 60 Hz	Expected Neutral Voltage	Measured Neutral Voltage
10 V	100 V	
30 V	300 V	
50 V	500 V	

7.2.5 Negative Sequence Current Accuracy

The 489 measures negative sequence current as a percent of Full Load Amperes (FLA). sample calculation of negative sequence current is shown below. Given the following generator parameters:

Rated MVA (P_A) = 1.04 Voltage Phase to Phase (V_{DD}): 600 V

We have:

$$FLA = \frac{P_A}{\sqrt{3} \times V_{DD}} = \frac{1.04 \times 10^6}{\sqrt{3} \times 600} = 1000 \text{ A}$$
 (EQ 7.1)

With the following output currents:

$$I_a = 780 \angle 0^{\circ}$$
, $I_b = 1000 \angle 113^{\circ} \log$, $I_c = 1000 \angle 247^{\circ} \log$ (EQ 7.2)

The negative-sequence current Ins is calculated as:

$$I_{ns} = \frac{1}{3}(I_a + a^2I_b + aI_c) \quad \text{where } a = 1 \angle 120^\circ = -0.5 + j0.866$$

$$= \frac{1}{3}(780 \angle 0^\circ + (1 \angle 120^\circ)^2 (1000 \angle -113^\circ) + (1 \angle 120^\circ) (1000 \angle 113^\circ))$$

$$= \frac{1}{3}(780 \angle 0^\circ + 1000 \angle 127^\circ + 1000 \angle 233^\circ)$$

$$= \frac{1}{3}(780 - 601.8 + j798.6 - 601.8 - j798.6)$$

$$= -141.2$$

$$\Rightarrow \%I_{ns} = \frac{I_{ns}}{\text{FLA}} \times 100 = 14\%$$
Therefore, the negative sequence current is 14% of FLA. The specification for negative-sequence current accuracy is per output current inputs. Perform the steps below to verify accuracy.

▶ In the S2 SYSTEM SETUP ▷ ♥ GEN. PARAMETERS menu, set:

GENERATOR RATED MVA: "1.04" VOLTAGE PHASE-PHASE: "600"

Note that setting **VOLTAGE PHASE-PHASE** to "600" is equivalent to setting FLA = 1000 A. This is for testing purposes only!

► In the S2 SYSTEM SETUP ► CURRENT SENSING menu, set:

PHASE CT PRIMARY: "1000 A"

- ▶ Inject the values shown in the table below and verify accuracy of the measured values.
- View the measured values in the A2 METERING DATA ➤ CURRENT METERING menu.

Injected	Current	Expected Negative	Measured Negative
1 A Unit	5 A Unit	Sequence Current	Sequence Current
Ia = 0.78 A ∠0° Ib = 1 A ∠113° lag Ic = 1 A ∠247° lag	Ia = 3.9 A ∠0° Ib = 5 A ∠113° Iag Ic = 5 A ∠247° Iag	14% FLA	
Ia = 1.56 A ∠0° Ib = 2 A ∠113° Iag Ic = 2 A ∠247° Iag	la = 7.8 A ∠0° lb = 10 A ∠113° lag lc = 10 A ∠247° lag	28% FLA	
$ a = 0.39 \text{ A} \angle 0^{\circ}$ $ b = 0.5 \text{ A} \angle 113^{\circ} \text{ lag}$ $ c = 0.5 \text{ A} \angle 247^{\circ} \text{ lag}$	$ a = 1.95 \text{ A} \angle 0^{\circ}$ $ b = 2.5 \text{ A} \angle 113^{\circ} ag $ $ c = 2.5 \text{ A} \angle 247^{\circ} ag $	7% FLA	

7.2.6 RTD Accuracy

The specification for RTD input accuracy is $\pm 2^{\circ}$ for Platinum/Nickel and $\pm 5^{\circ}$ for Copper. Perform the steps below.

► In the S8 RTD TEMPERATURE MENU, set:

RTD TYPE ▷ STATOR RTD TYPE: "100 Ohm Platinum" (select desired type)
RTD #1 ▷ RTD #1 APPLICATION: "Stator" (repeat for RTDs 2 to 12)

Measured values should be $\pm 2^{\circ}\text{C}$ / $\pm 4^{\circ}\text{F}$ for platinum/nickel and $\pm 5^{\circ}\text{C}$ / $\pm 9^{\circ}\text{F}$ for copper.

- Alter the resistance applied to the RTD inputs as shown below to simulate RTDs and verify accuracy.
- \triangleright View the measured values in A2 METERING DATA $\triangleright \triangledown$ TEMPERATURE.

Applied Resistance	Expected RTD Temperature Reading			Measured RTD Temperature Select One:°C°F										
100 Ω Platinum	$^{\circ}\mathrm{C}$	°F	1	2	3	4	5	6	7_	-8	9_	10	11	12
84.27 Ω	-40°C	-40°F												
100.00 Ω	0°C	32°F										\		
119.39 Ω	50°C	122°F								_				
138.50Ω	100°C	21 2° F												
157.32 Ω	150°C	302°F										/		
175.84 Ω	200°C	392°F												
194.08 Ω	250°C	482°F												

Applied Resistance	Expected RTD Temperature Reading			Measured RTD Temperature Select One:°C°F										
120 Ω Nickel	°C	°F	1	2	3	4	5	6	7	8	9	10	11	12
92.76 Ω	-40°C	-40°F												
120.00 Ω	0°C	32°F												
157.74 Ω	50°C	122°F												
200.64 Ω	100°C	212°F												
248.95 Ω	150°C	302°F							(3	7.3	2	m	2
303.46 Ω	200°C	392°F							0	TO.	7	201		200
366.53 Ω	250°C	482°F												

Applied Resistance	Expected RTD Temperature Reading			Measured RTD Temperature Select One:°C°F										
100 Ω Nickel	°C	°F	1	2	3	4	5	6	7	8	9	10	11	12
77.30 Ω	-40°C	-40°F												
100.00 Ω	0°C	32°F												
131.45 Ω	50°C	122°F												
167.20 Ω	100°C	212°F												
207.45 Ω	150°C	302°F												
252.88 Ω	200°C	392°F												
305.44 Ω	250°C	482°F												

Applied Resistance	Expected RTD Temperature Reading			Measured RTD Tempeature Select One:°C°F										
10 Ω Copper	°C	°F	1	2	3	4	5	6	7	8	9	10	11	12
7.49 Ω	-40°C	-40°F												
9.04 Ω	0°C	32°F												
10.97 Ω	50°C	122°F												
12.90 Ω	100°C	212°F												
14.83 Ω	150°C	302°F												
16.78 Ω	200°C	392°F												

Applied Resistance 10 Ω Copper	Expected RTD Temperature Reading			Measured RTD Tempeature Select One:°F										
10 Ω Copper	°C	°F	1	2	3	4	5	6	7	8	9	10	11	12
18.73 Ω	250°C	482°F												

7.2.7 Digital Inputs and Trip Coil Supervision

The digital inputs and trip coil supervision can be verified easily with a simple switch or pushbutton. Verify the Switch +24 V DC with a voltmeter. Perform the steps below to verify functionality of the digital inputs.

- Den switches of all of the digital inputs and the trip coil supervision circuit.
- View the status of the digital inputs and trip coil supervision in the A1 STATUS > V DIGITAL INPUTS menu.
- Close switches of all of the digital inputs and the trip coil supervision circuit.
- View the status of the digital inputs and trip coil supervision in the A1 STATUS ▷ ♥ DIGITAL INPUTS menu.

Input	Expected Status (Switch Open)	4 Pass 8 Fail	Expected Status (Switch Closed)	4 Pass 8 Fail
Access	Open		Shorted	
Breaker Status	Open		Shorted	
Assignable Input 1	Open		Shorted	SOUS
Assignable Input 2	Open		Shorted	
Assignable Input 3	Open		Shorted	
Assignable Input 4	Open		Shorted	
Assignable Input 5	Open		Shorted	
Assignable Input 6	Open		Shorted	
Assignable Input 7	Open		Shorted	
Trip Coil Supervision	No Coil		Coil	

7.2.8 Analog Inputs and Outputs

The specification for analog input and analog output accuracy is $\pm 1\%$ of full scale. Perform the steps below to verify accuracy. Verify the Analog Input +24 V DC with a voltmeter.

4 to 20 mA Inputs:

ightharpoonup In the S11 ANALOG I/O ho
ightharpoonup ANALOG INPUT 1 menu, set:

ANALOG INPUT 1: "4-20 mA"

ANALOG INPUT 1 MINIMUM: "0"

ANALOG INPUT 1 MAXIMUM: "1000" (repeat all for Analog Inputs 2 to 4)

Analog output values should be ± 0.2 mA on the ammeter. Measured analog input values should be ± 10 units.

► Force the analog outputs using the following setpoints from the S12 TESTING ► TEST ANALOG OUTPUT menu:

FORCE ANALOG OUTPUTS FUNCTION: "Enabled"
ANALOG OUTPUT 1 FORCED VALUE: "0%" (enter %, repeat for Outputs 2 to 4)

- Verify the ammeter readings and the measured analog input readings. For the purposes of testing, the analog input is fed in from the analog output (see Secondary Current Injection Testing on page 7–3).
- View the measured values in the A2 METERING DATA ▷ ANALOG INPUTS menu.

Analog Output	Expected Ammeter			Amme ng (ma)		Expected Analog Input	Meas	sured A Readin	Analog Input ng (units)	
Force Value	Reading	<u> </u>	2	3	4	Reading	1	2	3	4
0%	4 mA					0 units				
25%	8 mA					250 units				
50%	12 mA					500 units				
75%	16 mA					750 units				
100%	20 mA					1000 units				

0 to 1 mA Analog Inputs:

 \triangleright In the S11 ANALOG I/O $\triangleright \nabla$ ANALOG INPUT 1 menu, set:

ANALOG INPUT 1: "0-1 mA"

ANALOG INPUT 1 MINIMUM: "0"

ANALOG INPUT 1 MAXIMUM: "1000" (repeat for Analog Inputs

Analog output values should be ± 0.01 mA on the ammeter. Measured analog input values should be ± 10 units.

► Force the analog outputs using the following setpoints in the S12 TESTING ► TEST ANALOG OUTPUT menu:

FORCE ANALOG OUTPUTS FUNCTION: "Enabled" **ANALOG OUTPUT 1 FORCED VALUE:** "0%" (enter %, repeat for Outputs 2 to 4)

- ▶ Verify the ammeter readings as well as the measured analog input readings.
- \triangleright View the measured values in the A2 METERING DATA $\triangleright \nabla$ ANALOG INPUTS menu.

Analog Output Force	Expected Ammeter	Measured Ammeter Reading (mA)			Expected Analog Input	Measured Analog Input Reading (units)				
Value	Reading	1	2	3	4	Reading	1	2	3	4
0%	0 mA					0 units				
25%	0.25 mA					250 units				
50%	0.50 mA					500 units				
75%	0.75 mA					750 units				
100%	1.00 mA					1000 units				

7.2.9 Output Relays

To verify the functionality of the output relays, perform the following steps: Using the setpoint:

S12 TESTING $\triangleright \triangledown$ TEST OUTPUT RELAYS $\triangleright \triangledown$ FORCE OPERATION OF RELAYS: "1 Trip"

> Select and store values as per the table below, verifying operation

Force		L	Expe	cted	Mea	sure	emen	ıt (4	for	shor	t)				Actu	al N	1eas	urei	nen	(4 f	or s	hort)	
Operation Setpoint				2	3	3	4	1		5		Ó	1	1	(:	2		3		1	5	5	6	5
	no	nc	no	nc	no	nc	no	nc	no	nc	no	nc	no	nc	no	ne_	no	nc	no	nc	no	nc	no	nc
1 Trip	4			4		4		4		4	4)										
2 Auxiliary		4	4		/	4		4		4	4													
3 Auxiliary		4/		4	4			4		4	4				1									
4 Auxiliary		4		4		4	4		L	4	4													
5 Alarm		4		4		4		4	4		4													
6 Service		4		4		4		4		4		4												
All Relays	4		4		4		4		4			4												
No Relays		4		4		4		4		4	4													



The 6 Service relay is failsafe or energized normally. Operating output relay 6 causes it to de-energize.



7.3 Additional Functional Tests

7.3.1 Overload Curve Accuracy

The specification for overload curve timing accuracy is ± 100 ms or $\pm 2\%$ of time to trip. Pickup accuracy is as per the current inputs ($\pm 0.5\%$ of 2 × CT when the injected current is less than 2 × CT and $\pm 1\%$ of 20 × CT when the injected current is equal to or greater than 2 × CT). Perform the steps below to verify accuracy.

▶ In the S2 SYSTEM SETUP ▷ ♥ GEN. PARAMETERS menu, set:

GENERATOR RATED MVA: "1.04"

GENERATOR VOLTAGE PHASE-PHASE: "600"

Note that setting **GENERATOR VOLTAGE PHASE-PHASE** to "600" is equivalent to setting FLA = 1000 A. For testing purposes ONLY!

► In the S2 SYSTEM SETUP ► CURRENT SENSING menu, set:

PHASE CT PRIMARY: "1000"

▶ In the S9 THERMAL MODEL ▶ MODEL SETUP menu, set:

SELECT CURVE STYLE: "Standard"
OVERLOAD PICKUP LEVEL: "1.10 x FLA"
UNBALANCE BIAS K FACTOR: "0"
HOT/COLD SAFE STALL RATIO: "1.00"
ENABLE RTD BIASING: "No"

STANDARD OVERLOAD CURVE NUMBER: "4"

ENABLE THERMAL MODEL: "Yes"

► In the S9 THERMAL MODEL ► THERMAL ELEMENTS menu. set:

THERMAL MODEL TRIP: "Latched" or "Unlatched"

Any trip must be reset prior to each test. Short the emergency restart terminals momentarily immediately prior to each overload curve test to ensure that the thermal capacity used is zero. Failure to do so will result in shorter trip times. Inject the current of the proper amplitude to obtain the values as shown and verify the trip times. Motor load may be viewed in the A2 METERING DATA \triangleright CURRENT METERING menu.

The thermal capacity used and estimated time to trip may be viewed in the A1 STATUS $\triangleright \nabla$ GENERATOR STATUS menu.

Average Phase Current Displayed	Pickup Level	Expected Time to Trip	Tolerance Range	Measured Time to Trip (sec.)
1050 A	1.05 × FLA	never	n/a	
1200 A	1.20 × FLA	795.44 s	779.53 to 811.35 s	
1750 A	1.75 × FLA	169.66 s	166.27 to 173.05 s	
3000 A	3.00 × FLA	43.73 s	42.86 to 44.60 s	
6000 A	6.00 × FLA	9.99 s	9.79 to 10.19 s	
10000 A	10.00 × FLA	5.55 s	5.44 to 5.66 s	



FLA =
$$\frac{\text{Generator Rated MVA}}{\sqrt{3} \times \text{Generator Phase-to-Phase Voltage}}$$
 (EQ 7.4)

7.3.2 Power Measurement Test

The specification for reactive and apparent power is \pm 1% of $\sqrt{3}$ × 2 × CT × VT_{ratio} × VT_{full-scale} at I_{ava} < 2 × CT. Perform the steps below to verify accuracy.



PHASE CT PRIMARY: "1000"

 \triangleright In the S2 SYSTEM SETUP $\triangleright \nabla$ VOLTAGE SENSING menu, set:

VT CONNECTION TYPE: "Wye"

VOLTAGE TRANSFORMER RATIO: "10.00:1"

▶ Inject current and apply voltage as per the table below.

∀ Verify accuracy of the measured values.

View the measured values in the A2 METERING DATA ▷ ▼ POWER METERING menu:

Injected Current (Ia is the ref]	Power Quantit	y	Power	Factor	
1 A UNIT	5 A UNIT	Expected	Tolerance	Measured	Expected	Measured
la = 1 A∠0° lb = 1 A∠120° lag lc = 1 A∠240° lag Va = 120 V∠342° lag Vb = 120 V∠102° lag Vc = 120 V∠222° lag	la = 5 A∠0° lb = 5 A∠120° lag lc = 5 A∠240° lag la = 120 V∠342° lag Vb = 120 V∠102° lag Vc = 120 V∠222° lag	+3424 kW	3355 to 3493 kW		0.95 lag	
$ a = 1 \text{ A} \angle 0^{\circ}$ $ b = 1 \text{ A} \angle 120^{\circ} \text{ag}$ $ c = 1 \text{ A} \angle 240^{\circ} \text{ag}$ $ c = 120 \text{ V} \angle 288^{\circ} \text{ag}$ $ c = 120 \text{ V} \angle 48^{\circ} \text{ag}$ $ c = 120 \text{ V} \angle 168^{\circ} \text{ag}$	la = 5 A∠0° lb = 5 A∠120° lag lc = 5 A∠240° lag Va = 120 V∠288° lag Vb = 120 V∠48° lag Vc = 120 V∠168° lag	+3424 kvar	3355 to 3493 kvar	Sto	0.31 lag)S.US

7.3.3 Reactive Power Accuracy

The specification for reactive power is $\pm 1\%$ of $\sqrt{3}\times2\times$ CT \times VT_{ratio} \times VT_{full scale} at I_{ava} < $2\times$ CT. Perform the steps below to verify accuracy and trip element.

▶ In the S2 SYSTEM SETUP ▶ CURRENT SENSING menu, set:

PHASE CT PRIMARY: "5000"

▶ In the S2 SYSTEM SETUP ▷ VOLTAGE SENSING menu, set:

VT CONNECTION TYPE: "Wye"
VOLTAGE TRANSFORMER RATIO: "100:1"

, oblitor italian or other resident in the second

ight
angle In the S2 System Setup htarrow
ightrarrow Gen. Parameters menu, set

GENERATOR RATED MVA: "100"

GENERATOR RATED POWER FACTOR: "0.85"

GENERATOR VOLTAGE PHASE-PHASE: "12000"

The rated reactive power is $100\sin(\cos^{-1}(0.85)) = \pm 52.7$ Mvar.

▶ Alter the following reactive power setpoints in the S7 POWER ELEMENTS
▶ REACTIVE POWER menu:

REACTIVE POWER ALARM: "Unlatched"
ASSIGN ALARM RELAYS(2-5): "---5"
POSTIVE MVAR ALARM LEVEL: "0.6 x Rated"
NEGATIVE MVAR ALARM LEVEL: "0.6 x Rated"
REACTIVE POWER ALARM DELAY: "5 s"
REACTIVE POWER ALARM EVENT: "On"
REACTIVE POWER TRIP: "Unlatched"
ASSIGN TRIP RELAYS(1-4): "1---"
POSTIVE MVAR TRIP LEVEL: "0.75 x Rated"
NEGATIVE MVAR TRIP LEVEL: "0.75 x Rated"

REACTIVE POWER TRIP DELAY: "10 s"

> Inject current and apply voltage as per the table below.

Verify the alarm/trip elements and the accuracy of the measured values.

View the measured values in the A2 METERING DATA ▷ POWER METERING page.

View the Event Records in the A5 EVENT RECORD menu.

Current/Voltage	Mvar				Alarm			Trip	
	Expected	Tolerance	Measured	Expected	Observed	Delay	Expected	Observed	Delay
Vab=120V∠0° Vbc=120V∠120°lag Vca=120V∠240°lag lan=5 A∠10°lag lbn=5 A∠130°lag lcn=5 A∠250°lag	18	13 to 23		4		N/A	8		N/A
Vab=120V∠0° Vbc=120V∠120°lag Vca=120V∠240°lag lan=5 A∠340°lag lbn=5 A∠100°lag lcn=5 A∠220°lag	-35	-40 to -30		4		(300i	e.ip	SJ N/A
Vab=120V∠0° Vbc=120V∠120°lag Vca=120V∠240°lag lan=5 A∠330°lag lbn=5 A∠90°lag lcn=5 A∠210°lag	-52	-57 to -47		4			4		
Vab=120V∠0° Vbc=120V∠120°lag Vca=120V∠240°lag lan=5 A∠30°lag lbn=5 A∠150°lag lcn=5 A∠270°lag	52	47 to 57		4			4		

^{4:} Activated, **8**: Not Activated

7.3.4 Voltage Phase Reversal Accuracy

The relay can detect voltage phase rotation and protect against phase reversal. To test the phase reversal element, perform the following steps:

 \triangleright In the S2 SYSTEM SETUP $\triangleright \nabla$ VOLTAGE SENSING menu, set:

VT CONNECTION TYPE: "Wye"

 \triangleright In the S2 SYSTEM SETUP $\triangleright \triangledown$ GEN. PARAMETERS menu, set:

GENERATOR PHASE SEQUENCE: "ABC"

▶ In the S3 DIGITAL INPUTS ▶ BREAKER STATUS menu, set:

BREAKER STATUS: "Breaker Auxiliary a"

▶ In the S6 VOLTAGE ELEMENTS ▷ ♥ PHASE REVERSAL menu, set:

PHASE REVERSAL TRIP: "Unlatched" ASSIGN TRIP RELAYS: "1---"

Apply voltages as per the table below. Verify the operation on voltage phase reversal

/ \		
Applied Voltage	Expected Result	Observed Result
Va = 120 V∠0° Vb = 120 V∠120° lag Vc = 120 V∠240° lag	No Trip	
$Va = 120 \text{ V} \angle 0^{\circ}$ $Vb = 120 \text{ V} \angle 240^{\circ} \text{ lag}$ $Vc = 120 \text{ V} \angle 120^{\circ} \text{ lag}$	Phase Reversal Trip	

7.3.5 Injection Test Setup #2

Set up the 489 device as follows for the GE Multilin HGF Ground Accuracy Test, Neutral Voltage (3rd Harmonic) Accuracy Test, and the Phase Differential Trip Test.

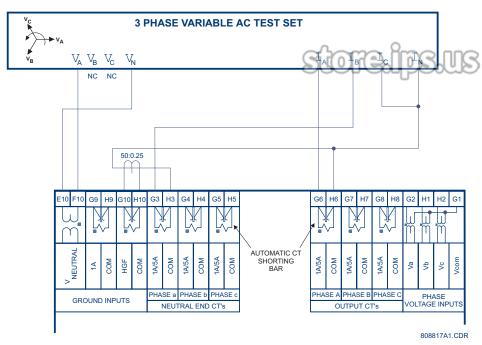


FIGURE 7-2: Secondary Injection Setup #2

7.3.6 GE Multilin 50:0.025 Ground Accuracy

The specification for GE Multilin HGF 50:0.025 ground current input accuracy is $\pm 0.5\%$ of $2 \times CT$ rated primary (25 A). Perform the steps below to verify accuracy.

► In the S2 SYSTEM SETUP ► CURRENT SENSING menu, set:

GROUND CT: "50:0.025 CT"

Measured values should be ± 0.25 A.

- □ Inject the values shown in the table below either as primary values into a
 □ GE Multilin 50:0.025 Core Balance CT or as secondary values that
 □ simulate the core balance CT.
- Verify accuracy of the measured values in the A2 METERING DATA ▷
 CURRENT METERING menu.

Injected	Current	Current	Reading
Primary 50:0.025 CT	Secondary	Expected	Measured
0.25 A	0.125 mA	0.25 A	1
1 A	0.5 mA	1.00 A	
5 A	2.5 mA	5.00 A	
10 A	5 mA	10.00 A	

7.3.7 Neutral Voltage (3rd Harmonic) Accuracy

The 489 specification for neutral voltage (3rd harmonic) accuracy is $\pm 0.5\%$ of full scale (100 V). Perform the steps below to verify accuracy.

ight
angle In the S2 SYSTEM SETUP hd riangle riangle riangle voltage sensing menu, set

NEUTRAL VOLTAGE TRANSFORMER: "Yes" NEUTRAL V.T. RATIO: "10.00:1"

ightrightarrow In the S2 SYSTEM SETUP hd riangledown GEN. PARAMETERS menu, set

GENERATOR NOMINAL FREQUENCY: "60 Hz"

Measured values should be ± 5.0 V.

- Apply the voltage values shown in the table and verify accuracy of the measured values.
- **View the measured values in the A2 METERING DATA ▷ VOLTAGE METERING menu.**

Applied Neutral Voltage at 180 Hz	Expected Neutral Voltage	Measured Neutral Voltage
10 V	100 V	
30 V	300 V	
50 V	500 V	

7.3.8 Phase Differential Trip Accuracy



These tests will require a dual channel current source. The unit must be capable of injecting prefault currents and fault currents of a different value. Application of excessive currents (greater than $3 \times CT$) for extended periods will cause damage to the relay.

Minimum Pickup Check

- \triangleright Connect the relay test set to inject Channel X current (I_x) into the G3 terminal and out of H3 terminal (Phase A). Increase I_x until the differential element picks up.
- > Switch off the current.

The theoretical pickup can be computed as follows:

 $I_{XPU} = Pickup setting \times CT$ (EQ 7.5)

Single Infeed Fault

 \triangleright Set the I_x prefault current equal to 0.

Set the fault current equal to CT.

- ▶ Apply the fault.
- > Switch off the current.
- \triangleright Set the I_x prefault current equal to 0.
- \triangleright Set the fault current equal to 5 × CT.
- ▶ Apply the fault.
- > Switch off the current.
- > Record the operating time.



Slope 1 Check

- Connect the relay test set to inject Channel Y current (I_Y) into the G6 terminal and out of H6 terminal.
 The angle between I_X and I_Y will be 180°.
- \triangleright Set pre-fault current, I_x and I_y equal to zero.
- \triangleright Set fault current, I_Y equal to $1\frac{1}{2}$ CT.

At this value the relay should operate according to the following formula:

$$I_{XOP1} = \frac{2 - \text{Slope 1 setting}}{2 + \text{Slope 1 setting}} \times \frac{3 \times \text{CT}}{2}$$
 (EQ 7.6)

- \triangleright Set fault current, I_x equal to $0.95 \times I_{XOP1}$.
- Apply the fault.

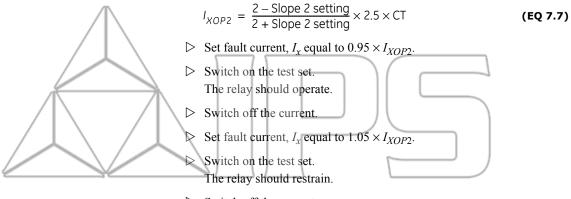
 The relay should operate.
- > Switch off the current.
- \triangleright Set fault current, I_x equal to $1.05 \times I_{XOP1}$.
- Apply the fault.

 The relay should restrain.
- > Switch off the current.

Slope 2 Check

 \triangleright Set fault current, I_Y equal to $2.5 \times CT$.

At this value the relay should operate according to the following formula.



> Switch off the current.

Directional Check

- \triangleright Set pre-fault current, I_x and I_Y equal to $3.5 \times CT$. At this value the conditions for CT saturation detection are set and the relay will enable the directional check.
- \triangleright Set fault current, I_x equal to $0.95 \times I_{XOP2}$.
- Switch on the test set.The relay should restrain.
- > Switch off the current.
- **▷** Repeat steps from Minimum Pickup Check onward for phases B and C.

Test Results

Test	Pha	se A	Pha	se B	Phase C		
	Calculated	Measured	Calculated	Measured	Calculated	Measured	
Minimum Pickup							

Test	Pha	se A	Pha	se B	Phase C		
	CT	5×CT	CT	5×CT	CT	5×CT	
Single Infeed Fault							

	Test		Phase A		Phase B		Phase C	
			operate	restrain	operate	restrain	operate	restrain
	Slope 1	I _×						
		l _y						
		Operation (OK/not OK)						
	Slope 2	×						
/ []		ly						
		Operation (OK/not OK)						
	Directional Check	I _×	N/A		N/A		N/A	
		ly	N/A		N/A		N/A	
		Operation (OK/not OK)	N/A		N/A		N/A	

7.3.9 Injection Test Setup #3

Setup the 489 device as follows for the Voltage Restrained Overcurrent test.

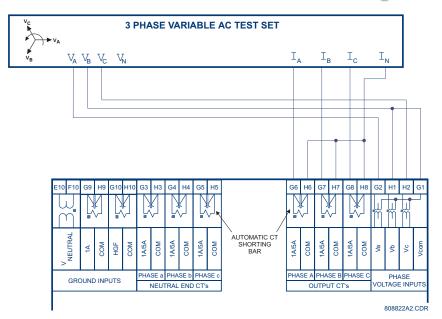


FIGURE 7–3: Secondary Injection Test Setup #3

7.3.10 Voltage Restrained Overcurrent Accuracy

Setup the relay as shown in FIGURE 7-3: Secondary Injection Test Setup #3 on page 7-19.

 \triangleright In the S2 SYSTEM SETUP $\triangleright \nabla$ GEN. PARAMETERS menu, set:

> Ir

GENERATOR RATED MVA: "100 MVA"
GENERATOR VOLTAGE PHASE-PHASE: "12000"

 \triangleright In the S2 SYSTEM SETUP $\triangleright \nabla$ VOLTAGE SENSING menu, set:

VT CONNECTION TYPE: "Open Delta"
VOLTAGE TRANSFORMER RATIO: "100:1"

▶ In the S5 CURRENT ELEMENTS ▶ OVERCURRENT ALARM menu, set:

OVERCURRENT ALARM: "Unlatched"
O/C ALARM LEVEL: "1.10 x FLA"
OVERCURRENT ALARM DELAY: "2 s"
O/C ALARM EVENTS: "On"

▶ In the S5 CURRENT ELEMENTS ▷ ♥ PHASE OVERCURRENT menu, set:

PHASE OVERCURRENT TRIP: "Latched"
ENABLE VOLTAGE RESTRAINT: "Yes"
PHASE O/C PICKUP: "1.5 x CT"
CURVE SHAPE: "ANSI Extremely Inv."
O/C CURVE MULTIPLIER: "2.00"
O/C CURVE RESET: "Instantaneous"

The trip time for the extremely inverse ANSI curve is given as:

Time to Trip =
$$M \times \left(A + \frac{B}{\frac{I}{\langle K \rangle \times I_p} - C} + \frac{D}{\left(\frac{I}{\langle K \rangle \times I_p} - C \right)^2} + \frac{E}{\left(\frac{I}{\langle K \rangle \times I_p} - C \right)^3} \right)$$
 (EQ 7.8)

where:M = O/C CURVE MULTIPLIER setpoint

I = input current

 $I_D = PHASE O/C PICKUP setpoint$

A, B, C, D, E = curve constants, where A = 0.0399, B = 0.2294, C = 0.5000, D = 3.0094, and E = 0.7222

K = voltage restrained multiplier < optional >

The voltage restrained multiplier is calculated as:

$$K = \frac{\text{phase-to-phase voltage}}{\text{rated phase-to-phase voltage}}$$
 (EQ 7.9)

and has a range of 0.1 to 0.9.

- Using *Secondary Injection Test Setup #3* on page 7–19, inject current and apply voltage as per the table below.
- ▶ Verify the alarm/trip elements and view the event records in the A5 EVENT RECORD menu.

Current/vol	Alarm			Trip		Trip Delay		
Current	Voltage	expected	observed	delay	expected	observed	expected	observed
lbn = 5 A∠120° lag	Vab = 120 V∠0° lag Vbc = 120 V∠120° lag Vca = 120 V∠240° lag	8		N/A	8		N/A	N/A
lbn = 6 A∠120° lag	Vab = 120 V∠0° Vbc = 120 V∠120° lag Vca = 120 V∠240° lag	4			8		N/A	N/A
Ibn = 10 A∠120° lag	Vab = 120 V∠0° Vbc = 120 V∠120° lag Vca = 120 V∠240° lag	4			4		11.8 s	
$lbn = 10 A \angle 120^{\circ} lag$	Vab = 100 V∠0° Vbc = 100 V∠120° lag Vca = 100 V∠240° lag	4			4		6.6 s	
$an = 10 A \angle 0^{\circ}$ $bn = 10 A \angle 120^{\circ}$ lag $cn = 10 A \angle 240^{\circ}$ lag		4			4		1.7 s	_

⁴ activated; 8 Not Activated

7.3.11 Distance Element Accuracy

The theoretical impedance on the R-X plane can be calculated as:

$$Z_{i} = \frac{0.875 \times Z_{d} \times \cos(\theta_{d} - \theta_{i}) + \sqrt{(0.875 \times Z_{d} \times \cos(\theta_{d} - \theta_{i}))^{2} + 4 \times Z_{d}^{2} \times 0.125}}{2}$$
(EQ 7.10)

where: Z_d = programmed distance impedance θ_d = programmed distance characteristic angle

 θ_i = variable angle on the R-X plane at point *i* for which boundary impedance is to be calculated

It is recommended that voltage is kept constant while increasing the current magnitude at certain angles referenced to voltage phase A until element operates.

Then the expected operating current (assuming that current in the two phases are 180° apart) can be calculated as:

$$\hat{l}_{i} = \frac{\overrightarrow{V_{o}} - \overrightarrow{V_{b}}}{2\overrightarrow{Z}_{i}}$$
 (EQ 7.11)

where
$$\vec{Z}_i = Z_i \times e^{j\theta_i}$$
.



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A.1 Stator Ground Fault

A.1.1 Description



This application note describes general protection concepts and provides guidelines on the use of the 489 to protect a generator stator against ground faults. Detailed connections for specific features must be obtained from the relay manual. Users are also urged to review the material contained in the 489 manual on each specific protection feature discussed here.

The 489 Generator Management Relay offers a number of elements to protect a generator against stator ground faults. Inputs are provided for a neutral-point voltage signal and for a zero-sequence current signal. The zero-sequence current input can be into a nominal 1 A secondary circuit or an input reserved for a special GE Multilin type HGF ground CT for very sensitive ground current detection. Using the HGF CT allows measurement of ground current values as low as 0.25 A primary. With impedance-grounded generators, a single ground fault on the stator does not require that the unit be quickly removed from service. The grounding impedance limits the fault current to a few amperes. A second ground fault can, however, result in significant damage to the unit. Thus the importance of detecting all ground faults, even those in the bottom 5% of the stator. The fault detection methods depend on the grounding arrangement, the availability of core balance CT, and the size of the unit. With modern full-featured digital generator protection relays such as the 489, users do not incur additional costs for extra protection elements as they are all part of the same device. This application note provides general descriptions of each of the elements in the 489 suitable for stator ground protection, and discusses some special applications.

A.1.2 Neutral Overvoltage Element

The simplest, and one of the oldest methods to detect stator ground faults on high-impedance-grounded generators, is to sense the voltage across the stator grounding resistor (See References [1, 2] at the end of this section). This is illustrated, in a simplified form in the figure below. The voltage signal is connected to the $V_{neutral}$ input of the 489, terminals E10 and F10. The $V_{neutral}$ signal is the input signal for the 489 neutral overvoltage protection element. This element has an alarm and a trip function, with separately adjustable operate levels and time delays. The trip function offers a choice of timing curves as well as a definite time delay. The neutral overvoltage function responds to fundamental frequency voltage at the generator neutral. It provides ground fault protection for approximately 95% of the stator winding. The limiting factor is the level of voltage signal available for a fault in the bottom 5% of the stator winding. The element has a range of adjustment, for the operate levels, of 2 to 100 V.

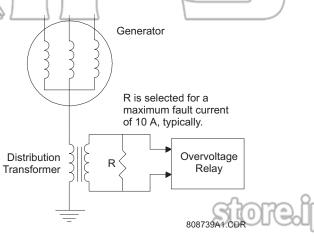


FIGURE A-1: Stator Ground Fault Protection

The operating time of this element should be coordinated with protective elements downstream, such as feeder ground fault elements, since the neutral overvoltage element will respond to external ground faults if the generator is directly connected to a power grid, without the use of a delta-wye transformer.

In addition, the time delay should be coordinated with the ground directional element (discussed later), if it is enabled, by using a longer delay on the neutral overvoltage element than on the directional element.

It is recommended that an isolation transformer be used between the relay and the grounding impedance to reduce common mode voltage problems, particularly on installations requiring long leads between the relay and the grounding impedance.

When several small generators are operated in parallel with a single step-up transformer, all generators may be grounded through the same impedance (the impedance normally consists of a distribution transformer and a properly sized resistor). It is possible that only one generator is grounded while the others have a floating neutral point when connected to the power grid (see the figure below). This operating mode is often adopted to prevent circulation of third-harmonic currents through the generators, if the installation is such that all the star points would end up connected together ahead of the common grounding impedance (if each generator has its own grounding impedance, the magnitude of the

circulating third harmonic current will be quite small). With a common ground point, the same $V_{neutral}$ signal is brought to all the relays but only the one which is grounded should have the neutral overvoltage element in service.

For these cases, the neutral overvoltage element has been provided with a supervising signal obtained from an auxiliary contact off the grounding switch. When the grounding switch is opened, the element is disabled. The grounding switch auxiliary contact is also used in the ground directional element, as is the breaker auxiliary contact, as discussed later.

If all the generators are left grounded through the same impedance, the neutral overvoltage element in each relay will respond to a ground fault in any of the generators. For this reason, the ground directional element should be used in each relay, in addition to the neutral overvoltage element.

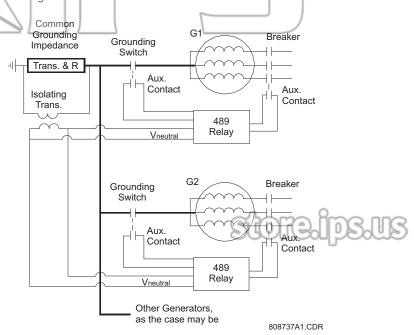


FIGURE A-2: Parallel Generators with Common Grounding Impedance

A.1.3 Ground Overcurrent Element

The ground overcurrent element can be used as a direct replacement or a backup for the neutral overvoltage element, with the appropriate current signal from the generator neutral point, for grounded generators. This element can also be used with a Core Balance CT, either in the neutral end or the output end of the generator, as shown below. The use of the special CT, with its dedicated input to the relay, offers very sensitive current detection, but still does not offer protection for the full stator. The setting of this element must be above the maximum unbalance current that normally flows in the neutral circuit. Having the element respond only to the fundamental frequency component allows an increase in sensitivity.

The core balance CT can be a conventional CT or a 50:0.025 Ground CT, allowing the measurement of primary-side current levels down to 0.25 A. Using a Core Balance CT, on the output side of the transformer will provide protection against stator ground faults in ungrounded generators, provided that there is a source of zero-sequence current from the grid.

Though in theory one could use this element with a zero sequence current signal obtained from a summation of the three phase currents (neutral end or output end), by connecting it in the star point of the phase CTs, Options 4 and 5 in the figure below, this approach is not very useful. The main drawback, for impedance-grounded generators is that the zero-sequence current produced by the CT ratio and phase errors could be much larger than the zero sequence current produced by a real ground fault inside the generator.

Again the time delay on this element must be coordinated with protection elements downstream, if the generator is grounded. Refer to *Ground Directional* on page 5–40 for the range of settings of the pickup levels and the time delays. The time delay on this element should always be longer than the longest delay on line protection downstream.

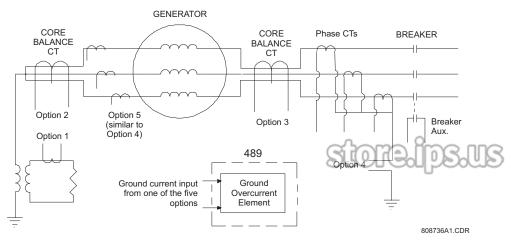


FIGURE A-3: Ground Overcurrent Element with Different Current Source Signals

A.1.4 Ground Directional Element

The 489 can detect internal stator ground faults using a Ground Directional element implemented using the $V_{neutral}$ and the ground current inputs. The voltage signal is obtained across the grounding impedance of the generator. The ground, or zero sequence, current is obtained from a core balance CT, as shown below (due to CT inaccuracies, it is generally not possible to sum the outputs of the conventional phase CTs to derive the generator high-side zero sequence current, for an impedance-grounded generator).

If correct polarities are observed in the connection of all signals to the relay, the $V_{neutral}$ signal will be in phase with the ground current signal. The element has been provided with a setting allowing the user to change the plane of operation to cater to reactive grounding impedances or to polarity inversions.

This element's normal 'plane of operation' for a resistor-grounded generator is the 180° plane, as shown in FIGURE A–4: Ground Directional Element Polarities and Plane of Operation, for an internal ground fault. That is, for an internal stator-to-ground fault, the $V_{\rm o}$ signal is 180° away from the $I_{\rm o}$ signal, if the polarity convention is observed. If the

grounding impedance is inductive, the plane of operation will be the 270° plane, again, with the polarity convention shown below. If the polarity convention is reversed on one input, the user will need to change the plane of operation by 180°.

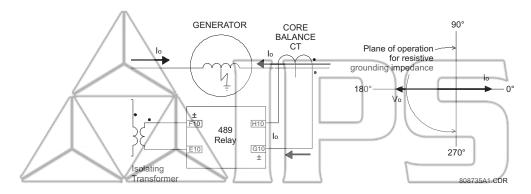


FIGURE A-4: Ground Directional Element Polarities and Plane of Operation

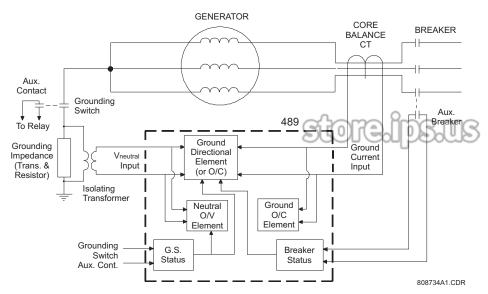


FIGURE A–5: Ground Directional Element Conceptual Arrangement

The operating principle of this element is quite simple: for internal ground faults the two signals will be 180° out of phase and for external ground faults, the two signals will be in phase. This simple principle allows the element to be set with a high sensitivity, not normally possible with an overcurrent element.

The current pickup level of the element can be adjusted down to $0.05 \times CT$ primary, allowing an operate level of 0.25 A primary if the 50:0.025 ground CT is used for the core balance. The minimum level of $V_{neutral}$ at which the element will operate is determined by hardware limitations and is internally set at 2.0 V.

Because this element is directional, it does not need to be coordinated with downstream protections and a short operating time can be used. Definite time delays are suitable for this element.

Applications with generators operated in parallel and grounded through a common impedance require special considerations. If only one generator is grounded and the other ones left floating, the directional element for the floating generators does not receive a correct $V_{neutral}$ signal and therefore cannot operate correctly. In those applications, the element makes use of auxiliary contacts off the grounding switch and the unit breaker to turn the element into a simple overcurrent element, with the pickup level set for the directional element (note that the ground directional element and the ground overcurrent elements are totally separate elements). In this mode, the element can retain a high sensitivity and fast operate time since it will only respond to internal stator ground faults. The table below illustrates the status of different elements under various operating conditions.

Table A-1: Detection Element Status

Generator Condition	Unit Ground Breaker Switch		Element				
Condition	Breaker	Switch	Ground Directional	Neutral Overvoltage	Ground Overcurrent		
Shutdown	Open	Open	Out-of-service	Out-of-service	In-service		
Open Circuit and grounded	Open	Closed	In-service (but will not operate due to lack of I ₀)	In-service	In-service		
Loaded and Grounded	Closed	Closed	In-service	In-service	In-service		
Loaded and Not Grounded	Closed	Open	In service as a simple overcurrent element	Out-of-service	In-service		

A.1.5 Third Harmonic Voltage Element

The conventional neutral overvoltage element or the ground overcurrent element are not capable of reliably detecting stator ground faults in the bottom 5% of the stator, due to lack of sensitivity. In order to provide reliable coverage for the bottom part of the stator, protective elements, utilizing the third harmonic voltage signals in the neutral and at the generator output terminals, have been developed (see Reference 4).

In the 489 relay, the third-harmonic voltage element, Neutral Undervoltage (3rd Harmonic) derives the third harmonic component of the neutral-point voltage signal from the $V_{neutral}$ signal as one signal, called V_{N3} . The third harmonic component of the internally summed phase-voltage signals is derived as the second signal, called V_{P3} . For this element to perform as originally intended, it is necessary to use wye-connected VTs.

Since the amount of third harmonic voltage that appears in the neutral is both load and machine dependent, the protection method of choice is an adaptive method. The following formula is used to create an adaptive third-harmonic scheme:

$$\frac{V_{N3}}{V_{P3}/3 + V_{N3}} \le 0.15$$
 which simplifies to $V_{P3} \ge 17V_{N3}$ (EQ 1.1)

The 489 tests the following conditions prior to testing the basic operating equation to ensure that V_{N3} is of a measurable magnitude:

$$V_{P3'} > 0.25 \text{ V}$$
 and $V_{P3'} \ge \text{Permissive_Threshold} \times 17 \times \frac{\text{Neutral CT Ratio}}{\text{Phase CT Ratio}}$ (EQ 1.2)

where: V_{N3} is the magnitude of third harmonic voltage at the generator neutral V_{P3} is the magnitude of third harmonic voltage at the generator terminals V_{P3} and V_{N3} are the corresponding voltage transformer secondary values Permissive_Threshold is 0.15 V for the alarm element and 0.1875 V for the trip element

In addition, the logic for this element verifies that the generator positive sequence terminal voltage is at least 30% of nominal, to ensure that the generator is actually excited.

This method of using 3rd harmonic voltages to detect stator ground faults near the generator neutral has proved feasible on larger generators with unit transformers. Its usefulness in other generator applications is unknown.

If the phase VT connection is "Open Delta", it is not possible to measure the third harmonic voltage at the generator terminals and a simple third harmonic neutral undervoltage element is used. In this case, the element is supervised by both a terminal voltage level and by a power level. When used as a simple undervoltage element, settings should be based on measured 3rd harmonic neutral voltage of the healthy machine. It is recommended that the element only be used for alarm purposes with open delta VT connections.

A.1.6 References

- 1. C. R. Mason, "The Art & Science of Protective Relaying", John Wiley & Sons, Inc., 1956, Chapter 10.
- 2. J. Lewis Blackburn, "Protective Relaying: Principles and Applications", Marcel Dekker, Inc., New York, 1987, chapter 8.
- 3. GE Multilin, "Instruction Manual for the 489 Generator Management Relay".
- 4. R. J. Marttila, "Design Principles of a New Generator Stator Ground Relay for 100% Coverage of the Stator Winding", IEEE Transactions on Power Delivery, Vol. PWRD-1, No. 4, October 1986.

A.2 Stator Differential Protection Special Application

A.2.1 Background

The 489 relay is applied in a dual breaker arrangement as shown in the figure below. In this configuration one breaker is closed at a time eliminating a danger of through fault conditions. However, the customer prefers not to sum up the two breaker currents to obtain effectively the terminal-side current of the generator, nor to install an extra CT at the generator to measure the terminal-side current explicitly. Instead, the customer applies two 489 relays each spanning its differential zone between the neutral-side CT of the generator and the CT at the corresponding breaker.

In this application, when a breaker is closed, the other (opposite) relay would measure the neutral-side current without the matching terminal-side current, as the latter flows via the other (closed) breaker and it not visible to the opposite relay.

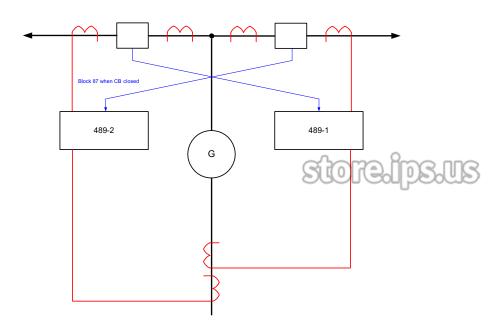


FIGURE A–6: Considered application of two 489s protecting a dual-breaker generator configuration

When both breakers are opened both relays be operational with the differential function enabled. The application is based on blocking the differential function using the position of the opposite breaker via the multiple setting group mechanism of the relay.

When both breakers are opened, both relays are in their setting group 1 with the differential functions operational. When a breaker is closed, its relay remains in group 1 so that no setting group switching takes place and therefore continuous uninterrupted protection is provided for the generator. At the same time the opposite relay is blocked by switching to group 2 in which the differential function is disabled. This prevents misoperation. There is no provision for an "advanced close" signal, and the breaker position signal is used instead.

In addition, enhanced differential protection algorithm takes care the timing offset between the main and auxiliary contacts of the breaker. As a result, maximum of 50ms timing offset between the main and auxiliary contacts of the breaker will block the differential function.

A.2.2 Stator Differential Logic

The differential function uses an internal timer of 130ms as shown in the figure below. This timer is a common timer for all three phases of the differential function. Normally, the timer is not engaged ensuring instantaneous operation and backward compatibility with the previous firmware revisions of the product.

The timer is engaged only when the terminal-side currents in all three phases are zero. If any of the terminal currents is above 5% of CT nominal, the timer is by-passed. Also, if any of the neutral-side current is above 5 times CT nominal, the timer is by-passed as well.

In this logic the current magnitudes are filtered fundamental frequency components (T stands for terminal-side currents, and N stands for neutral-side currents); PKP denotes the pickup state of the element prior to any user set delay that may or may not be used in a particular application; A, B and C designate phases.

The differential element works as follows:

With the machine under load, the terminal currents are above 5% of CT nominal and no delay is applied to the differential function.

With the machine on-line but with no load (below 5%) the delay is applied. However, should a fault occur at that time, at least one of the terminal current would get elevated cancelling the delay and resulting in an instantaneous trip.

With the opposite breaker being closed as in the considered dual-breaker application, a current is drawn (either transformer inrush or load or both). This will activate the differential characteristic. However, the timer remains engaged because all the terminal currents (ABC) are zero, and all the neutral-side currents (ABC) are below 5 times CT nominal. The timer keeps timing out. However, before it expires the relay switches to group 2 and blocks the differential function. This prevents misoperation.

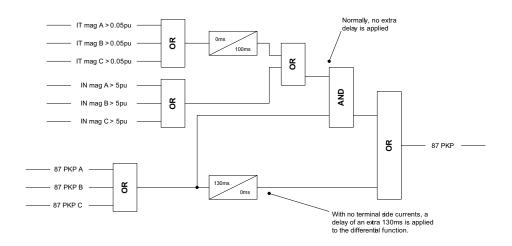


FIGURE A-7: Enhancements to the stator differential logic

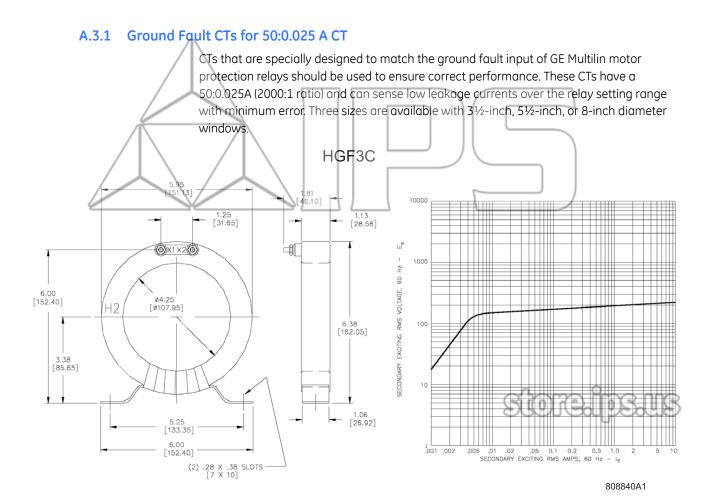
Should a fault occur during the first 50-60ms after closing the breaker, the corresponding relay would trip instantly. Before closing the breaker the corresponding relay too applies a delay. However, once the load/inrush current exceeds 5% of CT nominal, its timer is bypassed and instantaneous protection is provided.

Should a fault occur during generator start-up with both breakers opened, both relays would operate after the extra time delay of 130ms. This delay is acceptable under such conditions. Even this delay will be eliminated if the fault is heavy enough to draw more than 5 times CT nominal from the neutral-side of the generator.

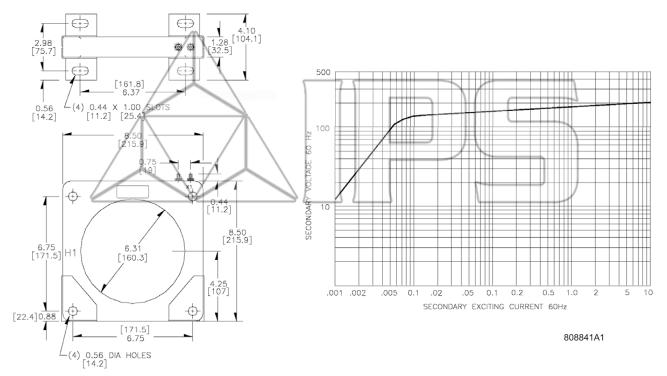
For proper implementation, the internal timer is cleared each time the 87 function becomes enabled (so that a partial time out from the previous "enabled" period does not affect the intended operation).



A.3 Current Transformers

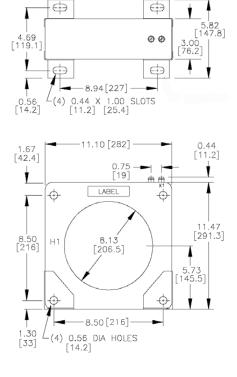


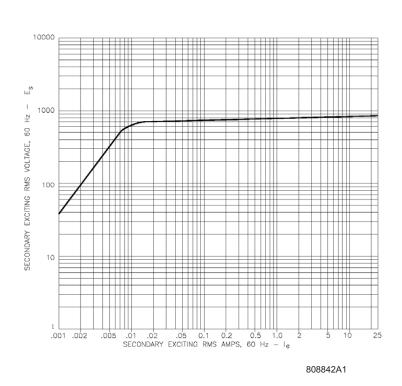
HGF5C



store.ips.us

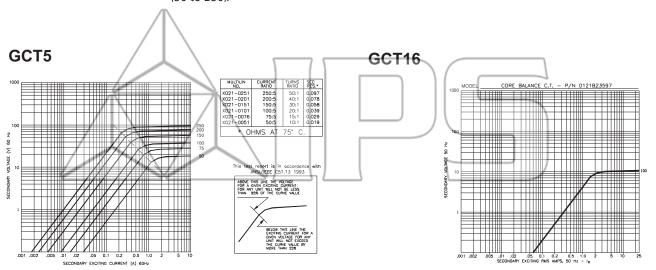
HGF8



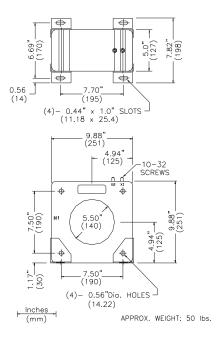


A.3.2 Ground Fault CTs for 5 A Secondary CT

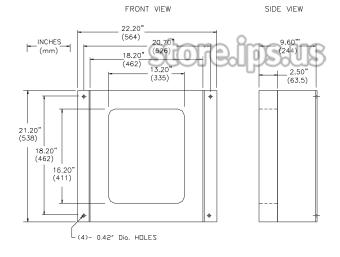
For low resistance or solidly grounded systems, a 5 A secondary CT should be used. Two sizes are available with $5\frac{1}{2}$ " or 13" \times 16" windows. Various Primary amp CTs can be chosen (50 to 250).



DIMENSIONS



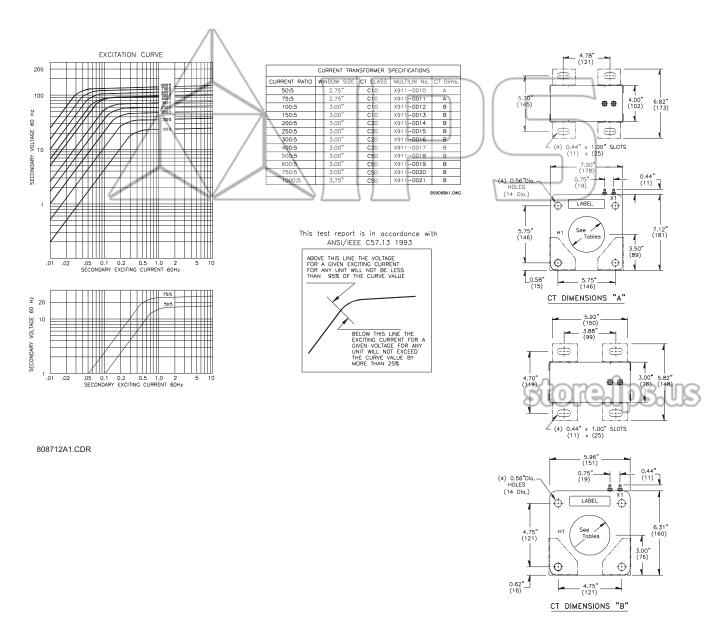
DIMENSIONS



808709A1.CDR

A.3.3 Phase CTs

Current transformers in most common ratios from 50.5 to 1000.5 are available for use as phase current inputs with motor protection relays. These come with mounting hardware and are also available with 1 A secondaries. Voltage class: 600 V BIL, 10 KV.



A.4 Time Overcurrent Curves

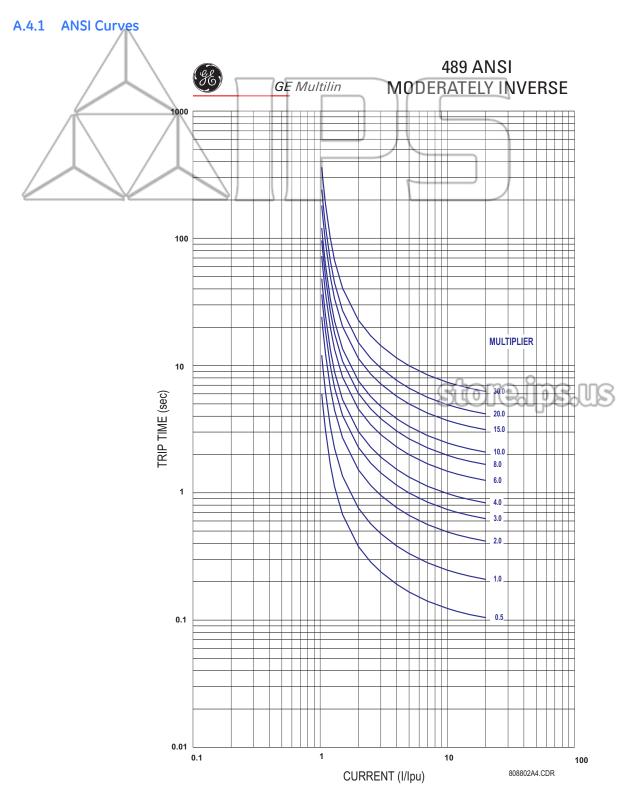
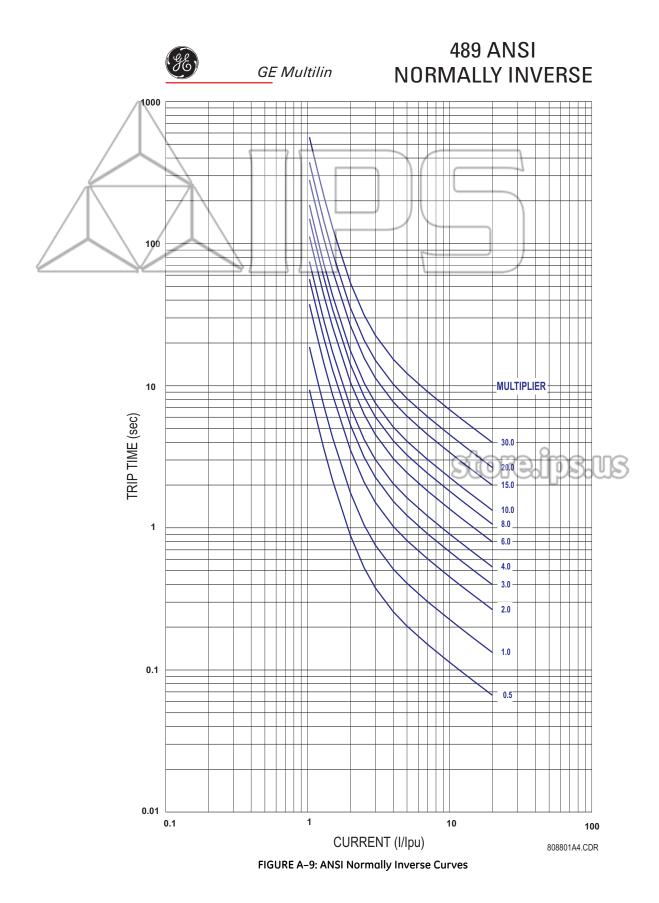
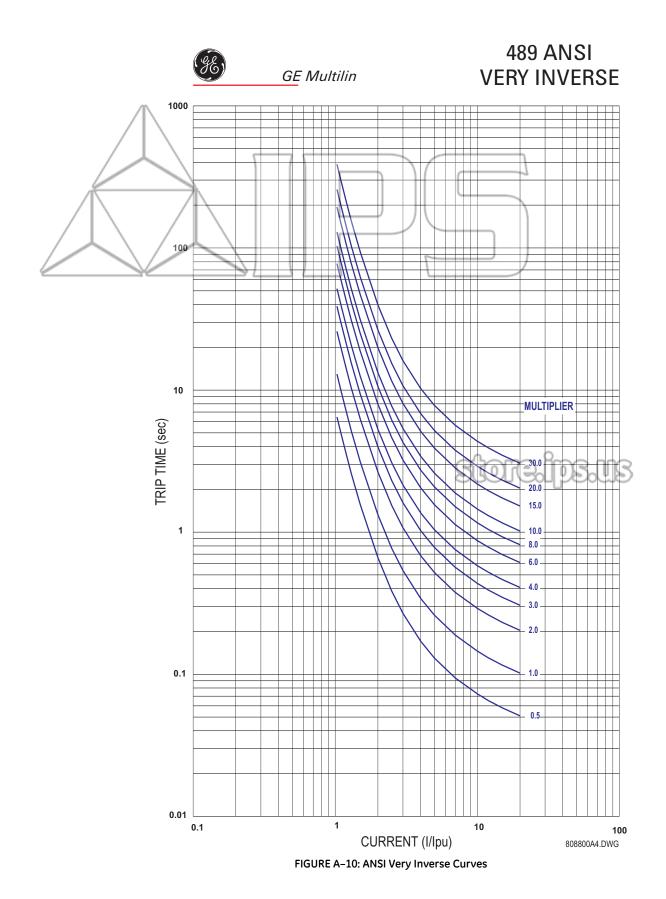


FIGURE A-8: ANSI Moderately Inverse Curves





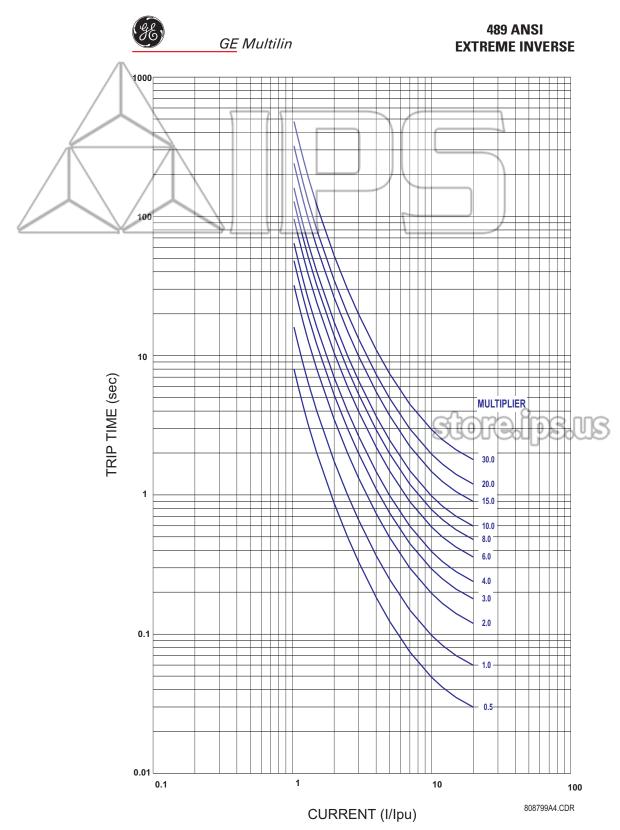


FIGURE A-11: ANSI Extremely Inverse Curves

A.4.2 Definite Time Curves

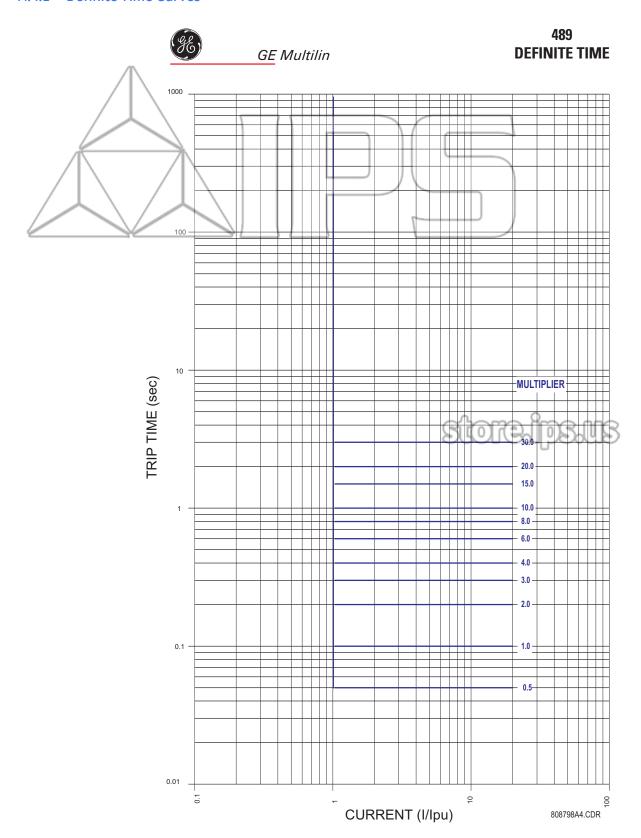


FIGURE A-12: Definite Time Curves

A.4.3 IAC Curves

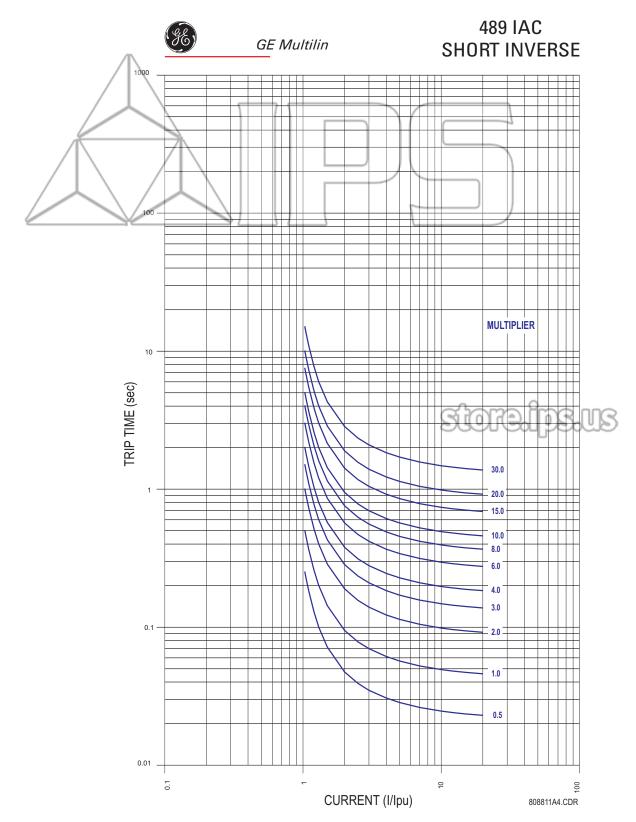
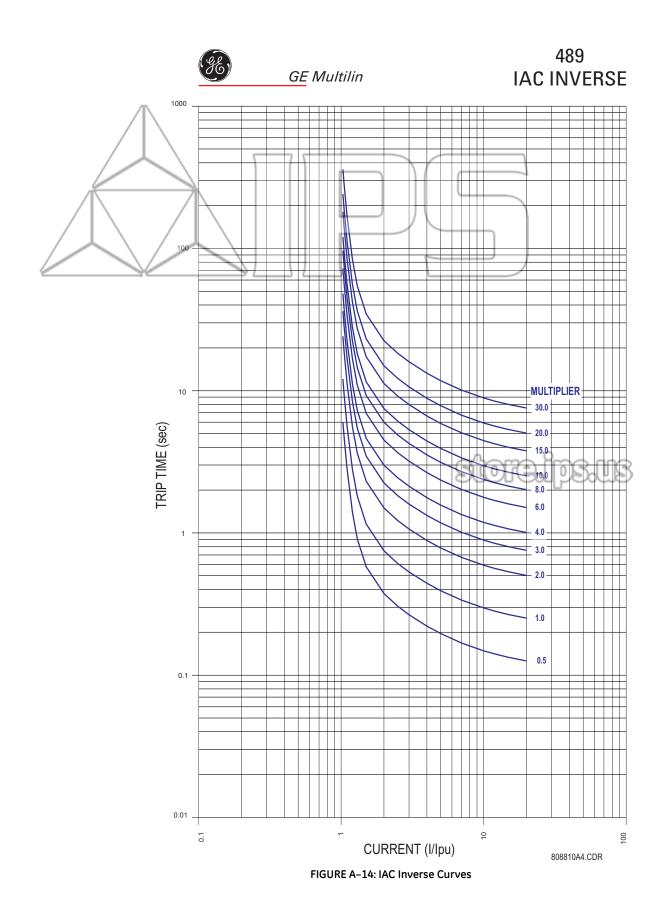
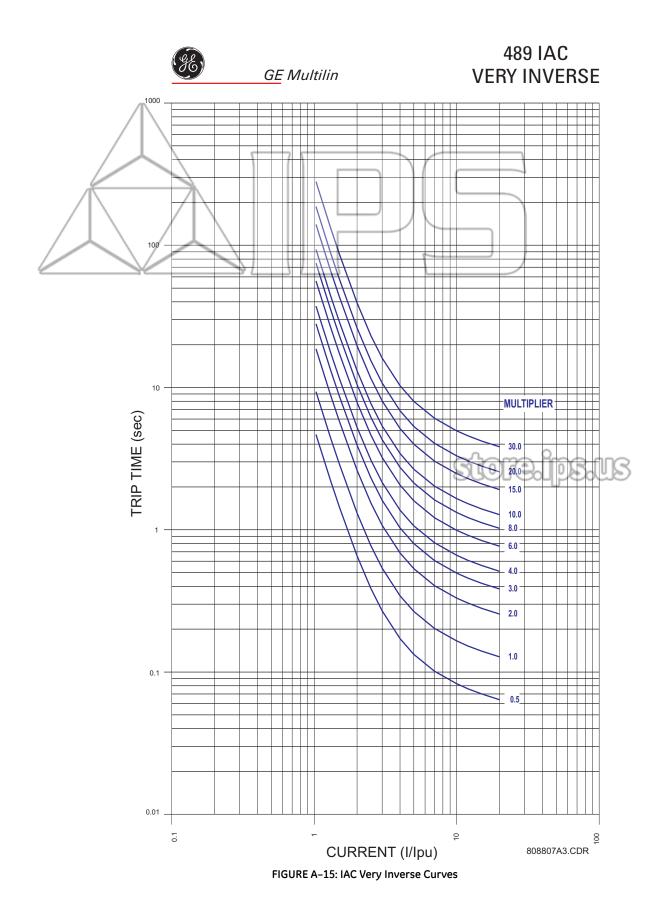
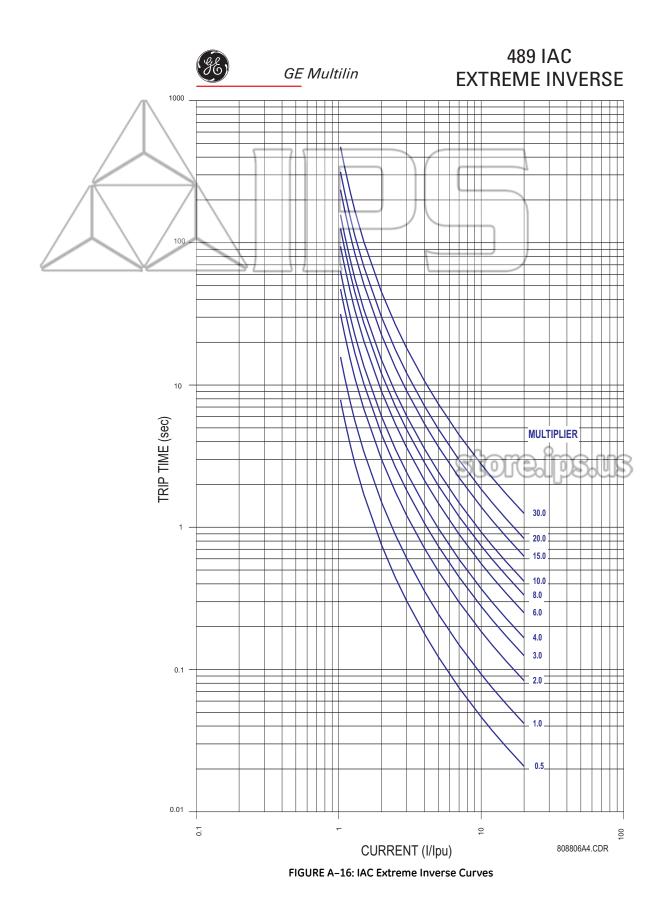


FIGURE A-13: IAC Short Inverse Curves







489 GENERATOR MANAGEMENT RELAY - INSTRUCTION MANUAL

A.4.4 IEC Curves

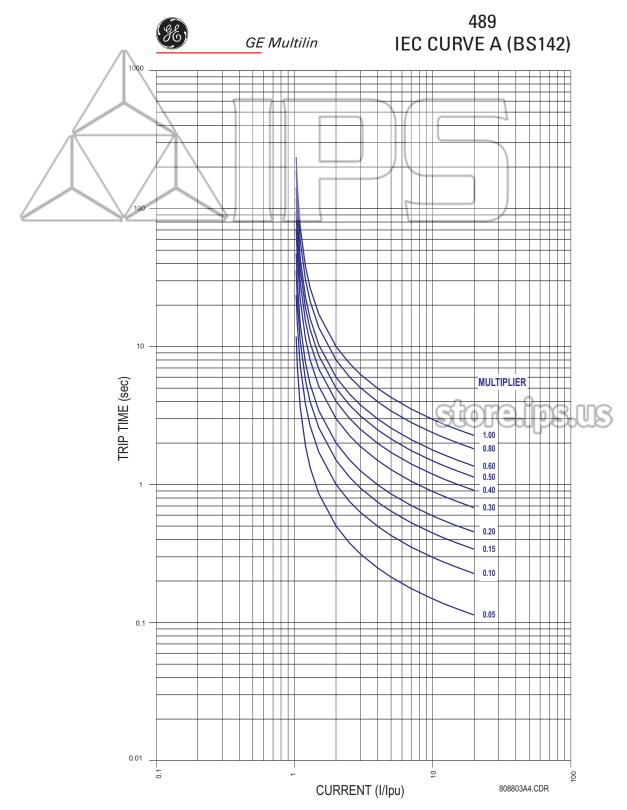
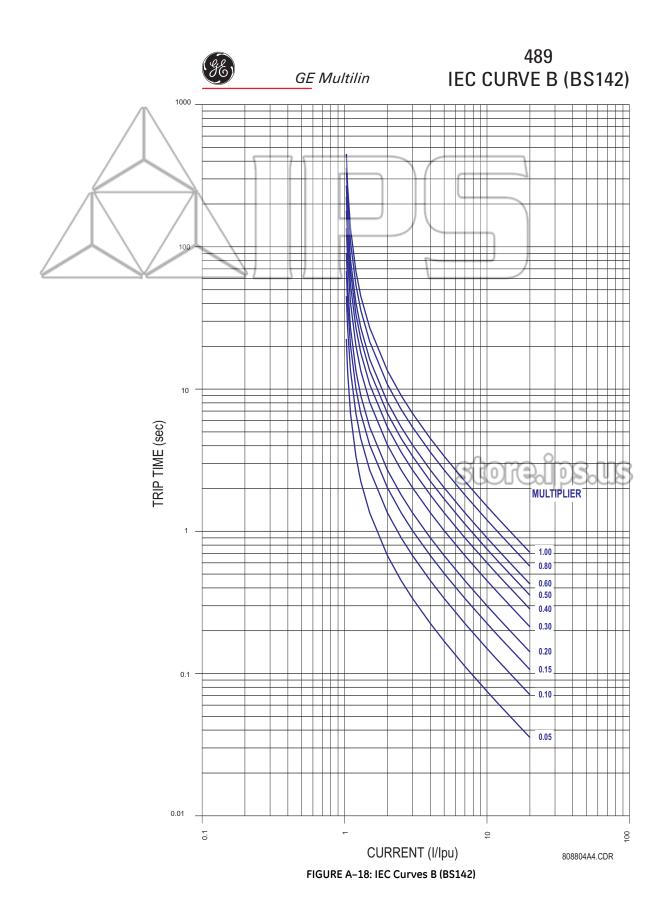
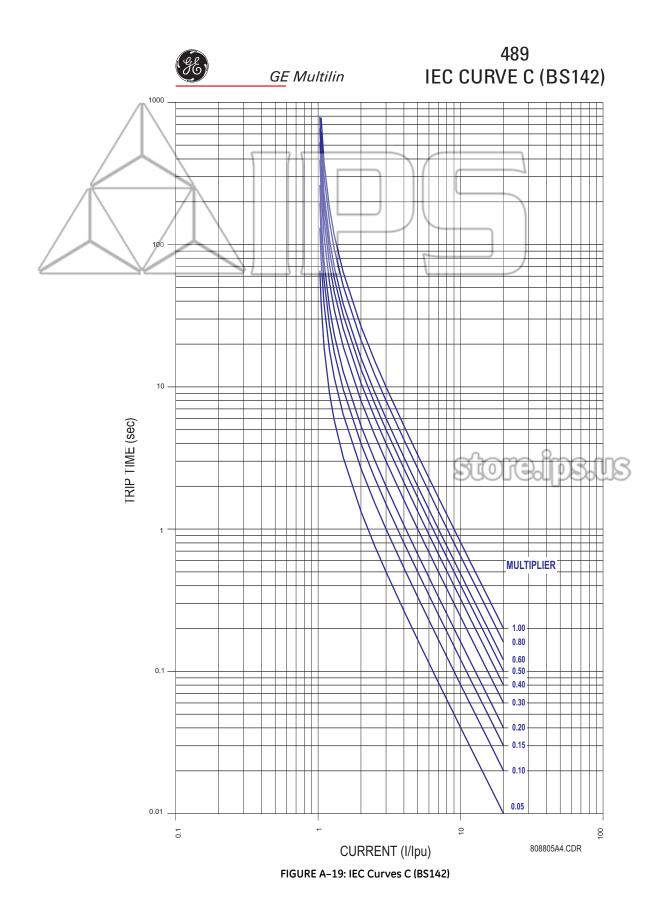


FIGURE A-17: IEC Curves A (BS142)





A.5 Revision History

A.5.1 Change Notes

Table A-2: Revision History

MANUAL P/N	REVISION	RELEASE DATE	ECO
1601-0150-A1	3.00	26 April 2004	489-249
1601-0150-A2	3.00	21 May 2004	
1601-0150 - A3	3.00	22 July 2004	J
1601-0150-A4			
1601-0150-A5	4.0x	21 July 2006	
1601-0150-A6	4.0x	9 February, 2007	
1601-0150-A7	4.0x	31 March, 2007	
1601-0150-A8	4.0x	3 April, 2008	
1601-0150-A9	4.0x	12 June, 2008	
1601-0150-AA	4.0x	10 September, 2008	
1601-0150-AB	4.0x	2 December, 2008	alinga
1601-0150-AC	4.0x	23 April, 2009	

A.5.2 Changes to the 489 Manual

Table A-3: Major Updates for 489 Manual Revision AC

SECT (AB)	SECT (AC)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-AC
4.1.7	4.1.7	Revision	Self-test Warnings table: Relay Not Configured revised.

Table A-4: Major Updates for 489 Manual Revision AB

SECT (AA)	SECT (AB)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-AB
2.2.5	2.2.5	Revision	Power Metering - changes to spec.

Table A-4: Major Updates for 489 Manual Revision AB

SECT (AA)	SECT (AB)	CHANGE	DESCRIPTION
7.3.2	7.3.2	Revision	Changes to specs.
//\			

Table A-5: Major Updates for 489 Manual Revision AA

SECT (A9)	SECT (AA)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-AA
5.6.9	5.6.9		Change Note (Pickup Level)

Table A-6: Major Updates for 489 Manual Revision A9

SECT (A8)	SECT (A9)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-A9
5.6.5	5.6.5		Fig 5-2: Change graph

Table A-7: Major Updates for 489 Manual Revision A8

SECT (A7)	SECT (A8)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-A8
2.1.2 2.2.5	2.1.2 2.2.5	Update	Changes to DC Power Supply range
fig 5-2	fig 5-2		Change graph
	8.2.1	Add	New Section: Stator Differential Protection
8.2.1	8.3.1	Update	Drawings changed
Equn 7.7	Equn 7.7	Update	Change equation

Table A-8: Major Updates for 489 Manual Revision A7

PAGE (A5)	SECT (A6)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-A6
5-31	5.6.8	Correction	Changes to step value - Differential Trip Delay

Table A–8: Major Updates for 489 Manual Revision A7

	PAGE (A5)	SECT (A6)	CHANGE	DESCRIPTION	
A	2-9	2.2.6	Correction	Changes to Littelfuse SLO-BLO data	
	2-7,8 5-39,40	2.2.3 5.7.5,6	Update	Changes to OverFrequency and Underfrequency parameters	
	\rightarrow	Tab	le A-9: Major	Updates for 489 Manual Revision A6	
	PAG E (A5)	PAG E (A6)	CHANGE	DESCRIPTION	
	Title	Title U	pdate	Manual part number to 1601-0150-A6	
	2-14	2-14 U	pdate	Changes to ELECTROSTATIC DISCHARGE value	

Table A-10: Major Updates for 489 Manual Revision A4

PAG E (A3)	PAG E (A4)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-A4
2-	2-	Update	Updated ORDERING section
2-	2-	Update	Updated SPECIFICATIONS section
	3-4	Add	Added ETHERNET COMMUNICATION section
5-		Remove	Removed SERIAL PORTS section
	5-	Add	Added COMMUNICATIONS section
5-44	5-44	Update	Updated DISTANCE ELEMENT section
	6-3	Add	Added NETWORK STATUS section
	7-16	Add	Added DISTANCE ELEMENT ACCURACY section

Table A-11: Major Updates for 489 Manual Revision A3

PAG E (A2)	PAG E (A3)	CHANGE	DESCRIPTION
Title	Title	Update	Manual part number to 1601-0150-A3

Table A–11: Major Updates for 489 Manual Revision A3

	PAG E (A2)	PAG E (A3)	CHANGE	DESCRIPTION			
,	5-67	5-67	Update	Updated THERMAL MODEL COOLING diagram to 808705A2			
	Table A–12: Major Updates for 489 Manual Revision A2						
	PAG E (A1)	PAG E (A2)	CHANGE	DESCRIPTION			
	Title	Title	Update	Manual part number to 1601-0150-A2			
	Addition	nal chang	ges for revision A	A2 were cosmetic. There was no change to content.			



EU Declaration of Conformity

A.6.1 EU Declaration of Conformity

General Electric Multilin

215 Anderson Ave. Markham, Ontario Canada. L6E 1B3 Tel: (905) 294-6222 Fax: (905) 294-8512

EU DECLARATION OF CONFORMITY

Applicable Council Directive(s): 1) 73/23/EEC The Low Voltage Directive

89/336/EEC The EMC Directive 2)

Standard(s) to Which Conformity is Declared:

Low-voltage switchgear and control gear EN 60947-1: 1999

Safety Requirements for Electrical Equipment for Measurement, Control and EN 1010-1:1990+ A 1:1992+ A 2:1995

Laboratory Use

EN 50263: 1999 EMC Product Standard for Measuring Relays and Protection Equipment

> General Electric Multilin Manufacturer's Name:

Manufacturer's Address: 215 Anderson Ave.

Markham, Ontario, Canada

L6E 1B3

Jokin Galletero Manufacturer's Representative in the EU:

GE Multilin

Avenida Pinoa 10

48170 Zamudio, Spain

Tel.: 34-94-4858817 Fax: 34-94-4858838

Type of Equipment:

Protection & Control Relay

Model Number:

SR489

First Year of Manufacture:

1999

I the undersigned, hereby declare that the equipment specified above conforms to the above Directives and Standards.

Full Name:

Jeff Mazereeuw

Position:

Technology Manager

Signature:

Place:

GE Multilin

Date:

February 13, 2006

A.7 Warranty

A.7.1 GE Multilin Warranty

General Electric Multilin Inc. (GE Multilin) warrants each relay it manufactures to be free from defects in material and workmanship under normal use and service for a period of 24 months from date of shipment from factory.

In the event of a failure covered by warranty, GE Multilin will undertake to repair or replace the relay providing the warrantor determined that it is defective and it is returned with all transportation charges prepaid to an authorized service centre or the factory. Repairs or replacement under warranty will be made without charge.

Warranty shall not apply to any relay which has been subject to misuse, negligence, accident, incorrect installation or use not in accordance with instructions nor any unit that has been altered outside a GE Multilin authorized factory outlet.

GE Multilin is not liable for special, indirect or consequential damages or for loss of profit or for expenses sustained as a result of a relay malfunction, incorrect application or adjustment.

For complete text of Warranty (including limitations and disclaimers), refer to GE Multilin Standard Conditions of Sale.



Index

	Λ	
	Numerics	
/		
	0-1mA ANALOG INPUT	3-15
	4-20mA ANALOG INPUT	
	50:0.025 CT	3-12
/ \		
	$A/I \setminus I$	
	ACCESS SWITCH	5-21
	ACCESSORIES	/
,	ACTUAL VALUES	
	messages	6-3
	ALARM PICKUPS	
	ALARM RELAY	
	ALARM STATUS	
	ALARMS	
	ANALOG IN MIN/MAX	
	ANALOG INPUTS	
	actual values	
	analog I/P min/max	
	min/max	
	minimums and maximums	
	setpoints	C3 1 0 1 (2) 1 0 C5-98 C
	specifications	2-6
	testing	
	ANALOG OUTPUTS	3-15
	setpoints	5-96
	specifications	2-7
	table	
	testing	
	ANSI CURVES	
	ANSI DEVICE NUMBERS	2-2
	APPLICATION NOTES	
	current transformers	
	stator ground fault	
	AUXILIARY RELAY	3-17, 5-28
	В	
	BAUD RATE	2 14 5 12
	setpoints	
	BREAKER FAILURE	
	BREAKER STATUS	
	BURDEN	
	C	
	CALIBRATION INFO	6.31
		₩ 94

CASE	2-15, 3-1
CAUSE OF EVENTS TABLE	6-29
CERTIFICATIONS	2-15
CHANGING SETPOINTS	1-9
CLEAR DATA	5-16
CLOCK	
COMM PORT MONITOR	
COLUMBIA	
monitoring	5-104
RS232	4-11, 4-15, 4-17
RS485	
setpoints	5-12
specifications	
wiring	4-11, 4-12
CONTROL FEATURES	5-6
CONTROL POWER	3-10
COOLING	5-85
COOLING TIME CONSTANTS	
CORE BALANCE	
CT RATIO	
CTs	
burden	2-6
ground fault	
phase	
setpoints	
withstand	
CURRENT ACCURACY TEST	
CURRENT DEMAND	
CURRENT INPUTS	선생하다고 1120년 11
CURRENT METERING	6-16
CURRENT SENSING	
CURVES	
see OVERLOAD CURVES	
CUSTOM OVERLOAD CURVE	5-76
COSTOTT OVERLOAD CONVE	5-7 O
D	
DEFAULT MESSAGES	
DEFINITE TIME CURVE	
DEMAND DATA	
DEMAND METERING	
DEMAND PERIOD	5-94
DESCRIPTION	2-1
DEVICE NUMBERS	2-2
DIAGNOSTIC MESSAGES	6-32
DIELECTRIC STRENGTH	
specifications	2-14
testing	
DIFFERENTIAL CURRENT ACCURACY TEST	7-5
DIGITAL COUNTER	
DIGITAL INPUTS	
actual values	
dual setpoints	
field-breaker discrepancy	
general input	
- · · · · · · · · · · · · · · · · · · ·	

	ground switch status	5-27
	remote reset	5-23
	sequential trip	5-25
	specifications	
	tachometer	
	ntest input	
/	testing	
/	thermal reset	
	DIMENSIONS	
	DISPLAY	
	DISTANCE ELEMENTS	
	DRAWOUT INDICATOR	
/ \	DUAL SETPOINTS	5-8, 5-24
/ \		·
	É \	
	EMERGENCY RESTARTS	5-23
	ENERVISTA VIEWPOINT WITH THE 489	
	ENTERING TEXT	
	ENVIRONMENT	2-15
	ETHERNET	
	actual values	6-4
	setpoints	5-13
	EU	
	EU Declaration of Conformity	
	EVENT RECORD	
	cause of events	2.22
		and the second s
	EVENT RECORDER5	-17, 5-23, 6-28
	2000	
		0
	F	
	EACTORY CERVICE	
	FACTORY SERVICE	
	FAULT SETUP	
	FEATURES	2-2, 2-3, 2-10
	FIELD-BREAKER DISCREPANCY	2-11
	FIRMWARE	
	upgrading via EnerVista 489 setup software	4-30
	FLEXCURVE	
	FLOW	
	FREQUENCY TRACKING	2-6
	FRONT PANEL	
	using	1-3
	FUSE	
	G	
	G GENERAL COUNTERS	6-27
	GENERAL COUNTERSGENERAL INPUTS	6-27 2-12, 5-22
	GENERAL COUNTERS	6-27 2-12, 5-22 5-17
	GENERAL COUNTERS	6-27 2-12, 5-22 5-17 6-22
	GENERAL COUNTERS	6-27 2-12, 5-22 5-17 6-22
	GENERAL COUNTERS	6-27 2-12, 5-22 5-17 6-22 5-19

	GROUND CT	
	burden	2-6
	setpoint	5-18
	withstand	
	GROUND CURRENT ACCURACY TEST	
	GROUND CURRENT INPUT	3-12
	GROUND DIRECTIONAL	5-40, A-4
	GROUND FAULT CTs	A-13
/	GROUND OVERCURRENT	5-38, A-3
//	GROUND SWITCH STATUS	
		+
/ \	(H / \ \ \ \	
/	\/	
	HELP KEY	1-10
	HIGH-SET PHASE OVERCURRENT	5-42
	HI-POT	3-18
	HOT/COLD SAFE STALL RATIO	5-87
	I	
	IAC CURVES	5.04.4.00
		· · · · · · · · · · · · · · · · · · ·
	IDENTIFICATION	
	IEC CURVES	
	IED SETUP	
	INADVERTENT ENERGIZATION	
	INJECTION TEST SETUP	7-3, 7-15, 7-19
	INPUTS	ethana ina u
	analog	2-6, 3-14
	Current	2-1, 3-11, 3-12
	digital	
	general	
	RTD	•
	voltage	
	INSERTION	
	INSPECTION CHECKLIST	
	INSTALLATION	
	IRIG-B	3-17, 5-13
	K	
	KEYPAD	4.2
	help	
	πειρ	1-10
	L	
	_	
	LAST TRIP DATA	
	LEARNED PARAMETERS	5-23
	LEDs	4-1, 4-2, 4-3
	LONG-TERM STORAGE	
	LOOP POWERED TRANSDUCERS	
	LOSS OF EXCITATION	
	LOSS OF LOAD	
	LOW FORWARD POWER	
	LOVVIONVVAND FOVVLN	ე-თა

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3 4 4 4 8 6 7 7 7 7
3 4 4 4 8 6 4 7 7 7 7 7
3 4 4 4 8 6 7 7 7 7 7 7 7 8
3 4 4 4 8 6 4 7 7 7 7 7

	OUTPUTS	
	analog	2-7, 3-15
	OVERCURRENT	
	ground	5-38
	ground directional	5-40
	high-set	
	negative-sequence	
	phase	
	phase differential	
/	setpointsspecifications	
1	TOC	
/ \	OVERCURRENT ALARM	
/	OVERCURRENT CURVES	5-33
/]	ANSI	Δ_15
	characteristics	
	definite time	
	graphs	
	IAC	
	IEC	•
	OVERFREQUENCY	2-10, 5-50
	OVERLOAD CURVE MULTIPLIERS	
	OVERLOAD CURVES	
	custom	5-76
	definite time	
	standard multipliers	5-75
	testing	7-12
	OVERVOLTAGE	2 10 5 11
	OVERVOLIAGE	2-10, 3-44
	OVERVOLINGE	2-10, 5-44
	P	
	P	tore.ips.
	PACKAGING	2-15
	PACKAGINGPARAMETER AVERAGES	2-15 6-22
	PACKAGINGPARAMETER AVERAGESPARITY	2-15 6-22 5-12, 5-13
	PACKAGING	2-15 6-22 5-12, 5-13 5-9, 6-1
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND	2-15 6-22 5-12, 5-13 5-9, 6-1 5-17, 6-20
	PACKAGING	2-15 6-22 5-12, 5-13 5-9, 6-1 5-17, 6-20 5-18, 5-19
	PACKAGING	2-15 6-22 5-12, 5-13 5-9, 6-1 5-17, 6-20 5-18, 5-19 A-13
	PACKAGING	2-156-225-12, 5-135-9, 6-15-17, 6-205-18, 5-19
	PACKAGING	2-156-225-12, 5-135-9, 6-15-17, 6-205-18, 5-19A-133-115-39
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST	2-156-225-12, 5-135-9, 6-15-17, 6-205-18, 5-19A-13A-133-115-397-16
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE OVERCURRENT	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE OVERCURRENT PHASE REVERSAL	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL	
	PACKAGING	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL TEST POSITIVE-SEQUENCE CURRENT POWER DEMAND	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST PHASE OVERCURRENT PHASE REVERSAL POSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL PHOSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS POWER MEASUREMENT TEST	2-15
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTs PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL POSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS POWER MEASUREMENT TEST POWER MEASUREMENT TEST	2-15
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL TEST POSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS POWER MEASUREMENT TEST POWER METERING POWER SUPPLY	2-15
	PACKAGING	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL TEST POSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS POWER MEASUREMENT TEST POWER METERING POWER SUPPLY	
	PACKAGING	
	PACKAGING	
	PACKAGING PARAMETER AVERAGES PARITY PASSCODE PEAK DEMAND PHASE CT PRIMARY PHASE CTS PHASE CURRENT INPUTS PHASE DIFFERENTIAL PHASE DIFFERENTIAL TRIP TEST PHASE OVERCURRENT PHASE REVERSAL PHASE REVERSAL PHASE REVERSAL TEST POSITIVE-SEQUENCE CURRENT POWER DEMAND POWER MEASUREMENT CONVENTIONS POWER MEASUREMENT TEST POWER METERING POWER SUPPLY POWER SYSTEM PRE-FAULT SETUP PREFERENCES	

	PRODUCTION TESTS	2-14
	PROTECTION FEATURES	2-3
	PROXIMITY PROBE	3-14
	PULSE OUTPUT	
/	N-	
/	Ŕ	
	REACTIVE POWERREACTIVE POWER TEST	5-61
	REACTIVE POWER TEST	7-13
	REAL TIME CLOCK	5-13, 6-15
	RELAY ASSIGNMENT PRACTICES	5-7
/ \	RELAY RESET MODE	5-28
	REMOTE RESET	5-23
	RESETTING THE 489	5-28
	RESIDUAL GROUND CONNECTION	3-12
	REVERSE POWER	5-62
	REVISION HISTORY	
	RS232 COMMUNICATIONS	
	configuring with EnerVista 469 setup	
	configuring with EnerVista 489 setup	
	configuring with EnerVista 750/760 Setup	
	connections	
	RS485 COMMUNICATIONS	
	configuring with EnerVista 469 setup	•
	configuring with EnerVista 489 setup	
	configuring with EnerVista 750/760 Setup	
	connections	
	RTD actual values	51(0)(=) 610 623
	maximums	
	sensor connections	
	setpoints	
	specifications	
	testing	
	RTD ACCURACY TEST	
	RTD BIAS	
	RTD MAXIMUMS	
	RTD SENSOR, OPEN	
	RTD SHORT/LOW TEMPERATURE	
	RTD TYPES	
	RUNNING HOUR SETUP	
	RUNNING HOURS	5-23
	<u> </u>	
	S	
	SEQUENTIAL TRIP	2 12 5 25
	SERIAL PORTS	
	SERIAL START/STOP INITIATION	
	SERVICE RELAY	
	SETPOINT ENTRY	
	SETPOINT MESSAGE MAP	5-1
	SETPOINTS	
	changing	1-9
	dual setpoints	5-8

	entering with EnerVista 489 setup softwareloading from a file	
	messages	
	numerical	1-10
	saving to a file	4-30
	text	
	SIMULATION MODE	5-100
/	SINGLE LINE DIAGRAM	2-1
/	SLAVE ADDRESS	5-13
/	SOFTWARE	
	entering setpoints	4-21
	hardware requirements	4-10
/ \	installation	
/ \	loading setpoints	4-28
/ \ \ \	overview	4-10
	saying setpoints	
	serial communications	
	SPECIFICATIONS	
	SPEED	6-21
	STANDARD OVERLOAD CURVES	
	multipliers	5-75
	STARTER	
	information	
	operations	
	status	5-21
	STATOR GROUND FAULT PROTECTION	
	STATUS LEDs	4-2
	T Si	iore.ips.l
	TACHOMETER	2-12, 5-26, 6-21
	TACHOMETER TEMPERATURE	2-12, 5-26, 6-21 6-19
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY	2-12, 5-26, 6-21 6-19 5-10
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT	2-12, 5-26, 6-21 6-19 5-10 3-7
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS	2-12, 5-26, 6-21
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS TERMINAL SPECIFICATIONS	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT	2-12, 5-26, 6-21
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS TERMINAL SPECIFICATIONS	2-12, 5-26, 6-21
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL LOCATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-23
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-23 5-102
	TACHOMETER	2-12, 5-26, 6-21
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102 7-5 7-5 7-6 7-5
	TACHOMETER	2-12, 5-26, 6-21
	TACHOMETER	2-12, 5-26, 6-21
	TACHOMETER	2-12, 5-26, 6-21
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LOCATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT TEST OUTPUT RELAYS TESTS differential current accuracy ground current accuracy list negative-sequence current accuracy neutral current accuracy neutral voltage accuracy output current accuracy output relays overload curves	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102 7-5 7-5, 7-15 7-6 7-6 7-6 7-6 7-6 7-1 7-1 7-1 7-1 7-1
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL SPECIFICATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT TEST OUTPUT RELAYS TESTS differential current accuracy ground current accuracy list negative-sequence current accuracy neutral current accuracy neutral voltage accuracy output current accuracy output relays overload curves phase current accuracy	
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL SPECIFICATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT TEST OUTPUT RELAYS TESTS differential current accuracy ground current accuracy list negative-sequence current accuracy neutral voltage accuracy output current accuracy output relays overload curves phase current accuracy power measurement	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102 7-5 7-5 7-6 7-6 7-6 7-6 7-1 7-6 7-1
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL SPECIFICATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT TEST OUTPUT RELAYS TESTS differential current accuracy ground current accuracy list negative-sequence current accuracy neutral current accuracy neutral voltage accuracy output current accuracy output relays overload curves phase current accuracy power measurement production tests	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102 7-5 7-1 7-6 7-6 7-6 7-6 7-1
	TACHOMETER	2-12, 5-26, 6-21 6-19 5-10 3-7 3-8 3-7 2-15 5-103 5-23 5-102 7-5 7-5 7-6 7-6 7-6 7-6 7-13 2-14 7-13
	TACHOMETER TEMPERATURE TEMPERATURE DISPLAY TERMINAL LAYOUT TERMINAL LIST TERMINAL SPECIFICATIONS TERMINAL SPECIFICATIONS TEST ANALOG OUTPUT TEST INPUT TEST OUTPUT RELAYS TESTS differential current accuracy ground current accuracy list negative-sequence current accuracy neutral current accuracy neutral voltage accuracy output current accuracy output relays overload curves phase current accuracy power measurement production tests	

	voltage input accuracy	7-4
	voltage phase reversal	7-14
	TEXT SETPOINTS	1-15
	THERMAL CAPACITY USED	6-4
	THERMAL ELEMENTS	5-89
/	THERMAL MODEL	
/	machine cooling	5-85
/	setpointssetpoints	
/ /	specifications	2-10
	unbalance bias	
	THERMAL RESET	5-23
	THIRD HARMONIC VOLTAGE	A-6
/ \	TIMETIME OVERCURRENT CURVES	5-13, 6-15
/ \	TIME OVERCURRENT CURVES	A-15
	TIMERS	6 27
	TOC CHARACTERISTICS	5-29
	TOC CURVES	Δ-15
	TRIP COIL MONITOR	
	TRIP COIL SUPERVISION	
	TRIP COUNTER	
	TRIP PICKUPS	
	TRIP RELAY	
	TRIP TIME ON OVERLOAD, ESTIMATED	
	TRIPS	
	TYPE TESTS	
	TYPICAL WIRING DIAGRAM	3-9
	u Sto	re.ips.us
	UNBALANCE BIAS	5-84
	UNDERFREQUENCY	5-49
	UNDERVOLTAGE	2-11, 5-43
	UNPACKING THE RELAY	•
	UPGRADING FIRMWARE	
	V	
	VIBRATION	
	VOLTAGE DEPENDENT OVERLOAD CURVE	5-77
	VOLTAGE INPUTS	
	description	3-14
	specifications	2-6
	testing	7-4
	VOLTAGE METERING	6-17
	VOLTAGE RESTRAINED OVERCURRENT	
	setpoints	5-35
	testing	7-20
	·	
	testingVOLTAGE SENSING	5-18
	testing VOLTAGE SENSING VOLTS/HERTZ	5-18 5-45
	testing VOLTAGE SENSING VOLTS/HERTZ VT FUSE FAILURE	5-18 5-45 5-92
	testing VOLTAGE SENSING VOLTS/HERTZ VT FUSE FAILURE VT RATIO	5-18 5-45 5-92 5-18
	testing VOLTAGE SENSING VOLTS/HERTZ VT FUSE FAILURE VT RATIO VTFF	5-18 5-45 5-92 5-18
	testing VOLTAGE SENSING VOLTS/HERTZ VT FUSE FAILURE VT RATIO	5-18 5-45 5-92 5-18 5-92

setpointswye connected	
W	
WARRANTY	A-27, A-31
	5-27
	3-10
WITHDRAWAL	3-4
	5-53

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